



November 30, 2023

File: LD-00318

VIA EMAIL

The Municipality of Middlesex Centre
1 Tunks Lane
Komoka, ON N0L 1R0

Attention: Mr. Robert Cascaden, Director of Public Works and Engineering

Reference: MN 10919 Longwoods Road, Delaware
10919 Longwoods Road Inc.
Stormwater Servicing Brief

Introduction

10919 Longwoods Road Inc. has retained LDS Consultants Inc. (LDS) to prepare a stormwater management (SWM) strategy in support of a proposed draft plan redline for a vacant land condominium development in the community of Delaware, as illustrated in **Figure 1**. The subject site comprises agricultural lands currently used as a meadow measuring approximately 6.65 hectares. The site is bound to the north by Longwoods Road, to the south and west by agricultural lands and to the east by low-density residential properties fronting Carriage Road.

Background Information

The proposed stormwater management strategy was developed using the following information presented in the following reports:

- Middlesex Centre Infrastructure Design Standards, dated January 2018;
- Stormwater Management Policy Manual of the Municipality of Middlesex Centre, prepared by Stantec Consulting Ltd., dated June 2011;
- Stormwater Management Planning and Design Manual, organized by the Ministry of the Environment, dated March 2003; and,
- Geotechnical Investigation & Preliminary Hydrogeological Assessment, prepared by LDS Consultants Inc., dated November 2023;

Design Criteria

The SWM outlet for the site is located within the Lower Thames River Watershed. Accordingly, the following SWM design criteria apply to the proposed development area:

- *Water Quantity Control* - Ensure that stormwater flows are attenuated to pre-existing rates on-site, up to the 100-year event. Outflows from the SWM facility (SWMF) will need to be restricted to the capacity of the pipe of the proposed municipal drain for up to the 25-year design storm event. Major flows must be safely conveyed via an Overland Flow Route (OLFR) to an appropriate outlet without causing damage to private property or municipal infrastructure and with minimum risk to the public.
- *Water Quality Control* - Provide quality control based on 'Enhanced' Level 1 treatment (MOE, 2003).

Existing Condition

Google Maps© shows that the site comprises agricultural lands used as a meadow. Based on the watershed sketch by Spriet Associates London Ltd., a portion of the neighbouring properties and Longwoods Road drain towards the low-lying area of the subject site. Subsequently, stormwater infiltrates the ground where a subsurface agricultural drainage system drains the water south towards a natural surface water ravine feature adjacent to the Elviage Drain, which ultimately discharges into the Thames River. Existing catchment areas are described below. The site was modelled using the

SWMHYMO hydrologic software to calculate existing peak flows summarized in **Table 1**, whereas catchment areas are illustrated in **Figure 2**. Model documentation is attached to this letter report in **Appendix B**.

Catchment 101 – This area comprises the subject property currently used for agriculture and is covered with a meadow. This area drains to a low spot visible with a review of the contours on site, and the southern portion drains to the neighbouring agricultural field.

External Catchment EX-1 – This area comprises a portion of the neighbouring agricultural field located west of the subject site, which flows towards the low spot in *Catchment 101*.

External Catchment EX-2 – This area comprises a neighbouring single-family residential property located northwest of the subject site, which flows towards the low spot in *Catchment 101*.

External Catchment EX-3 – This area comprises half the Longwoods Road right-of-way (ROW) fronting the subject property. Stormwater runoff flows towards the low spot in *Catchment 101*.

External Catchment EX-4 – This area comprises a portion of the neighbouring agricultural field located east of the subject site and a portion of the low-density residential lotting fronting Carriage Road. Stormwater runoff flows towards the low spot in *Catchment 101*.

Table 1 - Existing Runoff Peak Flows

Storm Event	Surface Runoff (m ³ /s)
2-year	0.089
5-year	0.194
10-year	0.266
25-year	0.345
50-year	0.410
100-year	0.474
250-year	0.700

LDS conducted a geotechnical investigation to determine existing soil conditions at the subject site. Generally, soils observed in the boreholes consisted of topsoil overlying natural sand and silt soils. Therefore, LDS classified the soils within the Hydrologic Soil Group B category for modelling purposes.

Proposed Condition

It is proposed to develop the site into a light industrial type development comprising eighteen (18) vacant land condominium lots. The proposed development will include paved areas and some grass-landscaped areas. The internal storm sewer will convey runoff generated by minor storm events from the external area and on-site to the proposed municipal drain. Similarly, the OLFR will convey major event-generated runoff to the dry pond, which flows to the proposed municipal drain via the orifice-restricted outlet and emergency overflow structure. The proposed catchments are described below and illustrated in **Figure 3**. External drainage catchment areas will remain as described in this report's existing conditions section. The proposed condition was modelled using SWMHYMO software to estimate post-development peak flow rates, which are included in **Appendix B**.

Catchment 201 – This catchment area comprises the developed site. This area contains the 18 proposed industrial lots, the internal street network with grassed landscaped areas and SWMF. In addition, the sewer system, dry pond and site grading will convey minor and major flows to the site's southwest corner. This catchment will accept overland flows from *Catchment EX-1*.

Quantity Control

Under proposed conditions, an on-site detention strategy controls additional runoff generated by the development to meet water quantity objectives established by the MECP (Ministry of Environment, Conservation and Parks), Spreit Associates London Ltd. and the Municipality of Middlesex Centre. This strategy comprises a combination approach of an on-site storm sewer network, a dry pond, and an orifice-controlled outlet. It is proposed to provide forty-three hundred (4300) cubic metres of storage in surface ponding and underground storm sewers and maintenance holes, with the majority contained in the dry pond for peak flow attenuation. During major storm events, ponding will occur on the

private roadway. The SWM strategy will attenuate post-development stormwater runoff flow rates for all storm events, including the 250-year storm within the storage elements described above and released through an orifice-controlled pipe outlet and emergency overflow structure connected to the proposed municipal drain. The major storm event hydrographs are included in **Appendix B**. The stage-storage-discharge relationship for the 135 mm orifice-controlled system is outlined in **Table 2**. Orifice sizing is based on the capacity constraints of the outlet drain designed by Spriet Associates London Ltd.

Table 2 - Stage-Storage-Discharge for Orifice-Controlled Outlet

Stage (m)	Total Volume (m ³)	Discharge (m ³ /s)	Comment
232.83	0	0.000	Orifice Invert
236.20	188	0.059	Bottom of Dry Pond
236.50	2700	0.087	Top of Dry Pond
236.65	4003	0.299	Site Emergency Overland Spill Point

The resulting peak flows are presented in **Table 3**.

Table 3 – Post-Development Runoff Peak Flows

Storm Event	Municipal Drain (m ³ /s)	Infiltration (m ³ /s)
2-year	0.069	0.009
5-year	0.073	0.010
10-year	0.075	0.010
25-year	0.101	0.011
50-year	0.137	0.011
100-year	0.170	0.011
250-year	0.286	0.011

All supporting calculations are included in **Appendix C**.

Quality Control

The MECP recommends that an Enhanced Level of Protection be provided. Quality control will be achieved with the use of OGS technology. The OGS device will be placed at the site's storm sewer outlet and treats up to the 50-year storm event. The OGS will be sized to achieve above 80% total suspended solids (TSS) removal. This reaches the Enhanced Level of Protection recommended by the MECP. The OGS device proposed is the ADS Model FD-8HC or approved equivalent. The OGS device will treat runoff from the entire internal road network and driveways. OGS grit loading information is attached. It is expected that the OGS unit will have to be serviced once every 20-24 months. OGS sizing calculations are included in **Appendix D**.

Operation and Maintenance

During the construction of the SWM facility, it is recommended that monitoring and inspection of the erosion and sediment controls be conducted to ensure the satisfactory performance of these measures.

Reporting of the inspection and monitoring results will be distributed to the Owner. Suppose it is found that the erosion and sediment control measures need to be fixed. Then, based on field decisions, they shall be augmented to the Owner's satisfaction.

Furthermore, it is recommended that the owner initiate a post-construction monitoring program to ensure the long-term effectiveness of the SWM facility. The post-construction monitoring program should include the following:

- Periodic inspection of the SWM control facility and other erosion control works.
- Inspect the SWM facility and its outlet after significant rainfall events (generally more than 10 mm of rainfall).
- Removal of debris that may accumulate and hinder the functioning of the SWM facility.
- Implement remedial measures, including erosion stabilization, repair of damaged vegetation and sediment removal, as required.

The frequency of the post-construction monitoring will be at the Owner's discretion. However, it is recommended that a minimum of four (seasonal) inspections be made annually.

Erosion and Sediment Control

This section describes the Erosion and Sediment Control Plan implemented before, during and immediately after construction to reduce the possibility of sediment being conveyed from the proposed construction site.

Types of Selected Erosion/Sediment Control Methods

The details and locations of the proposed temporary and longer-term erosion and sediment control measures will be identified at the detailed design stage. The construction drawings, once complete, will form a part of the sediment and erosion control plan. Proposed erosion and sediment control measures include the following:

- The Contractor will install a light-duty silt fence along the site's perimeter.
- All disturbed areas where work will not occur for 30 days or more will be stabilized following OPSS 572.
- The Contractor will perform street sweeping to remove soil deposited on adjacent right-of-way by construction traffic.

The proposed temporary erosion and sediment control measures have been selected based on the site's susceptibility to erosion, the sensitivity of the downstream environment, site slopes, and the total drainage area. The proposed measures should provide adequate erosion and sediment control for the project without additional steps. However, the site will be monitored during construction; other actions will be added if required.

Installation of Erosion Control Measures

Proposed erosion and sediment control measures are summarized in **Table 4**.

Table 4 - Erosion and Sediment Control Sequencing

Erosion and Sediment Control Measures	
Pre-Construction	Create a contact list for emergency contingency plan operations.
	As appropriate, install a silt fence around the proposed work limits and the stormwater facility.
	Install robust siltation barrier.
	Preparation of a Construction Dewatering Discharge Plan, including discharge location and temporary storage locations and identifying measures to reduce suspended solids or other treatment, if required.
Construction	Monitor water quality (turbidity) for construction dewatering discharge water discharged at the surface.
	Regularly inspect erosion and sediment control measures to confirm they are practical and operating as intended.
	Monitor weather reports for significant precipitation events for contingency planning.
	Install filter cloth in on-site catch basins.
	Perform street sweeping as necessary to remove accumulated sediment from the adjacent right-of-way.
	Complete final paving.
	Complete final landscaping and vegetation plantings.
Post-Construction	Remove robust siltation barrier.
	Remove the silt fence from the proposed work limits.
	Remove filter cloth from on-site catch basins.
	Remove the construction fence from the proposed work limits.

The proposed erosion and sediment control measures have been designed according to the site slopes, drainage area, and the risks and consequences of failure. Based on these factors, additional steps will likely be optional.

However, the site will be monitored during construction, and additional measures (i.e., additional rows of silt fence) may be installed at the discretion of the Contract Administrator. Although this is not an exhaustive list, inspections should include checks on siltation barriers to confirm it is properly installed and secured, including a review for evidence of damage, tears, overtopping or undermining; checking the condition of surface water ponding areas and storm drain inlets; and documenting areas where seeding/sodding/mulching is implemented to re-establish vegetative cover. In addition, due to the high groundwater condition, inspections shall include checking exposed banks for seepage. If seepage is encountered, erosion control blankets shall be installed to mitigate any damage to the banks.

The triggers for installing enhanced erosion and sediment control measures would include breaching the proposed erosion and sediment control measures and re-evaluation based on site conditions during construction. As described below, site conditions and the proposed erosion and sediment control measures will be monitored regularly.

Inspection Requirements

The effectiveness of the erosion and sediment control measures will need to be monitored during site grading and site servicing work. This will require frequent inspections. Therefore, the following minimum inspection intervals are recommended:

- The Contractor and Contract Administrator shall monitor weather reports daily and record temperatures and rainfall. When rainfall is anticipated, the Contractor and the Contract Administrator shall inspect the erosion control works immediately before and immediately after the rainfall event and snowmelt event (timing for inspections is based on predicted weather forecasts);
- Daily during extended or significant precipitation (i.e., rainfall amounts that exceed 25 millimetres) or during significant snowmelt periods;
- Daily during any construction activity that would potentially yield significant runoff volumes or otherwise impact the quality of the runoff leaving the site;
- Daily while deficiencies are present which fail to contain, filter or otherwise treat runoff or contribute to sediment loading in surface water;
- Weekly during dry periods while construction activity is occurring at the site. The Contractor and the Contract Administrator shall inspect the erosion control measures the day before the last business day of the week (typically Thursday) to allow any work to be completed on damaged erosion control works before the weekend.; and,
- Monthly during inactive periods (> 30 days).

The Contract Administrator will document all inspection activities in weekly erosion and sediment control reports.

The Contractor shall construct and maintain all erosion and sediment control measures. This shall include but not be limited to preserving fencing and removing accumulated sediment. Temporary erosion and sediment control measures will not be removed until the areas they serve are restored and stable. The builder will remove the erosion and sediment control measures after the sod has been rooted on the site.

Contingency Plan

The contingency plan aims to help minimize the risk or consequence of a failure of the erosion and sediment control works. Failure could result from insufficient measures, lack of maintenance, or severe weather conditions. The contingency plan includes two areas of consideration:

- Procedures that will be followed where a failure has occurred; and
- Contingency measures will be implemented where there is potential for loss.

The Contractor shall be responsible for following the contingency plan and will prepare the following items:

- The Contractor will maintain a contact list for emergencies.
- Workers shall be on call for emergencies for all aspects of the emergency, from design to installation of sediment and erosion control measures. Any associated health and safety issues are the responsibility of the Contractor.
- Sediment and erosion control measures such as erosion control blanket, straw bales and stakes, sandbags, and silt fences shall be available for emergency installation.

- Gas-powered pumps, appropriately sized hoses, filtration hose socks, and filter cloth will be available for emergency dewatering.
- Heavy equipment shall be on standby for emergency works.
- A supplemental contact list for any required equipment or materials shall be prepared and available for emergencies.

Monitoring

As noted previously, regular monitoring of the site's erosion and sediment control measures makes up an integral part of the contingency plan by providing an early indication should environmental control measures (such as sediment and erosion control measures) or practices fail to achieve prescribed standards. Recommended inspection intervals were discussed previously.

If monitoring identifies a high potential for failure, steps will be taken to reduce the risk. These measures may include repairing existing efforts, modifying current measures, and adding new measures.

If unforeseen events cause the strategies set out in the contingency plan to be insufficient or inappropriate to meet the objective of containing sediment within the working limits, the Contractor, either independently or as directed by the Contract Administrator, will respond promptly with all reasonable measures to prevent, counteract, or remedy any effects on aquatic habitat, and human interest (i.e., public safety, property value).

Updates to the Erosion and Sediment Control Plan may be required to reflect changes at the site during various stages of construction. The municipality will be circulated with updated plans to ensure they have the most current techniques available for review and consultation.

Severe Weather Anticipated

In cases where the weather forecast indicates that significant rainfall is expected within 24 hours, the Contractor shall immediately complete the following:

- Inspect existing erosion and sediment control measures to confirm that they are secure and in good working order;
- Review site conditions to identify and protect areas of exposed soil that could be susceptible to surface erosion; and,
- Monitor all measures during the rainfall event and take corrective action where a potential for failure is identified.

The Contract Administrator shall document the status of the above-listed steps.

Responding to Failures

The Contractor will cease all construction-related work and focus on erosion and sediment control as required to stabilize the site where a failure has occurred or is imminent. The work shall be completed to the satisfaction of the Contract Administrator and any regulatory agencies having jurisdiction.

Any unexpected discharge of silt, sediment, or other deleterious substance shall be reported to the Municipality of Middlesex Centre within 24 hours. The Contractor is responsible for advising the contract administrator and promptly notifying the incident to the Spills Action Centre. Depending on the type of incident, water sampling and quality testing may be warranted to document the extent of the impact. Scoping for the required testing will depend on the incident report.

The Owner's Engineer will develop a restoration plan if significant long-term damage to aquatic habitat or property is suspected. Consultation with an ecologist and biologist may be required to confirm that the remedial measures are appropriate. Development of the initial restoration plan will begin within 24 hours of discovering sediment discharge. It will be implemented immediately following consultation and approval from the MECP, Lower Thames River Conservation Authority (UTRCA), and Municipality of Middlesex Centre. The plan will address the following:

- Removal and disposal of sediment deposited outside of the work limits; and
- Restoration of any areas disturbed through deposition or removal.

Reporting Schedule

The Contract Administrator shall prepare weekly erosion and sediment control monitoring reports/summaries for the duration of site grading and site servicing and submit them to the Municipality of Thames Center by April 1, July 1, and November 1 of each year until all works and services included in the plan are assumed.

The monitoring reports should document the status of the ESC Plan, any repairs, rainfall or pumping that has occurred since the last report, and any risks of failure that may be present.

Additionally, any failure of erosion and sediment control measures shall be reported as described in the contingency plan.

Construction Dewatering Requirements

Based on the Geotechnical Investigation prepared by LDS, shallow groundwater conditions are observed throughout the site. Therefore, where minor groundwater infiltration occurs within open excavations during construction, conventional sump pumping techniques are expected to be suitable for groundwater control.

Sediment controls should be incorporated into the construction of dewatering discharge outlets. These may be silt bags, constructed sediment traps, or other discharge water filtering methods. The Contractor will be responsible for regular maintenance, including sediment removal. Under no circumstances will dewatering effluent be discharged directly to the receiving watercourse without incorporating suitable measures to prevent sediment discharge or cause erosion or scouring at the waterway. Both the Contractor and the Contract Administrator will be responsible for monitoring the water quality leaving the site.

As an introductory guide, the water discharged at the site should have a turbidity level within 8 NTU of the background levels within the watercourse/municipal drain.

For construction dewatering efforts involving a sizeable daily pumping volume, additional sediment control or filtration measures, such as settlement tanks, may be implemented as part of the construction dewatering plan. The discharge and associated sediment controls will depend on the scope of work and the location of the excavation to be dewatered. Thus, the Owner's Engineer should review the dewatering plan in consultation with the Contractor and the Contract Administrator.

For projects requiring positive groundwater control with a removal rate of 50,000 to 400,000 litres per day, a submission to the Environmental Activity and Sector Registry (EASR) will be required. For construction dewatering activities with volumes over 400,000 litres per day, a Category 3 Permit to Take Water (PTTW) would be necessary for groundwater control. EASR submissions and PTTW applications are submitted to and approved by MECP according to Sections 34 and 98 of the Ontario Water Resources Act R.S.O. 1990 and Water Taking and Transfer Regulation O. Reg. 387/04.

The supporting documents to support an EASR submission or PTTW application should include calculations for the zone of influence and identify potential qualitative and quantitative impacts on the shallow groundwater table. Details regarding volume monitoring, water quality analyses and method/location of discharge water will also be required for either submission type. In addition, impacts on local natural features will need to be assessed considering the proposed construction dewatering plan.

Conclusion and Recommendations

The analysis completed by LDS yields the following conclusions:

- Post-development peak flow rates are attenuated to less than existing flow rates into the proposed municipal drain;
- Post-development peak flow rates are attenuated to less than the capacity of the pipe of the proposed municipal drain for up-to-the 25-year design storm event;
- Surface storage contained within the dry pond will be used to attenuate peak runoff flows;
- Surface runoff from all road and driveway surfaces is treated with an OGS device; and,
- Sediment transport from the site during construction will be minimized by implementing appropriate ESC measures.

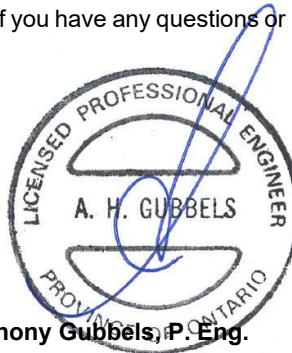
We trust this submission will meet with your approval. However, if you have any questions or require further information, please do not hesitate to contact the undersigned.

Respectfully,

LDS CONSULTANTS INC.



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Water Resources
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C: 519.859.5942
luke.jesson@LDSconsultants.ca

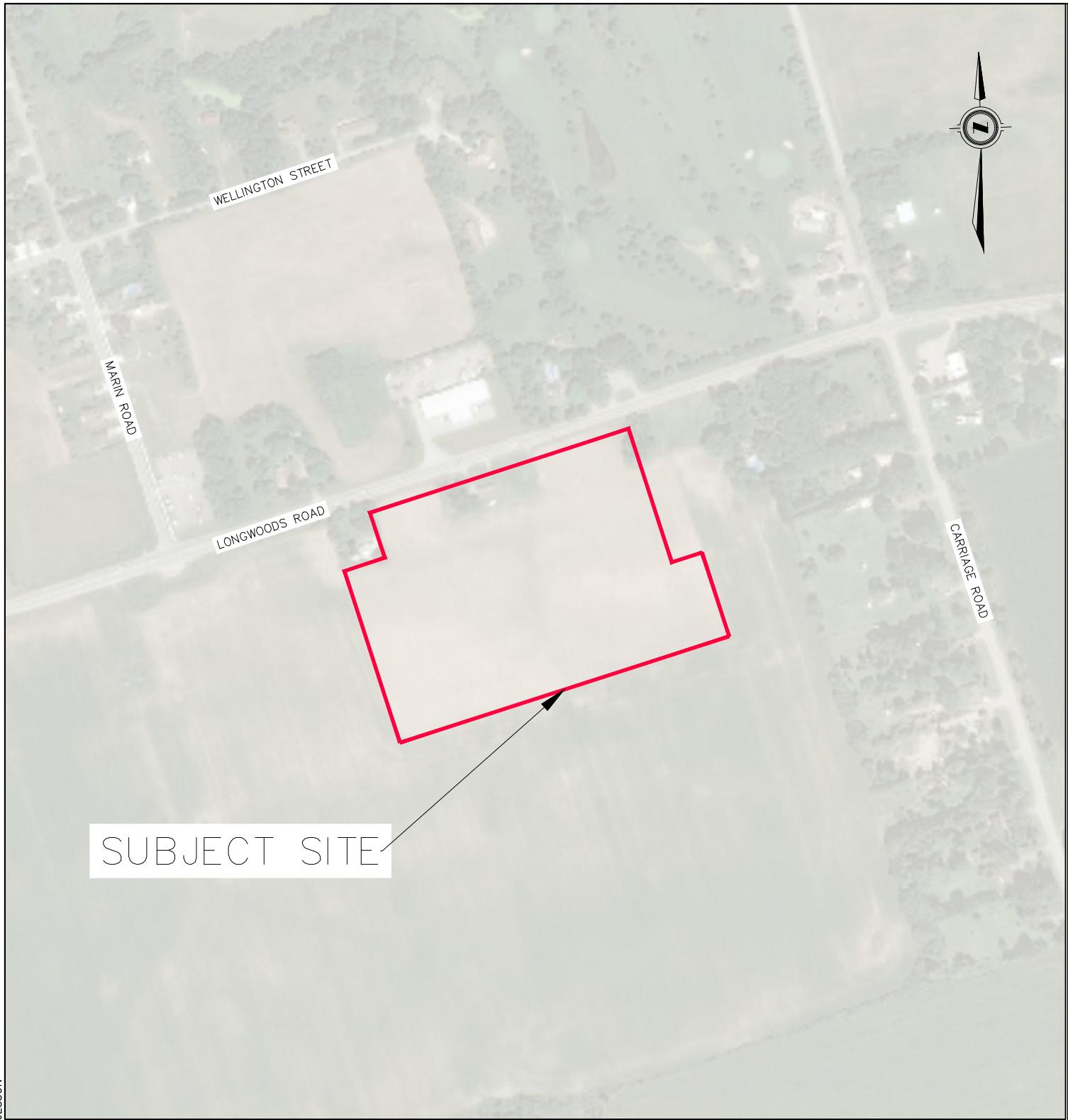


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anthony.gubbels@LDSConsultants.ca

Attachments:

- Appendix A – FIGURES
- Appendix B – SWMHYMO HYDROLOGIC MODEL
- Appendix C – SUPPORTING CALCULATIONS
- Appendix D – OGS SIZING SHEET

APPENDIX A
FIGURES



LDS

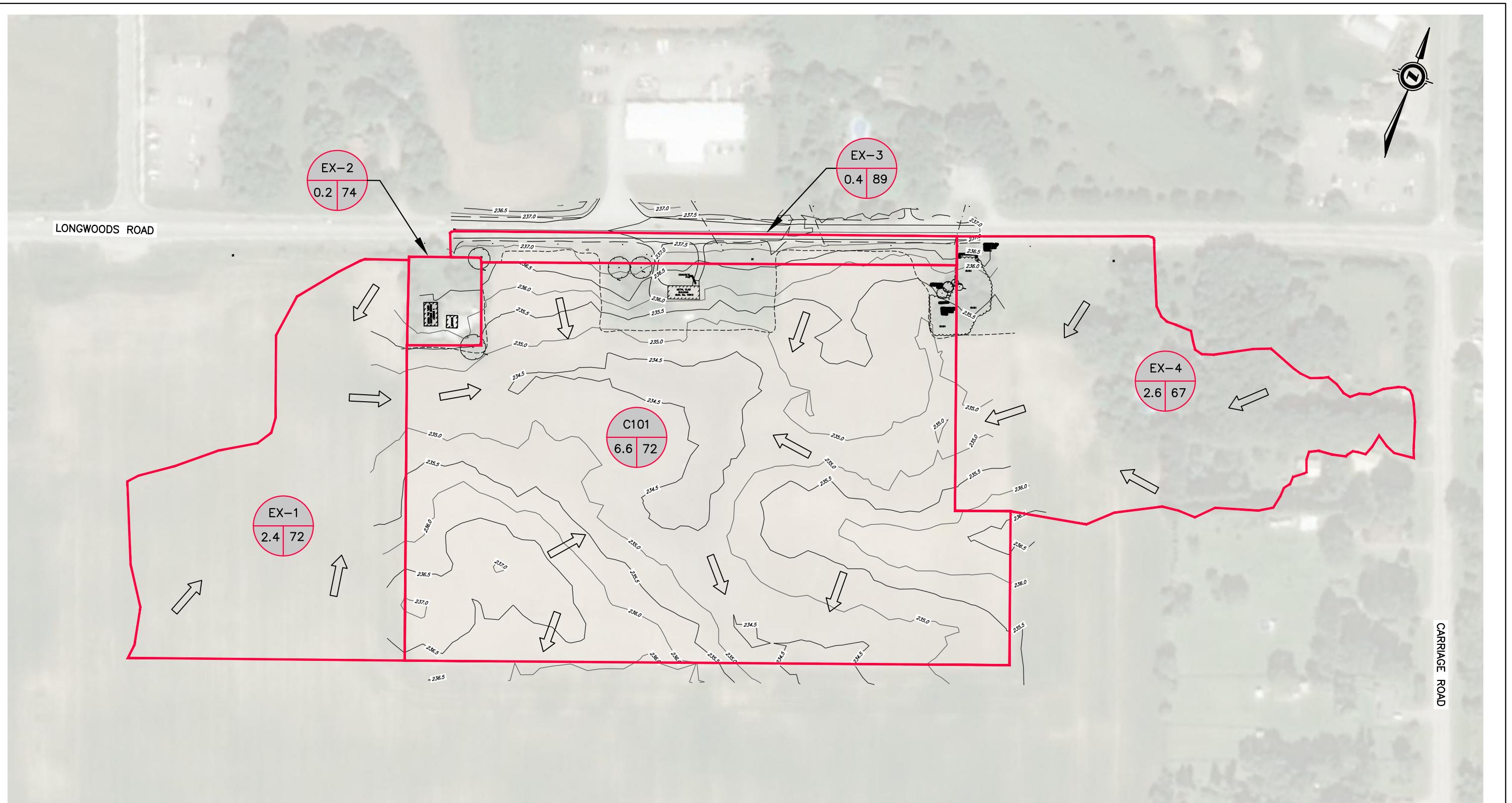
10919 LONGWOODS ROAD LIGHT INDUSTRIAL
10919 LONGWOODS ROAD INC.

LOCATION PLAN

PROJECT: LD-00318

SCALE: N.T.S.

FIGURE 1



LEGEND:

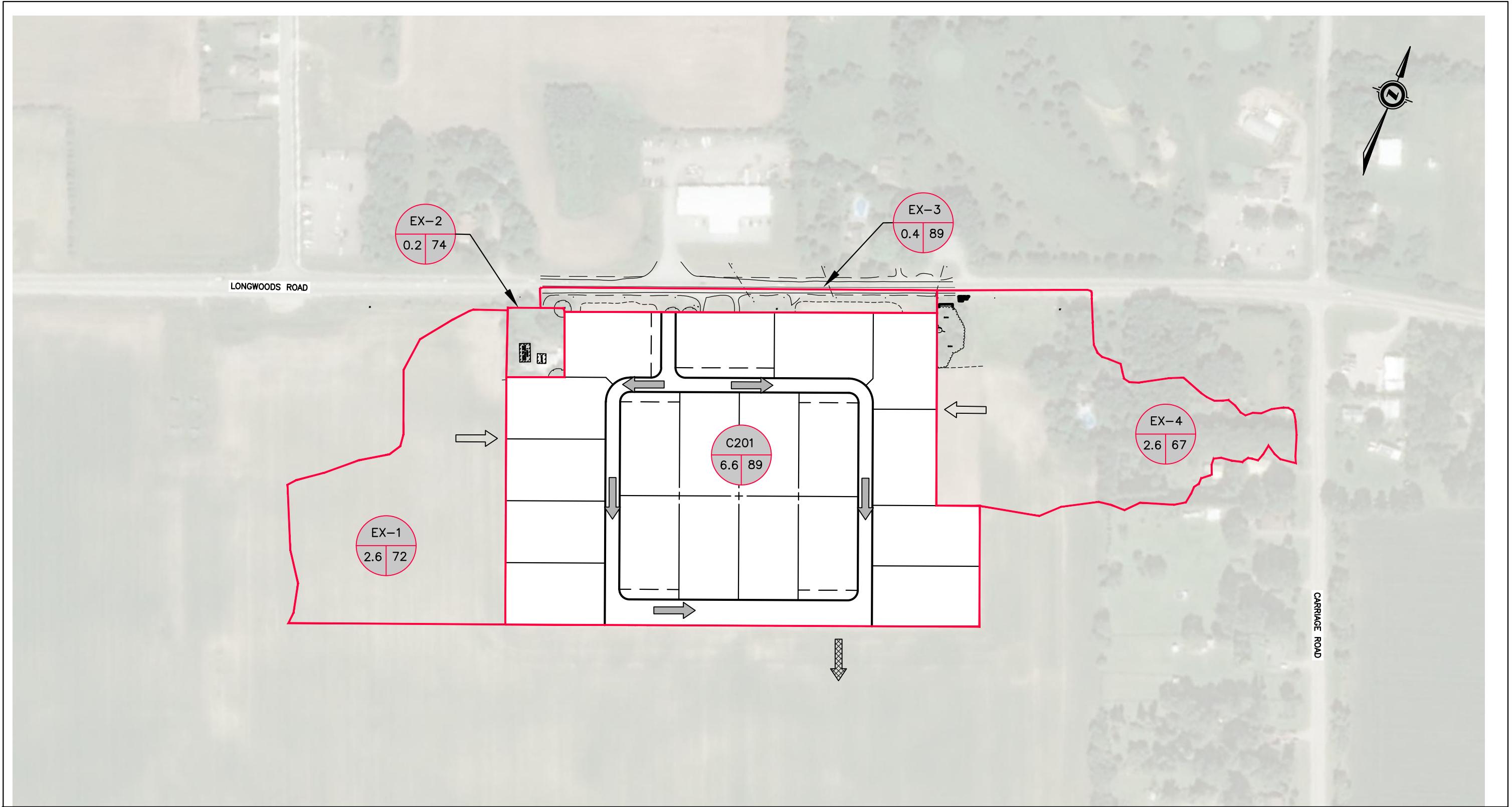
EXISTING CATCHMENT AREA		STORM DRAINAGE AREA DATA:	
		CATCHMENT ID	
	EXISTING CATCHMENT AREA	C101	
	EXISTING OVERLAND FLOW PATH	1.46	82
		AREA (ha)	CURVE NUMBER

LDS

10919 LONGWOODS ROAD LIGHT INDUSTRIAL
10919 LONGWOODS ROAD INC.

EXISTING CONDITIONS DRAINAGE AREA PLAN

PROJECT: LD-00318 SCALE: N.T.S. FIGURE 2



LEGEND:

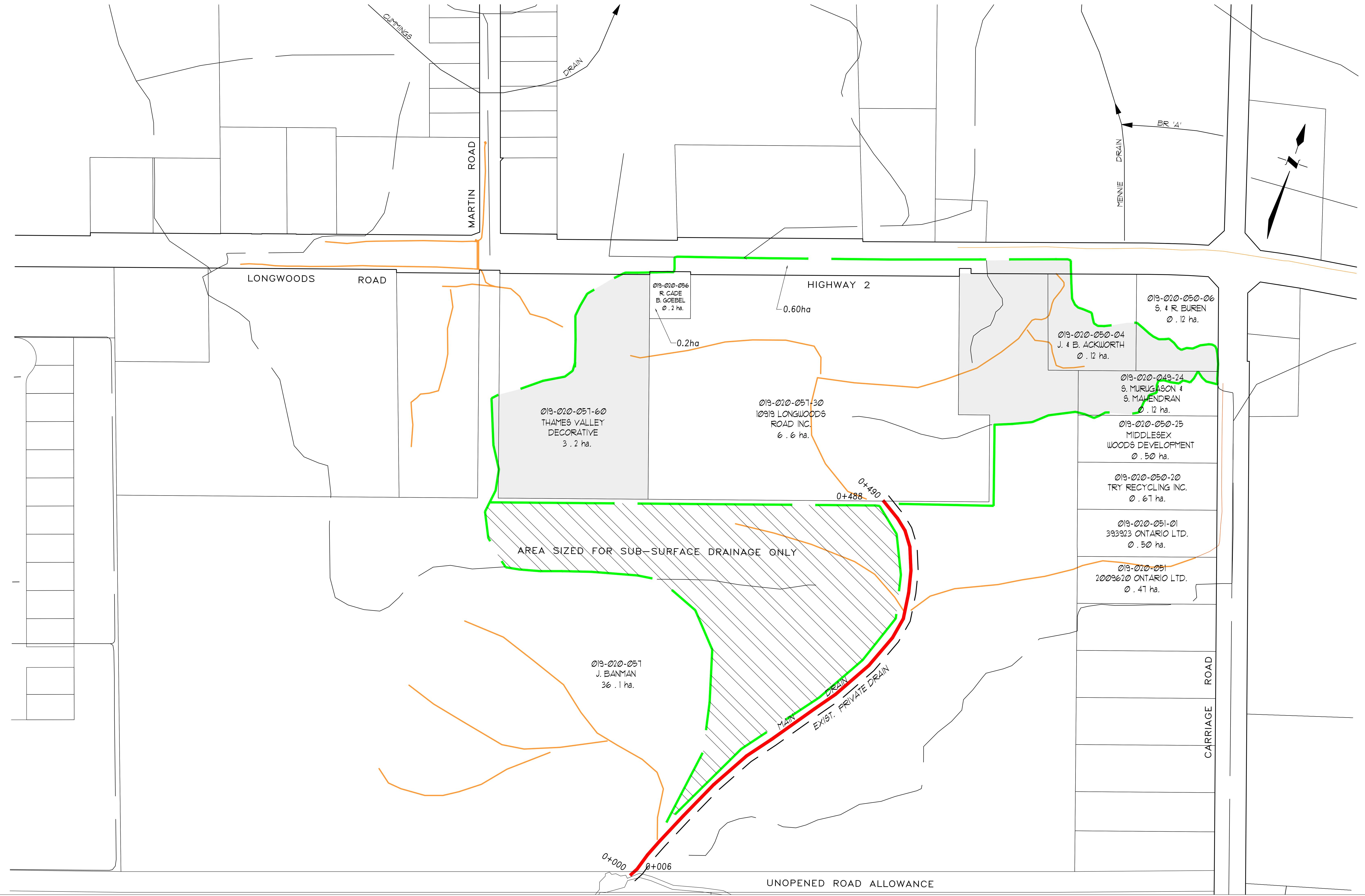
	PROPOSED CATCHMENT AREA	STORM DRAINAGE AREA DATA:	
	PROPOSED OVERLAND FLOW ROUTE	CATCHMENT ID	
	ULTIMATE OVERLAND FLOW ROUTE	AREA (ha)	CURVE NUMBER

LDS

10919 LONGWOODS ROAD LIGHT INDUSTRIAL
10919 LONGWOODS ROAD INC.

POST-DEVELOPMENT DRAINAGE AREA PLAN

PROJECT: LD-00318 SCALE: N.T.S. FIGURE 3



APPENDIX B

SWMHYMO HYDROLOGIC MODEL

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00001> =====
00002> =====
00003> SSSSS W W M M H H Y Y M M OOO 999 999 =====
00004> S W W W MM MM H H Y Y MM MM O O # 9 9 9 9 Ver 4.05
00005> SSSSS W W M M M M HHHHH Y M M O O # 9 9 9 9 Ver 4.05
00006> S W W M M H H Y M M O O 9999 9999 Sept 2011
00007> SSSSS W W M M H H Y M M O O 9 9 9 9 =====
00008> 9 9 9 9 # 4058874
00009> StormWater Management Hydrologic Model 999 999 =====
0010>
0011> **** SWMMHYO Version 4.05 ****
0012> **** A single event and continuous hydrologic simulation model ****
0013> **** based on the principles of HYMO and its successors ****
0014> **** OTTHYMO-83 and OTTHYMO-89. ****
0015> ****
0016> **** Distributed by: J.F. Sabourin and Associates Inc.
0017> Ottawa, Ontario: (613) 836-3884
0018> Gatineau, Québec: (819) 243-6858
0019> E-Mail: swmhmo@fsa.com
0020>
0021> ****
0022>
0023> **** Licensed user: Land Development Solutions ****
0024> London SERIAL# 4058874 ****
0025> ****
0026> ****
0027> ****
0028> ****
0029> **** PROGRAM ARRAY DIMENSIONS ****
0030> **** Maximum value of ID numbers : 10 ****
0031> **** Max. number of rainfall points: 105408 ****
0032> **** Max. number of flow points : 105408 ****
0033> ****
0034>
0035>
0036> ***** D E T A I L E D O U T P U T *****
0037> **** DATE: 2023-11-21 TIME: 14:53:34 RUN COUNTER: 000760 ****
0038> * Input filename: C:\SWMHMO\1\LD-00318\211123.dat
0041> * Output filename: C:\SWMHMO\1\LD-00318\211123.out
0042> * Binary filename: C:\SWMHMO\1\LD-00318\211123.sum
0043> * User comments:
0044> * 1:
0045> * 2:
0046> * 3:
0047> ****
0048>
0049>
0050> 001:0001
0051>
0052> ## Project Name:[LONGWOODS INDUSTRIAL VLC, DELAWARE] Project Number:[LD-00318]
0053> ## Date 20-11-2023
0054> ## Modeler : [LJ]
0055> ## Company : LDS Consultants Inc.
0056> ## License # : 4058874
0057> ****
0058>
0059> | START | Project dir. C:\SWMHMO\1\LD-00318\
0060> ----- Rainfall dir. C:\SWMHMO\1\LD-00318\
0061> TZERO = .00 hrs on 0
0062> METRIC= 2 (output = METRIC)
0063> NRUN = 000
0064> NSTORM= 0
0065>
0066> 001:0002
0067> *#####
0068> #
0069> # 2-year
0070> #=====
0071> #=====
0072> #*****
0073> CHICAGO STORM | IDF curve parameters: A= 724.690
0074> | Pttotal= 33.31 mm |
0075> TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
0076> hrs mm/hr hrs mm/hr hrs mm/hr hrs mm/hr
0077> .08 2.718 | .83 15.099 | 1.59 9.604 | 2.33 3.537
0078> .17 2.063 | .92 35.585 | 1.67 6.700 | 2.42 3.650
0079> .25 3.263 | 1.00 110.459 | 1.75 5.997 | 2.50 3.184
0080> .33 3.638 | 1.08 45.982 | 1.83 5.435 | 2.58 3.034
0081> .42 4.124 | 1.17 25.234 | 1.92 4.976 | 2.67 2.899
0082> .50 4.778 | 1.25 17.203 | 2.00 4.593 | 2.75 2.777
0083> .58 5.709 | 1.33 13.032 | 2.08 4.268 | 2.83 2.666
0084> .67 7.143 | 1.42 10.502 | 2.17 3.990 | 2.92 2.564
0085> .75 9.644 | 1.50 8.812 | 2.25 3.749 | 3.00 2.470
0086>
0087>
0088> 001:0003
0089> ######
0090> # EXISTING CONDITIONS
0091> #=====
0092> #*****
0093> CALIB NASHYD | Area (ha)= 2.37 Curve Number (CN)=72.00
0094> | 01:EX-1 DT= 1.00 | Ia (mm)= 8.000 # of Linear Res.(N)= 3.00
0095> | U.H. Tp(hrs)= .330
0096> Unit Hyd Qpeak (cms)= .274
0097> PEAK FLOW (cms)= .027 (i)
0098> TIME TO PEAK (hrs)= 1.517
0099> RUNOFF VOLUME (mm)= 5.161
0100> TOTAL RAINFALL (mm)= 33.307
0101> RUNOFF COEFFICIENT = .155
0102>
0103> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
0104>
0105>
0106>
0107> 001:0004
0108>
0109> COMPUTE DUALHYD | Average inlet capacities [CINLET] = .001 (cms)
0110> | TotalHyd 01:EX-1 | Number of inlets in system [NINLET] = 1
0111> | | Total minor system capacity = .001 (cms)
0112> | | Total major system storage [TMJSTO] = 99999. (cu.m.)
0113>
0114> ID: NYHD AREA QPEAK TPEAK R.V. DWF
0115> | NYHD (ha) (cms) (hrs) (mm) (cms)
0116> TOTAL HYD. 01:EX-1 2.37 .027 1.517 5.161 .000
0117>
0118> MAJOR SYST 02:THMDS .00 .000 .000 .000 .000
0119> MINOR SYST 03:toDRAIN 2.37 .001 43.450 5.162 .000
0120>
0121> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
0122>
0123> Maximum MAJOR SYSTEM storage used = 114. (cu.m.)
0124>
0125>
0126>
0127>
0128>
0129> COMPUTE DUALHYD | Average inlet capacities [CINLET] = .001 (cms)
0130> | TotalHyd 01:EX-1 | Number of inlets in system [NINLET] = 1
0131> | | Total minor system capacity = .001 (cms)
0132> | | Total major system storage [TMJSTO] = 99999. (cu.m.)
0133>
0134> ID: NYHD AREA QPEAK TPEAK R.V. DWF
0135> | NYHD (ha) (cms) (hrs) (mm) (cms)
0136> TOTAL HYD. 01:EX-1 2.37 .027 1.517 5.161 .000
0137> 001:0005
0138>
0139> | CALIB NASHYD | Area (ha)= .19 Curve Number (CN)=74.00
0140> | 01:EX-2 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res.(N)= 3.00
0141> | U.H. Tp(hrs)= .090
0142> Unit Hyd Qpeak (cms)= .081
0143> PEAK FLOW (cms)= .006 (i)
0144> TIME TO PEAK (hrs)= 1.117
0145> RUNOFF VOLUME (mm)= 6.816
0146> TOTAL RAINFALL (mm)= 33.307
0147> RUNOFF COEFFICIENT = .205
0148>
0149>
0150>
0151> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
0152>
0153> 001:0006
0154>
0155> | CALIB STANDHYD | Area (ha)= .45
0156> | 04:EX-3 DT= 1.00 | Total Imp(%)= 65.00 Dir. Conn.(%)= 1.00
0157> | U.H. Tp(hrs)= .230
0158>
0159> IMPERVIOUS PVIOUS (i)
0160> Surface Area (ha)= .29 .16
0161> Dep. Storage (mm)= 2.00 8.00
0162> Average Slope (%)= 1.00 20.00
0163> Length (m)= 5.00 25.00
0164> Mannings n = .013 .240
0165>
0166> Max.eff. Int.(mm/hr)= 110.46 135.03
0167> Tp(hrs) over (min)= 1.00 3.00
0168> Storage Coeff. (min)= .41 (ii) 2.72 (ii)
0169> Unit Hyd. Tpeak (min)= 1.00 3.00
0170> Unit Hyd. peak (cms)= 1.55 .40
0171>
0172> *TOTALS*
0173> PEAK FLOW (cms)= .00 .04 .045 (iii)
0174> TIME TO PEAK (hrs)= 1.00 1.02 1.017
0175> RUNOFF VOLUME (mm)= 31.31 14.20 14.375
0176> TOTAL RAINFALL (mm)= 33.31 33.31 33.307
0177> RUNOFF COEFFICIENT = .94 .43 .432
0178>
0179> (i) CN PROCEDURE SELECTED FOR PVIOUS LOSSES:
0180> CN* = 72.0 Ia = Dep. Storage (Above)
0181> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
0182> THAN THE STORAGE COEFFICIENT.
0183> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
0184>
0185> 001:0007
0186>
0187> | CALIB NASHYD | Area (ha)= 2.59 Curve Number (CN)=67.00
0188> | 05:EX-4 DT= 1.00 | Ia (mm)= 8.000 # of Linear Res.(N)= 3.00
0189> | U.H. Tp(hrs)= .230
0190>
0191> Unit Hyd Qpeak (cms)= .430
0192>
0193> PEAK FLOW (cms)= .029 (i)
0194> TIME TO PEAK (hrs)= 1.367
0195> RUNOFF VOLUME (mm)= 4.258
0196> TOTAL RAINFALL (mm)= 33.307
0197> RUNOFF COEFFICIENT = .128
0198>
0199> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
0200>
0201>
0202> 001:0008
0203>
0204> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .001 (cms)
0205> | TotalHyd 05:EX-4 | Number of inlets in system [NINLET] = 1
0206> | | Total minor system capacity = .001 (cms)
0207> | | Total major system storage [TMJSTO] = 99999. (cu.m.)
0208>
0209> ID: NYHD AREA QPEAK TPEAK R.V. DWF
0210> | NYHD (ha) (cms) (hrs) (mm) (cms)
0211> TOTAL HYD. 05:EX-4 2.59 .029 1.367 4.258 .000
0212>
0213> MAJOR SYST 06:BANNAN .00 .000 .000 .000 .000
0214> MINOR SYST 07:toDRAIN 2.59 .001 39.250 4.258 .000
0215>
0216> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
0217>
0218> Maximum MAJOR SYSTEM storage used = 102. (cu.m.)
0219>
0220>
0221> 001:0009
0222>
0223> | CALIB NASHYD | Area (ha)= 6.64 Curve Number (CN)=72.00
0224> | 05:CO10 DT= 1.00 | Ia (mm)= 8.000 # of Linear Res.(N)= 3.00
0225> | U.H. Tp(hrs)= .310
0226>
0227> Unit Hyd Qpeak (cms)= .818
0228>
0229> PEAK FLOW (cms)= .077 (i)
0230> TIME TO PEAK (hrs)= 1.483
0231> RUNOFF VOLUME (mm)= 5.161
0232> TOTAL RAINFALL (mm)= 33.307
0233> RUNOFF COEFFICIENT = .155
0234>
0235> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
0236>
0237>
0238> 001:0010
0239>
0240> | ADD HYD (PRE ) ID: NYHD AREA QPEAK TPEAK R.V. DWF
0241> | ID1 01:EX-2 .19 .006 1.12 6.82 .000
0242> | +ID2 03:toDRAIN 2.37 .001 4.45 5.16 .000
0243> | +ID3 04:EX-3 2.37 .001 4.45 5.16 .000
0244> | +ID4 05:CO10 6.64 .077 1.48 5.16 .000
0245> | +ID5 07:toDRAIN 2.59 .001 39.25 4.26 .000
0246> |
0247> SUM 08:PRE 12.24 .089 1.45 5.33 .000
0248>
0249>
0250> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
0251>
0252>
0253> 001:0011
0254> #####
0255> # PROPOSED CONDITIONS
0256> # =====
0257> # =====
0258> # =====
0259>
0260> | CALIB NASHYD | Area (ha)= 2.37 Curve Number (CN)=72.00
0261> | 01:EX-1 DT= 1.00 | Ia (mm)= 8.000 # of Linear Res.(N)= 3.00
0262> | U.H. Tp(hrs)= .330
0263>
0264> Unit Hyd Qpeak (cms)= .274
0265>
0266> PEAK FLOW (cms)= .027 (i)
0267> TIME TO PEAK (hrs)= 1.517
0268> RUNOFF VOLUME (mm)= 5.161
0269> TOTAL RAINFALL (mm)= 33.307
0270> RUNOFF COEFFICIENT = .155

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00271> 00272> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
 00273>
 00274>-----
 00275> 001:0012-----
 00276>-----
 00277> | COMPUTE_DUALHYD | Average inlet capacities [CINLET] = .001 (cms)
 00278> | TotalHyd 01:EX-1 | Number of inlets in system [NINLET] = 1
 00279>----- Total minor system capacity = .001 (cms)
 00280>----- Total major system storage [TMJSTO] = 99999. (cu.m.)
 00281>
 00282> ID: NYHD AREA QPEAK TPEAK R.V. DWF
 00283> (ha) (cms) (hrs) (mm) (cms)
 00284> TOTAL HYD. 01:EX-1 2.37 .027 1.517 5.161 .000
 00285>=====
 00286> MAJOR SYST 02:THAMES .00 .000 .000 .000 .000
 00287> MINOR SYST 03:tdRAI 2.37 .001 43.450 5.162 .000
 00288>
 00289> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
 00290>
 00291> Maximum MAJOR SYSTEM storage used = 114. (cu.m.)
 00292>
 00293>-----
 00294> 001:0013-----
 00295>-----
 00296> | CALIB_NASHYD | Area (ha)= .19 Curve Number (CN)=74.00
 00297> | 01:EX-2 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res.(N)= 3.00
 00298>----- U.H. Tp(hrs)= .090
 00299>
 00300> Unit Hyd Ppeak (cms)= .081
 00301>
 00302> PEAK FLOW (cms)= .006 (i)
 00303> TIME TO PEAK (hrs)= 1.117
 00304> RUNOFF VOLUME (mm)= 6.816
 00305> TOTAL RAINFALL (mm)= 33.307
 00306> RUNOFF COEFFICIENT = .205
 00307> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
 00308>
 00309>
 00310>
 00311> 001:0014-----
 00312>-----
 00313> | CALIB_STANDHYD | Area (ha)= .45
 00314> | 04:EX-3 DT= 1.00 | Total Imp(%)= 65.00 Dir. Conn. (%)= 1.00
 00315>
 00316> IMPERVIOUS PEROVIOUS (i)
 00317> Surface Area (ha)= .29 .16
 00318> Dep. Storage (mm)= 2.00 8.00
 00319> Average Slope (%)= 1.00 20.00
 00320> Length (m)= 5.00 25.00
 00321> Mannings n = .013 .240
 00322>
 00323> Max.eff.Inten.(mm/hr)= 110.46 135.03
 00324> over (min)= 1.00 3.00
 00325> Storage Coeff. (min)= .41 (ii) 2.72 (ii)
 00326> Unit Hyd. Tpeak (min)= 1.00 3.00
 00327> Unit Hyd. peak (cms)= 1.55 .40
 00328>
 00329> PEAK FLOW (cms)= .00 .04 .045 (iii)
 00330> TIME TO PEAK (hrs)= 1.00 1.02 1.017
 00331> RUNOFF VOLUME (mm)= 31.31 14.20 14.375
 00332> TOTAL RAINFALL (mm)= 33.31 33.31 33.307
 00333> RUNOFF COEFFICIENT = .94 .43 .432
 00334>
 00335> (i) CN PROCEDURE SELECTED FOR PREVIOUS LOSSES:
 00336> CN* = 72.0 Ia = Dep. Storage (Above)
 00337> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 00338> THAN THE STORAGE COEFFICIENT.
 00339> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
 00340>
 00341>-----
 00342> 001:0015-----
 00343>-----
 00344> | CALIB_NASHYD | Area (ha)= 2.59 Curve Number (CN)=67.00
 00345> | 05:EX-4 DT= 1.00 | Ia (mm)= 8.000 # of Linear Res.(N)= 3.00
 00346>----- U.H. Tp(hrs)= .230
 00347>
 00348> Unit Hyd Ppeak (cms)= .430
 00349>
 00350> PEAK FLOW (cms)= .029 (i)
 00351> TIME TO PEAK (hrs)= 1.367
 00352> RUNOFF VOLUME (mm)= 4.258
 00353> TOTAL RAINFALL (mm)= 33.307
 00354> RUNOFF COEFFICIENT = .128
 00355>
 00356> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
 00357>
 00358>
 00359> 001:0016-----
 00360>-----
 00361> | COMPUTE_DUALHYD | Average inlet capacities [CINLET] = .001 (cms)
 00362> | TotalHyd 05:EX-4 | Number of inlets in system [NINLET] = 1
 00363>----- Total minor system capacity = .001 (cms)
 00364>----- Total major system storage [TMJSTO] = 99999. (cu.m.)
 00365>
 00366> ID: NYHD AREA QPEAK TPEAK R.V. DWF
 00367> (ha) (cms) (hrs) (mm) (cms)
 00368> TOTAL HYD. 05:EX-4 2.59 .029 1.367 4.258 .000
 00369>=====
 00370> MAJOR SYST 06:BANNAN .00 .000 .000 .000 .000
 00371> MINOR SYST 07:tdRAI 2.59 .001 39.250 4.258 .000
 00372>
 00373> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
 00374>
 00375> Maximum MAJOR SYSTEM storage used = 102. (cu.m.)
 00376>
 00377>
 00378> 001:0017-----
 00379>
 00380> | CALIB_STANDHYD | Area (ha)= 6.64
 00381> | 05:C201 DT= 1.00 | Total Imp(%)= 90.00 Dir. Conn. (%)= 80.00
 00382>
 00383> IMPERVIOUS PEROVIOUS (i)
 00384> Surface Area (ha)= 5.98 .66
 00385> Dep. Storage (mm)= 2.00 5.00
 00386> Average Slope (%)= 1.00 2.00
 00387> Length (m)= 50.00 25.00
 00388> Mannings n = .013 .250
 00389>
 00390> Max.eff.Inten.(mm/hr)= 110.46 36.87
 00391> over (min)= 2.00 10.00
 00392> Storage Coeff. (min)= 1.62 (ii) 9.55 (ii)
 00393> Unit Hyd. Tpeak (min)= 2.00 10.00
 00394> Unit Hyd. peak (cms)= .64 .12
 00395>
 00396> PEAK FLOW (cms)= 1.55 .04 1.565 (iii)
 00397> TIME TO PEAK (hrs)= 1.00 1.18 1.000
 00398> RUNOFF VOLUME (mm)= 31.31 8.47 26.740
 00399> TOTAL RAINFALL (mm)= 33.31 33.31 33.307
 00400> RUNOFF COEFFICIENT = .94 .25 .803
 00401>
 00402> (i) CN PROCEDURE SELECTED FOR PREVIOUS LOSSES:
 00403> CN* = 61.0 Ia = Dep. Storage (Above)
 00404> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 00405> THAN THE STORAGE COEFFICIENT.

00406> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
 00407>
 00408>
 00409> 001:0018-----
 00410> | ADD HYD (POST) | ID: NYHD AREA QPEAK TPEAK R.V. DWF
 00411> (ha) (cms) (hrs) (mm) (cms)
 00412> ID1 01:EX-2 .19 .006 1.12 6.82 .000
 00413> +ID2 03:tdRAI 2.37 .001 40.45 5.16 .000
 00414> +ID3 04:EX-3 .45 .045 1.02 14.38 .000
 00415> +ID4 05:C201 6.64 1.565 1.00 26.74 .000
 00416> +ID5 07:tdRAI 2.59 .001 39.25 4.26 .000
 00417>
 00418> =====
 00419> SUM 09:POST 12.24 1.610 1.00 17.04 .000
 00420>
 00421> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
 00422>
 00423>
 00424> 001:0019-----
 00425> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
 00426> | IN:09:(POST) |
 00427> | OUT:01:(SWMF) | ===== OUTFLOW STORAGE TABLE =====
 00428> | OUTFLOW STORAGE | OUTFLOW STORAGE
 00429> (ha.m.) (cms) (ha.m.) (cms)
 00430>
 00431> .000 .0000E+00 .079 .1497E+00
 00432> .059 .1884E+01 .080 .1683E+00
 00433> .069 .3388E+01 .082 .1875E+00
 00434> .079 .4780E+01 .083 .2273E+00
 00435> .072 .6439E+01 .085 .2485E+00
 00436> .073 .8041E+01 .086 .2700E+00
 00437> .075 .9693E+01 .087 .2700E+00
 00438> .076 .1140E+00 .299 .4003E+00
 00439> .078 .1316E+00 .000 .0000E+00
 00440> ROUTING RESULTS AREA QPEAK TPEAK R.V.
 00441> (ha) (cms) (hrs) (mm)
 00442> INFLOW >09: (POST) 12.24 1.610 1.000 17.041
 00443> OUTFLOW:01: (SWMF) 12.24 .078 2.083 17.041
 00444> OVERFLOW:02: (000003) .00 .000 .000 .000
 00445>
 00446> TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
 00447> CUMULATIVE TIME OF OVERFLOWS (hours) = .00
 00448> PERCENTAGE OF TIME OVERFLOWING (%) = .00
 00449>
 00450>
 00451> PEAK FLOW REDUCTION [Qout/Qin](%)= 4.843
 00452> TIME SHIFT OF PEAK FLOW (min)= 65.00
 00453> MAXIMUM STORAGE USED (ha.m.)=.1315E+00
 00454>
 00455>
 00456>
 00457> TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
 00458> CUMULATIVE TIME OF OVERFLOWS (hours) = .00
 00459> PERCENTAGE OF TIME OVERFLOWING (%) = .00
 00460> | DIVERT HYD |
 00461> | INID:01 (SWMF) |
 00462> Outflow / Inflow Relationships
 00463> Flow 03 + Flow 04 + Flow 05 = Total
 00464> (cms) (cms) (cms) (cms)
 00465> .000 .000 .000 .000
 00466> .000 .059 .000 .059
 00467> .001 .061 .000 .068
 00468> .007 .063 .000 .070
 00469> .008 .064 .000 .072
 00470> .008 .065 .000 .073
 00471> .008 .066 .000 .075
 00472> .009 .068 .000 .076
 00473> .009 .069 .000 .078
 00474> .009 .070 .000 .079
 00475> .009 .071 .000 .080
 00476> .010 .072 .000 .082
 00477> .010 .073 .000 .083
 00478> .010 .074 .000 .085
 00479> .010 .075 .000 .086
 00480> .011 .077 .000 .087
 00481> .011 .078 .210 .299
 00482>
 00483> NYHD AREA QPEAK TpeakDate_hh:mm R.V. NFE WetHrs
 00484> IDin = 01:SWMF 12.24 .078 No_date 2:05 17.041 1 51.
 00485> =====
 00486> IDout = 03:Infilt 1.04 .009 No_date 2:05 17.041 1 6.
 00487> IDout = 04:rfific 11.20 .069 No_date 2:05 17.041 1 51.
 00488> IDout = 05:Emerge .00 .000 No_date 0:00 .000 0 0.
 00489>
 00490>
 00491> 001:0020-----
 00492> * * * * *
 00493> * * * * * 5-year
 00494> * * * * *
 00495> * * * * *
 00496> * * * * *
 00497> * * * * *
 00498> * * * * *
 00499> | CHICAGO STORM | IDF curve parameters: A=1330.310
 00500> | Ptotal= 45.37 mm |
 00501> | C= .855
 00502> used in: INTENSITY = A / (t + B)^C
 00503> 001:0021-----
 00504> Duration of storm = 3.00 hrs
 00505> Storm time step = 5.00 min
 00506> Time to peak ratio = .33
 00507>
 00508> TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
 00509> hrs mm/h | hrs mm/h | hrs mm/hr | hrs mm/h
 00510> .08 3.038 | .83 21.781 | 1.58 10.023 | 2.33 4.120
 00511> .17 3.356 | .92 53.191 | 1.87 8.657 | 2.42 3.866
 00512> .25 3.675 | 1.01 100.611 | 1.75 7.313 | 2.50 6.646
 00513> .33 4.257 | 1.08 68.676 | 1.83 6.790 | 2.58 3.449
 00514> .42 4.925 | 1.17 37.777 | 1.92 6.127 | 2.67 3.273
 00515> .50 5.845 | 1.25 25.123 | 2.00 5.581 | 2.75 3.114
 00516> .58 7.190 | 1.33 18.497 | 2.08 5.125 | 2.83 2.971
 00517> .67 9.326 | 1.42 14.500 | 2.17 4.739 | 2.92 2.841
 00518> .75 13.171 | 1.50 11.874 | 2.25 4.407 | 3.00 2.722
 00519>
 00520>
 00521> 001:0022-----
 00522> * * * * *
 00523> * * * * * EXISTING CONDITIONS
 00524> * * * * *
 00525> * * * * *
 00526> * * * * *
 00527>
 00528> | CALIB_NASHYD | Area (ha)= 2.37 Curve Number (CN)=72.00
 00529> | 01:EX-1 DT= 1.00 | Ia (mm)= 8.000 # of Linear Res.(N)= 3.00
 00530>----- U.H. Tp(hrs)= .330
 00531>
 00532> Uni Hyd Ppeak (cms)= .274
 00533>
 00534> PEAK FLOW (cms)= .060 (i)
 00535> TIME TO PEAK (hrs)= 1.483
 00536> RUNOFF VOLUME (mm)= 10.255
 00537> TOTAL RAINFALL (mm)= 45.366
 00538> RUNOFF COEFFICIENT = .226
 00539>
 00540> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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00541>
00542> -----
00543> 001:0023-----
00544> -----
00545> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .001 (cms)
00546> | TotalHyd 01:EX-1 | Number of inlets in system [NINLET] = 1
00547> -----
00548> Total minor system capacity = .001 (cms)
00549> Total major system storage [TMJSTO] = 99999. (cu.m.)
00549>
00550> ID: NYHD AREA QPEAK TPEAK R.V. DWF
00551> (ha) (cms) (hrs) (mm) (cms)
00552> TOTAL HYD. 01:EX-1 2.37 .060 1.483 10.255 .000
00553> =====
00554> MAJOR SYST 02:THAMES .00 .000 .000 .000 .000
00555> MINOR SYST 03:toDRAI 2.37 .001 85.350 10.257 .000
00556>
00557> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00558>
00559> Maximum MAJOR SYSTEM storage used = 234. (cu.m.)
00560>
00561>
00562> 001:0024-----
00563>
00564> | CALIB NASHYD | Area (ha)= .19 Curve Number (CN)=74.00
00565> | 01:EX-2 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res.(N)= 3.00
00566> U.H. Tp(hrs)= .090
00567>
00568> Unit Hyd Qpeak (cms)= .081
00569>
00570> PEAK FLOW (cms)= .012 (i)
00571> TIME TO PEAK (hrs)= 1.117
00572> RUNOFF VOLUME (mm)= 12.571
00573> TOTAL RAINFALL (mm)= 45.366
00574> RUNOFF COEFFICIENT = .277
00575>
00576> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00577>
00578> -----
00579> 001:0025-----
00580>
00581> | CALIB STANDHYD | Area (ha)= .45
00582> | 04:EX-3 DT= 1.00 | Total Imp(%)= 65.00 Dir. Conn.()%= 1.00
00583>
00584> IMPERVIOUS PEROVIOUS (i)
00585> Surface Area (ha)= .29 .16
00586> Dep. Storage (mm)= 2.00 8.00
00587> Average Slope (%)= 1.00 20.00
00588> Length (m)= 5.00 25.00
00589> Mannings n = .013 .240
00590>
00591> Max.eff.Inten.(mm/hr)= 149.04 237.09
00592> Ia (mm/hr) over (min)= 1.00 2.00
00593> Storage Coeff. (min)= .36 (ii) 2.20 (ii)
00594> Unit Hyd. Tpeak (min)= 1.00 2.00
00595> Unit Hyd. peak (cms)= 1.59 .52
00596> *TOTALS*
00597> PEAK FLOW (cms)= .00 .08 .085 (iii)
00598> TIME TO PEAK (hrs)= .98 1.02 1.000
00599> RUNOFF VOLUME (mm)= 43.37 23.36 23.560
00600> TOTAL RAINFALL (mm)= 45.37 45.37 45.366
00601> RUNOFF COEFFICIENT = .96 .51 .519
00602>
00603> (i) CN PROCEDURE SELECTED FOR PEROVIOUS LOSSES:
00604> CN* = 72.0 Ia = Dep. Storage (Above)
00605> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
00606> THAN THE STORAGE COEFFICIENT
00607> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00608>
00609> -----
00610> 001:0026-----
00611>
00612> | CALIB NASHYD | Area (ha)= 2.59 Curve Number (CN)=67.00
00613> | 05:EX-4 DT= 1.00 | Ia (mm)= 8.000 # of Linear Res.(N)= 3.00
00614> U.H. Tp(hrs)= .230
00615>
00616> Unit Hyd Qpeak (cms)= .430
00617>
00618> PEAK FLOW (cms)= .067 (i)
00619> TIME TO PEAK (hrs)= 1.333
00620> RUNOFF VOLUME (mm)= 8.594
00621> TOTAL RAINFALL (mm)= 45.366
00622> RUNOFF COEFFICIENT = .189
00623>
00624> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00625>
00626>
00627> 001:0027-----
00628>
00629> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .001 (cms)
00630> | TotalHyd 05:EX-4 | Number of inlets in system [NINLET] = 1
00631> -----
00632> Total minor system capacity = .001 (cms)
00633> Total major system storage [TMJSTO] = 99999. (cu.m.)
00634>
00635> ID: NYHD AREA QPEAK TPEAK R.V. DWF
00636> (ha) (cms) (hrs) (mm) (cms)
00637> TOTAL HYD. 05:EX-4 2.59 .067 1.333 8.594 .000
00638>
00639> MAJOR SYST 06:BANNAN .00 .000 .000 .000 .000
00640> MINOR SYST 07:toDRAI 2.59 .001 78.217 8.595 .000
00641>
00642> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
00643>
00644> Maximum MAJOR SYSTEM storage used = 214. (cu.m.)
00645>
00646> 001:0028-----
00647>
00648> | CALIB NASHYD | Area (ha)= 6.64 Curve Number (CN)=72.00
00649> | 05:C101 DT= 1.00 | Ia (mm)= 8.000 # of Linear Res.(N)= 3.00
00650> U.H. Tp(hrs)= .310
00651>
00652> Unit Hyd Qpeak (cms)= .818
00653>
00654> PEAK FLOW (cms)= .175 (i)
00655> TIME TO PEAK (hrs)= 1.450
00656> RUNOFF VOLUME (mm)= 10.255
00657> TOTAL RAINFALL (mm)= 45.366
00658> RUNOFF COEFFICIENT = .226
00659>
00660> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
00661>
00662>
00663> 001:0029-----
00664>
00665> | ADD HYD (PRE ) | ID: NYHD AREA QPEAK TPEAK R.V. DWF
00666> (ha) (cms) (hrs) (mm) (cms)
00667> ID1 01:EX-2 .19 .012 1.12 12.57 .000
00668> ID2 04:EX-3:RAIN 2.37 .001 85.35 10.26 .000
00669> +ID3 04:EX-3 .45 .081 1.19 20.56 .000
00670> +ID4 05:C101 6.64 .175 1.45 10.26 .000
00671> +ID5 07:toDRAIN 2.59 .001 78.22 8.59 .000
00672>
00673> SUM 08:PRE 12.24 .194 1.42 10.43 .000
00674>
00675> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

00811> Average Slope (%) = 1.00 2.00
 00812> Length (m) = 50.00 25.00
 00813> Mannings n = .013 .250
 00814>
 00815> Max.eff.Inten.(mm/hr) = 149.04 73.97
 00816> over (min) = 1.00 7.00
 00817> Storage Coeff. (min) = 1.44 (ii) 7.44 (ii)
 00818> Unit Hyd. Tpeak (min) = 1.00 7.00
 00819> Unit Hyd. peak (cms) = .85 .16
 00820> *TOTALS*
 00821> PEAK FLOW (cms) = 2.16 .09 2.194 (iii)
 00822> TIME TO PEAK (hrs) = 1.00 1.12 1.000
 00823> RUNOFF VOLUME (mm) = 43.37 14.81 37.655
 00824> TOTAL RAINFALL (mm) = 45.37 45.37 45.366
 00825> RUNOFF COEFFICIENT = .96 .33 .830
 00826>
 00827> (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:
 00828> CN* = 61.0 Ta = Dep. Storage (Above)
 00829> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 00830> THAN THE STORAGE COEFFICIENT.
 00831> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
 00832>
 00833> 001:0037-----
 00834> | ADD HYD (POST) | ID: NYHD AREA QPEAK TPEAK R.V. DWF
 00835> | | | (ha) (cms) (hrs) (mm) (cms)
 00836> | ID1 01:EX-2 .19 .012 1.12 12.57 .000
 00837> | ID2 03:toRAIN 2.37 .008 85.35 10.26 .000
 00838> | ID3 04:EX-3 .45 .085 15.12 23.56 .000
 00840> | ID4 04:C021 6.64 2.04 1.00 37.56 .000
 00841> | ID5 07:toDRAIN 2.59 .001 78.22 8.59 .000
 00842> ======
 00843> SUM 09:POST 12.24 2.287 1.00 25.29 .000
 00845>
 NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
 00847>
 00849> 001:0038-----
 00851> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
 00852> | IN>09: (POST) |
 00853> | OUT<01: (SWMF) | ====== OUTFLOW STORAGE TABLE ======
 00854> OUTFLOW STORAGE OUTFLOW STORAGE
 00855> (cms) (ha.m.) (cms) (ha.m.)
 00856> .000 .0000E+00 .079 1497E+00
 00857> .059 .1884E-01 .080 1.683E+00
 00858> .069 .3388E-01 .082 1.875E+00
 00859> .070 .4889E-01 .083 2.073E+00
 00860> .072 .6439E-01 .085 2.276E+00
 00861> .073 .8045E-01 .086 2.475E+00
 00862> .075 .9693E-01 .087 2.700E+00
 00863> .076 .1140E+00 .089 3.000E+00
 00864> .078 .1316E+00 .090 3.000E+00
 00865>
 ROUTING RESULTS AREA QPEAK TPEAK R.V.
 00866> ----- (ha) (cms) (hrs) (mm)
 00868> INFLOW >09: (POST) 12.24 2.287 1.000 25.294
 00869> OUTFLOW<01: (SWMF) 12.24 .083 2.250 25.294
 00870> OVERFLOW<02: (000003) .000 .000 .000 .000
 00871>
 00872> TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
 00873> CUMULATIVE TIME OF OVERFLOWS (hours) = .00
 00874> PERCENTAGE OF TIME OVERFLOWING (%) = .00
 00875>
 00876> PEAK FLOW REDUCTION [Qout/Qin] (%) = 3.620
 00877> TIME SHIFT OF PEAK FLOW (min) = 75.00
 00879> MAXIMUM STORAGE USED (ha.m.)=.2028E+00
 00880>
 00881>
 00882> 001:0039-----
 00883>
 00884> | DIVERT HYD |
 00885> | INID=01 (SWMF) |
 00886>
 00887> Outflow / Inflow Relationships Flow 03 + Flow 04 + Flow 05 = Total
 00888> (cms) (cms) (cms) (cms)
 00889> .000 .000 .000 .000
 00890> .000 .059 .000 .059
 00891> .007 .061 .000 .069
 00892> .07 .063 .000 .070
 00893> .008 .064 .000 .072
 00894> .008 .065 .000 .073
 00895> .008 .066 .000 .073
 00896> .009 .068 .000 .076
 00897> .009 .069 .000 .078
 00898> .009 .070 .000 .079
 00899> .009 .071 .000 .080
 00901> .010 .072 .000 .082
 00902> .010 .073 .000 .083
 00903> .010 .074 .000 .085
 00904> .010 .075 .000 .086
 00905> .011 .077 .000 .087
 00906> .011 .078 .210 .239
 00907>
 00908> NYHD AREA QPEAK TpeakDate_hh:mm R.V. NFE WetHrs
 00909> (ha) (cms) (hrs) (hrs) (mm)
 00910> IDin = 01:SWMF 12.24 .083 No_date 2:15 25.294 1 93.
 00911> ======
 00912> IDout= 03:Infil 1.07 .010 No_date 2:15 25.294 1 9.
 00913> IDout= 04:Orific 11.16 .073 No_date 2:15 25.294 1 93.
 00914> IDout= 05:Emerge .00 .000 No_date 0:00 .000 0 0.
 00915>
 00916> 001:0040-----
 00917> *#
 00918> *#
 00919> *# 10-year
 00920> *#
 00921> *# ======
 00922> ******
 00923> | CHICAGO STORM | IDF curve parameters: A=1497.190
 00924> | Ptotal= 52.59 mm | B= 7.188
 00925> | C= .850
 00926> used in: INTENSITY = A / (t + B)^C
 00927>
 Duration of storm = 3.00 hours
 00928> Storm time step = 5.00 min
 00929> Time to peak ratio = .33
 00930>
 00931>
 00932>
 00933> TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
 00934> hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
 00935> .08 3.544 | .83 24.635 | 1.58 11.418 | 2.33 4.775
 00936> .17 3.907 | .92 60.893 | 1.67 9.866 | 2.42 4.490
 00937> .25 4.357 | 1.00 178.445 | 1.75 8.714 | 2.50 4.237
 00938> .33 4.936 | 1.00 178.445 | 1.83 7.514 | 2.58 4.013
 00939> .42 5.586 | 1.17 42.842 | 1.92 7.043 | 2.67 3.812
 00940> .50 6.728 | 1.25 28.407 | 2.00 6.428 | 2.75 3.521
 00941> .58 8.239 | 1.33 20.928 | 2.08 5.913 | 2.83 3.467
 00942> .67 10.636 | 1.42 16.445 | 2.17 5.476 | 2.92 3.318
 00943> .75 14.947 | 1.50 13.493 | 2.25 5.101 | 3.00 3.182
 00944>
 00945>

00946> 001:0041-----
 00947> ******
 00948> *# EXISTING CONDITIONS
 00949> *#
 00950> *#
 00951> ******
 00952> | CALIB NASHYD | Area (ha) = 2.37 Curve Number (CN)=72.00
 00953> | 01:EX-1 DT= 1.00 | Ta (mm) = 8.000 # of Linear Res.(N) = 3.00
 00954> U.H. Tp(hrs) = .330
 00955>
 00956> Unit Hyd Opeak (cms) = .274
 00957>
 00958>
 00959> PEAK FLOW (cms) = .083 (i)
 00960> TIME TO PEAK (hrs) = 1.467
 00961> RUNOFF VOLUME (mm) = 13.868
 00962> TOTAL RAINFALL (mm) = 52.590
 00963> RUNOFF COEFFICIENT = .264
 00964>
 00965> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
 00966>
 00967>
 00968> 001:0042-----
 00969>
 00970> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .001 (cms)
 00971> | TotalHyd 01:EX-1 | Number of inlets in system [NINLET] = 1
 00972> | | Total minor system capacity = .001 (cms)
 00973> | | Total major system storage [TMJSTO] = 99999. (cu.m.)
 00974>
 00975> ID: NYHD AREA QPEAK TPEAK R.V. DWF
 00976> (ha) (cms) (hrs) (mm) (cms)
 00977> TOTAL HYD. 01:EX-1 2.37 .083 1.467 13.868 .000
 00978>
 00979> MAJOR SYST 02:THAMES .00 .000 .000 .000 .000
 00980> MINOR SYST 03:toDRAI 2.37 .001 115.050 13.867 .000
 00981>
 00982> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
 00983>
 00984> Maximum MAJOR SYSTEM storage used = 319. (cu.m.)
 00985>
 00986>
 00987> 001:0043-----
 00988>
 00989> | CALIB NASHYD | Area (ha) = .19 Curve Number (CN)=74.00
 00990> | 01:EX-2 DT= 1.00 | Ta (mm) = 5.000 # of Linear Res.(N) = 3.00
 00991> U.H. Tp(hrs) = .090
 00992>
 00993> Unit Hyd Opeak (cms) = .081
 00994>
 00995> PEAK FLOW (cms) = .017 (i)
 00996> TIME TO PEAK (hrs) = 1.100
 00997> RUNOFF VOLUME (mm) = 16.551
 00998> TOTAL RAINFALL (mm) = 52.590
 00999> RUNOFF COEFFICIENT = .315
 01000>
 01001> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
 01002>
 01003>
 01004> 001:0044-----
 01005> | CALIB STANDHYD | Area (ha) = .45
 01006> | 04:EX-3 DT= 1.00 | Total Imp(%) = 65.00 Dir. Conn. (%) = 1.00
 01007>
 01008>
 01009> | CALIB NASHYD | Area (ha) = .19 Curve Number (CN)=74.00
 01010> | 01:EX-2 DT= 1.00 | Ta (mm) = 5.000 # of Linear Res.(N) = 3.00
 01011> U.H. Tp(hrs) = .090
 01012>
 01013> Surface Area (ha) = .29 .16
 01014> Dep. Storage (mm) = 2.00 8.00
 01015> Average Slope (%) = 1.00 20.00
 01016> Length (m) = 5.00 25.00
 01017> Mannings n = .013 .240
 01018>
 01019> Max.eff.Inten.(mm/hr) = 178.75 311.11
 01020> over (min) = 1.00 2.00
 01021> Storage Coeff. (min) = .34 (ii) 1.99 (ii)
 01022> Unit Hyd. Tpeak (min) = 1.00 2.00
 01023> Unit Hyd. peak (cms) = 1.61 .56
 01024> *TOTALS*
 01025> PEAK FLOW (cms) = .00 .11 116 (iii)
 01026> TIME TO PEAK (hrs) = .98 1.00 1.000
 01027> RUNOFF VOLUME (mm) = 50.59 29.24 29.454
 01028> TOTAL RAINFALL (mm) = 52.59 52.59 52.590
 01029> RUNOFF COEFFICIENT = .96 .56 .560
 01030>
 01031> (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:
 01032> CN* = 72.0 Ta = Dep. Storage (Above)
 01033> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 01034> THAN THE STORAGE COEFFICIENT.
 01035> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
 01036>
 01037> | CALIB NASHYD | Area (ha) = 2.59 Curve Number (CN)=67.00
 01038> | 05:EX-4 DT= 1.00 | Ta (mm) = 8.000 # of Linear Res.(N) = 3.00
 01039> U.H. Tp(hrs) = .230
 01040>
 01041> Unit Hyd Opeak (cms) = .430
 01042>
 01043> PEAK FLOW (cms) = .094 (i)
 01044> TIME TO PEAK (hrs) = 1.317
 01045> RUNOFF VOLUME (mm) = 11.717
 01046> TOTAL RAINFALL (mm) = 52.590
 01047> RUNOFF COEFFICIENT = .223
 01048>
 01049> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
 01050>
 01051>
 01052> 001:0046-----
 01053> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .001 (cms)
 01054> | TotalHyd 05:EX-4 | Number of inlets in system [NINLET] = 1
 01055> | | Total minor system capacity = .001 (cms)
 01056> | | Total major system storage [TMJSTO] = 99999. (cu.m.)
 01057>
 01058> ID: NYHD AREA QPEAK TPEAK R.V. DWF
 01059> (ha) (cms) (hrs) (mm) (cms)
 01060> TOTAL HYD. 05:EX-4 2.59 .094 1.317 11.717 .000
 01061>
 01062>
 01063> MAJOR SYST 06:BANNAN .00 .000 .000 .000 .000
 01064> MINOR SYST 07:toDRAI 2.59 .001 106.283 11.717 .000
 01065>
 01066> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
 01067>
 01068> Maximum MAJOR SYSTEM storage used = 295. (cu.m.)
 01069>
 01070>
 01071> 001:0047-----
 01072> | CALIB NASHYD | Area (ha) = 6.64 Curve Number (CN)=72.00
 01073> | 05:CO1 DT= 1.00 | Ta (mm) = 8.000 # of Linear Res.(N) = 3.00
 01074> U.H. Tp(hrs) = .310
 01075>
 01076> Unit Hyd Opeak (cms) = .818
 01077>
 01078> PEAK FLOW (cms) = .242 (i)
 01079>
 01080> TIME TO PEAK (hrs) = 1.433

01081> RUNOFF VOLUME (mm)= 13.868
 01082> TOTAL RAINFALL (mm)= 52.590
 01083> RUNOFF COEFFICIENT = .264
 01084>
 01085> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
 01086>
 01087>-----
 01088> 001:0049--
 01089>-----
 01090> | ADD HYD (PRE) | ID: NYHD AREA QPEAK TPEAK R.V. DWF
 01091> | | ID: NYHD (ha) (cms) (hrs) (mm) (cms)
 01092> | | ID1 01:EX-2 .19 .017 1.10 16.55 .000
 01093> | | +ID2 03:toDRAIN 2.37 .001 115.05 13.87 .000
 01094> | | +ID3 04:EX-3 .45 .116 1.00 29.45 .000
 01095> | | +ID4 05:C101 6.64 .242 1.43 13.87 .000
 01096> | | +ID5 07:toDRAIN 2.59 .001 106.28 11.72 .000
 01097>-----
 01098> SUM 08:PRE 12.24 .266 1.42 14.03 .000
 01099>
 01100> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
 01101>
 01102>-----
 01103> 001:0049--
 01104> *#*****
 01105> #=====
 01106> # PROPOSED CONDITIONS
 01107> #=====
 01108> *#*****
 01109>
 01110> | CALIB NASHYD | Area (ha)= 2.37 Curve Number (CN)=72.00
 01111> | 01:EX-1 DT= 1.00 | Ia (mm)= 8.000 # of Linear Res.(N)= 3.00
 01112> | U.H. Tp(hrs)= .330
 01113>
 01114> Unit Hyd Ppeak (cms)= .274
 01115>
 01116> PEAK FLOW (cms)= .083 (i)
 01117> TIME TO PEAK (hrs)= 1.467
 01118> RUNOFF VOLUME (mm)= 13.868
 01119> TOTAL RAINFALL (mm)= 52.590
 01120> RUNOFF COEFFICIENT = .264
 01121>
 01122> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
 01123>
 01124>-----
 01125> 001:0050--
 01126>
 01127> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .001 (cms)
 01128> | TotalHyd 01:EX-1 | Number of inlets in system [NINLET] = 1
 01129>-----
 01130> Total major system capacity = .001 (cms)
 01131> Total major system storage [TMJSTO] = 99999.000 (cu.m.)
 01132>
 01133> ID: NYHD AREA QPEAK TPEAK R.V. DWF
 01134> | TOTAL HYD. 01:EX-1 2.37 .083 1.467 13.868 .000
 01135>
 01136> MAJOR SYST 02:THAMES .00 .000 .000 .000 .000
 01137> MINOR SYST 03:toDRAIN 2.37 .001 115.050 13.867 .000
 01138>
 01139> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
 01140>
 01141> Maximum MAJOR SYSTEM storage used = 319.000 (cu.m.)
 01142>
 01143>
 01144> 001:0051--
 01145>
 01146> | CALIB NASHYD | Area (ha)= .19 Curve Number (CN)=74.00
 01147> | 01:EX-2 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res.(N)= 3.00
 01148> | U.H. Tp(hrs)= .090
 01149>
 01150> Unit Hyd Ppeak (cms)= .081
 01151>
 01152> PEAK FLOW (cms)= .017 (i)
 01153> TIME TO PEAK (hrs)= 1.100
 01154> RUNOFF VOLUME (mm)= 16.551
 01155> TOTAL RAINFALL (mm)= 52.500
 01156> RUNOFF COEFFICIENT = .315
 01157>
 01158> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
 01159>
 01160>-----
 01161> 001:0052--
 01162>
 01163> | CALIB STANDHYD | Area (ha)= .45
 01164> | 04:EX-3 DT= 1.00 | Total Imp(%)= 65.00 Dir. Conn. (%)= 1.00
 01165>
 01166> IMPERVIOUS PERVIOUS (i)
 01167> Surface Area (ha)= .29 .16
 01168> Dep. Storage (mm)= 2.00 8.00
 01169> Average Slope (%)= 1.00 20.00
 01170> Length (m)= 5.00 25.00
 01171> Mannings n = .013 .240
 01172>
 01173> Max.eff.Inten.(mm/hr)= 178.75 311.11
 01174> over (min)= 1.00 2.00
 01175> Storage Coef. (min)= .34 (ii) 1.99 (ii)
 01176> Unit Hyd. Tpeak (min)= 1.00 2.00
 01177> Unit Hyd. peak (cms)= 1.61 .56
 01178> *TOTALS*
 01179> PEAK FLOW (cms)= .00 .11 .116 (iii)
 01180> TIME TO PEAK (hrs)= .98 1.00 1.000
 01181> RUNOFF VOLUME (mm)= 50.59 29.24 29.454
 01182> TOTAL RAINFALL (mm)= 52.59 52.59 52.590
 01183> RUNOFF COEFFICIENT = .96 .56 .560
 01184>
 01185> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
 01186> CN* = 72.0 Ia Dep. Storage (Above)
 01187> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 01188> THAN THE STORAGE COEFFICIENT.
 01189> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
 01190>
 01191>-----
 01192> 001:0053--
 01193>
 01194> | CALIB NASHYD | Area (ha)= 2.59 Curve Number (CN)=67.00
 01195> | 05:EX-4 DT= 1.00 | Ia (mm)= 8.000 # of Linear Res.(N)= 3.00
 01196> | U.H. Tp(hrs)= .230
 01197>
 01198> Unit Hyd Ppeak (cms)= .430
 01199>
 01200> PEAK FLOW (cms)= .094 (i)
 01201> TIME TO PEAK (hrs)= 1.317
 01202> RUNOFF VOLUME (mm)= 11.717
 01203> TOTAL RAINFALL (mm)= 52.590
 01204> RUNOFF COEFFICIENT = .223
 01205>
 01206> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
 01207>
 01208>-----
 01209> 001:0054--
 01210>
 01211> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .001 (cms)
 01212> | TotalHyd 05:EX-4 | Number of inlets in system [NINLET] = 1
 01213>-----
 01214> Total minor system capacity = .001 (cms)
 01215> Total major system storage [TMJSTO] = 99999.000 (cu.m.)
 01216>
 01217> ID: NYHD AREA QPEAK TPEAK R.V. DWF
 01218> | ID: NYHD (ha) (cms) (hrs) (mm) (cms)
 01219>-----
 01220> TOTAL HYD. 05:EX-4 2.59 .094 1.317 11.717 .000
 01221>-----
 01222> MAJOR SYST 06:BANNAN .00 .000 .000 .000 .000
 01223> MINOR SYST 07:toDRAIN 2.59 .001 106.283 11.717 .000
 01224>
 01225> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
 01226>
 01227>-----
 01228> 001:0055--
 01229>
 01230> | CALIB STANDHYD | Area (ha)= 6.64
 01231> | 05:CO21 DT= 1.00 | Total Imp(%)= 90.00 Dir. Conn. (%)= 80.00
 01232>
 01233> IMPERVIOUS PERVIOUS (i)
 01234> Surface Area (ha)= 5.98 .66
 01235> Dep. Storage (mm)= 2.00 5.00
 01236> Average Slope (%)= 1.00 2.00
 01237> Length (m)= 50.00 25.00
 01238> Mannings n = .013 .250
 01239>
 01240> Max.eff.Inten.(mm/hr)= 178.75 100.19
 01241> over (min)= 1.00 7.00
 01242> Storage Coeff. (min)= 1.34 (ii) 6.66 (ii)
 01243> Unit Hyd. Tpeak (min)= 1.00 7.00
 01244> Unit Hyd. peak (cms)= .90 .17
 01245>
 01246> *TOTALS*
 01247>-----
 01248> (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
 01249> CN* = 61.0 Ia = Dep. Storage (Above)
 01250> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 01251> THAN THE STORAGE COEFFICIENT.
 01252> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
 01253>
 01254>
 01255>
 01256>
 01257>
 01258>
 01259> 001:0056--
 01260>
 01261> | ADD HYD (POST) | ID: NYHD AREA QPEAK TPEAK R.V. DWF
 01262>-----
 01263> | ID1 01:EX-2 .19 .017 1.10 16.55 .000
 01264> | +ID2 03:toDRAIN 2.37 .001 115.05 13.87 .000
 01265> | +ID3 04:EX-3 .45 .116 1.00 29.45 .000
 01266> | +ID4 05:CO21 6.64 2.653 1.00 44.29 .000
 01267> | +ID5 07:toDRAIN 2.59 .001 106.28 11.72 .000
 01268>
 01269>-----
 01270> SUM 09:POST 12.24 2.779 1.00 30.53 .000
 01271>
 01272> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
 01273>
 01274> 001:0057--
 01275>
 01276> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
 01277>-----
 01278> | IN>09: (POST) |
 01279> | OUT<01: (SWMF) | ===== OUTFLOW STORAGE TABLE =====
 01280>-----
 01281> OUTFLOW STORAGE TABLE =====
 01282> (cms) (ha.m.) (cms) (ha.m.)
 01283> .000 .0000E+00 .079 .1497E+00
 01284> .059 .1884E+01 .080 .1683E+00
 01285> .069 .3388E+01 .082 .1875E+00
 01286> .070 .4889E+01 .083 .2073E+00
 01287> .072 .6439E+01 .085 .2276E+00
 01288> .073 .8041E+01 .086 .2485E+00
 01289> .075 .9693E+01 .087 .2700E+00
 01290> .076 .1140E+00 .089 .4003E+00
 01291> .078 .1316E+00 .090 .0000E+00
 01292>-----
 01293> ROUTING RESULTS AREA QPEAK TPEAK R.V.
 01294>-----
 01295> INFLOW >9: (POST) (ha) (cms) (hrs) (mm)
 01296> OUTFLOW<01: (SWMF) 12.24 2.779 1.00 30.531
 01297> OUTFLOW<02: (000003) .00 .000 .000 .000
 01298>
 01299> TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
 01300> CUMULATIVE TIME OF OVERFLOWS (hours) = .00
 01301> PERCENTAGE OF TIME OVERFLOWING (%) = .00
 01302>
 01303> PEAK FLOW REDUCTION [Qout/Qin](%) = 3.089
 01304> TIME SHIFT OF PEAK FLOW (min) = 83.00
 01305> MAXIMUM STORAGE USED (ha.m.) = .2452E+00
 01306>
 01307> 001:0058--
 01308>
 01309> | DIVERT HYD |
 01310> | INID=01: (SWMF) |
 01311>-----
 01312> Outflow / Inflow Relationships
 01313> Flow 03 + Flow 04 + Flow 05 = Total
 01314> (cms) (cms) (cms) (cms)
 01315> .000 .000 .000 .000
 01316> .000 .059 .000 .059
 01317> .007 .061 .000 .069
 01318> .007 .063 .000 .070
 01319> .008 .064 .000 .072
 01320> .008 .065 .000 .073
 01321> .008 .066 .000 .075
 01322> .009 .067 .000 .076
 01323> .009 .069 .000 .078
 01324> .009 .070 .000 .079
 01325> .009 .071 .000 .080
 01326> .010 .072 .000 .082
 01327> .010 .073 .000 .083
 01328> .010 .074 .000 .085
 01329> .010 .075 .000 .086
 01330> .011 .077 .000 .087
 01331> .011 .078 .210 .229
 01332>
 01333> NYHD AREA QPEAK TpeakDate_hh:mm R.V. NFE WetHrs
 01334> IDin = 01:SWMF 12.24 .086 No_date 2:23 30.531 1 123.
 01335>-----
 01336>
 01337> IDout= 03:Infilt 1.07 .010 No_date 2:23 30.531 1 11.
 01338> IDout= 04:Orific 11.14 .075 No_date 2:23 30.531 1 123.
 01339> IDout= 05:Emerge .00 .000 No_date 0:00 .000 0 0.
 01340>
 01341> 001:0059--
 01342> *#*****
 01343> #
 01344> #-----
 01345> #-----
 01346> #-----
 01347> *#*****
 01348> -----
 01349> | CHICAGO STORM | IDF curve parameters: A=1455.000
 01350> Pttotal= 60.37 mm | B= 5.000

01351> -----
01352> used in: INTENSITY = A / (t + B)^C
01353>
01354> Duration of storm = 3.00 hrs
01355> Storm time step = 5.00 min
01356> Time to peak ratio = .33
01357>
01358> TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
01359> hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
01360> .08 4,464 | .83 26,338 | 1.58 12,906 | 2.33 5,854
01361> .17 4,878 | .92 65,076 | 1.67 11,320 | 2.42 5,536
01362> .25 5,387 | 1.00 220,223 | 1.75 10,095 | 2.50 5,253
01363> .33 6,027 | 1.08 85,162 | 1.83 9,119 | 2.58 4,999
01364> .42 6,858 | 1.17 45,078 | 1.92 8,324 | 2.67 4,771
01365> .50 7,983 | 1.25 30,164 | 2.00 7,664 | 2.75 4,564
01366> .58 9,594 | 1.33 22,579 | 2.08 7,106 | 2.83 4,376
01367> .67 12,097 | 1.42 18,039 | 2.17 6,629 | 2.92 4,204
01368> .75 16,515 | 1.50 15,035 | 2.25 6,216 | 3.00 4,046
01369>
01370> -----
01371> 001:0060-----
01372> *#*****
01373> *#
01374> *# EXISTING CONDITIONS
01375> *#
01376> *#*****
01377> -----
01378> | CALIB NASHYD | Area (ha) = 2.37 Curve Number (CN)=72.00
01379> | 01:EX-1 DT= 1.00 | Ia (mm) = 8,000 # of Linear Res.(N) = 3.00
01380> U.H. Tp(hrs) = .330
01381>
01382> Unit Hyd Ppeak (cms) = .274
01383> PEAK FLOW (cms) = .109 (i)
01384> TIME TO PEAK (hrs) = 1.433
01385> RUNOFF VOLUME (mm) = 18,147
01386> TOTAL RAINFALL (mm) = 60,373
01387> RUNOFF COEFFICIENT = .301
01388>
01389> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01390>
01391>
01392>
01393> 001:0061-----
01394>
01395> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .001 (cms)
01396> | TotalHyd 01:EX-1 | Number of inlets in system [NINLET] = 1
01397> ----- Total minor system capacity = .001 (cms)
01398> Total major system storage [TMJSTO] = 99999. (cu.m.)
01399>
01400> ID: NYHD AREA QPEAK TPEAK R.V. DWF
01401> (ha) (cms) (hrs) (mm) (hrs) (cms)
01402> TOTAL HYD. 01:EX-1 2.37 .109 1.433 18.147 .000
01403> -----
01404> MAJOR SYST 02:THAMES .00 .000 .000 .000 .000
01405> MINOR SYST 03:toDRAI 2.37 .001 150.250 18.146 .000
01406>
01407> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01408>
01409> Maximum MAJOR SYSTEM storage used = 421. (cu.m.)
01410>
01411> -----
01412> 001:0062-----
01413>
01414> | CALIB NASHYD | Area (ha) = .19 Curve Number (CN)=74.00
01415> | 01:EX-2 DT= 1.00 | Ia (mm) = 5,000 # of Linear Res.(N) = 3.00
01416> U.H. Tp(hrs) = .090
01417>
01418> Unit Hyd Ppeak (cms) = .081
01419> PEAK FLOW (cms) = .023 (i)
01420> TIME TO PEAK (hrs) = 1.100
01421> RUNOFF VOLUME (mm) = 21,201
01422> TOTAL RAINFALL (mm) = 60,373
01423> RUNOFF COEFFICIENT = .351
01424>
01425> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01426>
01427>
01428> 001:0063-----
01429>
01430>
01431> | CALIB STANDHYD | Area (ha) = .45
01432> | 04:EX-3 DT= 1.00 | Total Imp(%) = 65.00 Dir. Conn.(%) = 1.00
01433>
01434> IMPERVIOUS PERVIOUS (i)
01435> Surface Area (ha) = .29 .16
01436> Dep. Storage (mm) = 2.00 8.00
01437> Average Slope (%) = 1.00 20.00
01438> Length (m) = 5.00 25.00
01439> Mannings n = .013 .240
01440>
01441> Max.eff.Inten.(mm/hr) = 220.22 414.90
01442> over (min) = 1.00 2.00
01443> Storage Coeff. (min)= .31 (ii) 1.78 (ii)
01444> Unit Hyd. Peak (min)= 1.00 2.00
01445> Unit Hyd. peak (cms)= 1.63 .60
01446>
01447> PEAK FLOW (cms) = .00 .16 .159 (iii)
01448> TIME TO PEAK (hrs) = .98 1.00 1.000
01449> RUNOFF VOLUME (mm) = 58.37 35.81 36,038
01450> TOTAL RAINFALL (mm) = 60.37 60.37 60.373
01451> RUNOFF COEFFICIENT = .97 .59 .597
01452>
01453> (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:
01454> CN* = 72.0 Ia = Dep. Storage (Above)
01455> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
01456> THAN THE STORAGE COEFFICIENT.
01457> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01458>
01459> 001:0064-----
01460>
01461> | CALIB NASHYD | Area (ha) = 2.59 Curve Number (CN)=67.00
01462> | 05:EX-4 DT= 1.00 | Ia (mm) = 8,000 # of Linear Res.(N) = 3.00
01463> U.H. Tp(hrs) = .230
01464>
01465> Unit Hyd Ppeak (cms) = .430
01466>
01467> PEAK FLOW (cms) = .126 (i)
01468> TIME TO PEAK (hrs) = 1.300
01469> RUNOFF VOLUME (mm) = 15,455
01470> TOTAL RAINFALL (mm) = 60,373
01471> RUNOFF COEFFICIENT = .256
01472>
01473> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01474>
01475>
01476> 001:0065-----
01477>
01478> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .001 (cms)
01479> | TotalHyd 05:EX-4 | Number of inlets in system [NINLET] = 1
01480> ----- Total minor system capacity = .001 (cms)
01481> Total major system storage [TMJSTO] = 99999. (cu.m.)
01482>
01483>
01484> ID: NYHD AREA QPEAK TPEAK R.V. DWF
01485> (ha) (cms) (hrs) (mm) (cms)

01486> TOTAL HYD. 05:EX-4 2.59 .126 1.300 15,455 .000
01487> ======
01488> MAJOR SYST 06:BANNAN .00 .000 .000 .000 .000
01489> MINOR SYST 07:toDRAI 2.59 .001 139.883 15,454 .000
01490>
01491> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01492>
01493> Maximum MAJOR SYSTEM storage used = 392. (cu.m.)
01494>
01495> 001:0066-----
01496> 001:0067-----
01497> | CALIB NASHYD | Area (ha) = 6.64 Curve Number (CN)=72.00
01498> | 05:CO10 DT= 1.00 | Ia (mm) = 8,000 # of Linear Res.(N) = 3.00
01499> U.H. Tp(hrs) = .310
01500>
01501> Uni Hyd Ppeak (cms) = .818
01502>
01503> PEAK FLOW (cms) = .317 (i)
01504> TIME TO PEAK (hrs) = 1.417
01505> RUNOFF VOLUME (mm) = 18,147
01506> TOTAL RAINFALL (mm) = 60,373
01507> RUNOFF COEFFICIENT = .301
01508>
01509>
01510> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01511>
01512>
01513> 001:0068-----
01514> | ADD HYD (PRE) | ID: NYHY AREA QPEAK TPEAK R.V. DWF
01515> (ha) (.023) (.001) (21.20) (.000)
01516> ID1 01:EX-2 .19 .023 1.10 21.20 .000
01517> +ID2 03:toDRAIN 2.37 .001 150.25 18.15 .000
01518> +ID3 04:EX-3 .45 .159 1.00 36.04 .000
01519> +ID4 05:CO10 6.64 .317 1.42 18.15 .000
01520> +ID5 07:toDRAIN 2.59 .001 139.88 15.45 .000
01521>
01522> ======
01523> SUM 08:PRE 12.24 .345 1.40 18.28 .000
01524>
01525> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01526>
01527>
01528> 001:0069-----
01529> *#*****
01530> *# PROPOSED CONDITIONS
01531> *#
01532> *#
01533> *#*****
01534>
01535> | CALIB NASHYD | Area (ha) = 2.37 Curve Number (CN)=72.00
01536> | 01:EX-1 DT= 1.00 | Ia (mm) = 8,000 # of Linear Res.(N) = 3.00
01537> U.H. Tp(hrs) = .330
01538>
01539> Unit Hyd Ppeak (cms) = .274
01540> PEAK FLOW (cms) = .109 (i)
01541> TIME TO PEAK (hrs) = 1.433
01542> RUNOFF VOLUME (mm) = 18,147
01543> TOTAL RAINFALL (mm) = 60,373
01544> RUNOFF COEFFICIENT = .301
01545>
01546> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01547>
01548>
01549>
01550> 001:0069-----
01551>
01552> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .001 (cms)
01553> | TotalHyd 01:EX-1 | Number of inlets in system [NINLET] = 1
01554> ----- Total minor system capacity = .001 (cms)
01555> Total major system storage [TMJSTO] = 99999. (cu.m.)
01556>
01557> ID: NYHD AREA QPEAK TPEAK R.V. DWF
01558> (ha) (.023) (.001) (18.147) (.000)
01559> TOTAL HYD. 01:EX-1 2.37 .109 1.433 18.147 .000
01560>
01561> MAJOR SYST 02:THAMES .00 .000 .000 .000 .000
01562> MINOR SYST 03:toDRAI 2.37 .001 150.250 18.146 .000
01563>
01564> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01565>
01566> Maximum MAJOR SYSTEM storage used = 421. (cu.m.)
01567>
01568>
01569> 001:0070-----
01570>
01571> | CALIB NASHYD | Area (ha) = .19 Curve Number (CN)=74.00
01572> | 01:EX-2 DT= 1.00 | Ia (mm) = 5,000 # of Linear Res.(N) = 3.00
01573> U.H. Tp(hrs) = .090
01574>
01575> Unit Hyd Ppeak (cms) = .081
01576>
01577> PEAK FLOW (cms) = .023 (i)
01578> TIME TO PEAK (hrs) = 1.100
01579> RUNOFF VOLUME (mm) = 21,201
01580> TOTAL RAINFALL (mm) = 60,373
01581> RUNOFF COEFFICIENT = .351
01582>
01583> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01584>
01585> 001:0071-----
01586>
01587>
01588> | CALIB STANDHYD | Area (ha) = .45
01589> | 04:EX-3 DT= 1.00 | Total Imp(%) = 65.00 Dir. Conn.(%) = 1.00
01590>
01591> IMPERVIOUS PERVIOUS (i)
01592>
01593> Surface Area (ha) = .29 .16
01594> Dep. Storage (mm) = 2.00 8.00
01595> Average Slope (%) = 1.00 20.00
01596> Length (m) = 5.00 25.00
01597> Mannings n = .013 .240
01598>
01599> Max.eff.Inten.(mm/hr) = 220.22 414.90
01600> over (min) = 1.00 2.00
01601> Storage Coeff. (min)= .31 (ii) 1.78 (ii)
01602> Unit Hyd. Peak (min)= 1.00 2.00
01603> Unit Hyd. peak (cms)= 1.63 .60
01604>
01605> PEAK FLOW (cms) = .00 .16 .159 (iii)
01606> TIME TO PEAK (hrs) = .98 1.00 1.000
01607> RUNOFF VOLUME (mm) = 58.37 35.81 36,038
01608> TOTAL RAINFALL (mm) = 60.37 60.37 60.373
01609> RUNOFF COEFFICIENT = .97 .59 .597
01610>
01611> (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:
01612> CN* = 72.0 Ia = Dep. Storage (Above)
01613> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
01614> THAN THE STORAGE COEFFICIENT.
01615> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01616>
01617> 001:0072-----
01618>
01619> | CALIB NASHYD | Area (ha) = 2.59 Curve Number (CN)=67.00
01620> | 05:EX-4 DT= 1.00 | Ia (mm) = 8,000 # of Linear Res.(N) = 3.00

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01621> ----- U.H. Tp(hrs)= .230
01622>
01623> Unit Hyd Qpeak (cms)= .430
01624>
01625> PEAK FLOW (cms)= .126 (i)
01626> TIME TO PEAK (hrs)= 1.300
01627> RUNOFF VOLUME (mm)= 15.455
01628> TOTAL RAINFALL (mm)= 60.373
01629> RUNOFF COEFFICIENT = .256
01630>
01631> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01632>
01633>
01634> 001:0073-----
01635> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .001 (cms)
01636> | TotalHyd 05:EX-4 | Number of inlets in system [NINLET] = 1
01637> |----- Total minor system capacity = .001 (cms)
01638> |----- Total major system storage [TMJSTO] = 99999. (cu.m.)
01640>
01641> ID: NYHD AREA QPEAK TPEAK R.V. DWF
01642> (ha) (cms) (hrs) (mm) (cms)
01643> TOTAL HYD. 05:EX-4 2.59 .126 1.300 15.455 .000
01644> =====
01645> MAJOR SYST 06:BANNAN .00 .000 .000 .000 .000
01646> MINOR SYST 07:toDRAIN 2.59 .001 139.883 15.454 .000
01647>
01648> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01649>
01650> Maximum MAJOR SYSTEM storage used = 392. (cu.m.)
01651>
01652>
01653> 001:0074-----
01654> | CALIB STANDHYD | Area (ha)= 6.64
01655> | 05:C201 DT= 1.00 | Total Imp(%)= 90.00 Dir. Conn.(%)= 80.00
01656> |----- IMPERVIOUS PERVERIOUS (i)
01657> Surface Area (ha)= 5.98 .66
01658> Dep. Storage (mm)= 2.0 5.0
01659> Average Slope (%)= 1.00 2.00
01660> Length (m)= 50.00 25.00
01661> Manning's n = .013 .250
01662>
01663>
01664> Max.eff.Inten.(mm/hr)= 220.22 144.22
01665> over (min) 1.00 6.00
01666> Storage Coeff. (min)= 1.23 (ii) 5.83 (ii)
01667> Unit Hyd. Tpeak (min)= 1.00 6.00
01668> Unit Hyd. peak (cms)= .95 .19
01669>
01670> *TOTALS*
01671> PEAK FLOW (cms)= 3.21 .18 3.06 (iii)
01672> TIME TO PEAK (hrs)= 1.00 1.00
01673> RUNOFF VOLUME (mm)= 58.37 24.08 51.515
01674> TOTAL RAINFALL (mm)= 60.37 60.373
01675> RUNOFF COEFFICIENT = .97 .40 .853
01676>
01677> (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:
01678> CN*= 61.0 Ia = Dep. Storage (Above)
01679> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
01680> THAN THE STORAGE COEFFICIENT.
01681> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
01682>
01683>
01684> 001:0075-----
01685>
01686> | ADD HYD (POST ) | ID: NYHD AREA QPEAK TPEAK R.V. DWF
01687> |----- (ha) (cms) (hrs) (mm) (cms)
01688> |----- ID1 01:EX-2 .19 .023 1.10 21.20 .000
01689> |----- +ID2 03:toDRAIN 2.37 .001 150.25 18.15 .000
01690> |----- +ID3 04:EX-3 .45 .159 1.00 36.04 .000
01691> |----- +ID4 05:C201 6.64 3.306 1.00 51.52 .000
01692> |----- +ID5 07:toDRAIN 2.59 .001 139.88 15.45 .000
01693>
01694> SUM 09:POST 12.24 3.478 1.00 36.37 .000
01695>
01696> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
01697>
01698>
01699> 001:0076-----
01700>
01701> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
01702> | IN:09:(POST ) |
01703> | OUT<01:(SWMF ) |
01704> ===== OUTFLOW STORAGE TABLE =====
01705> |----- OUTFLOW STORED (cms) OUTFLOW (cms) STORAGE (ha.m.) (ha.m.)
01706> |----- .000 0.000E+00 | .079 1.975E+00
01707> |----- .059 1.984E-01 | .080 1.683E+00
01708> |----- .069 3.388E-01 | .082 1.875E+00
01709> |----- .070 4.889E-01 | .083 2.073E+00
01710> |----- .072 6.439E-01 | .085 .2276E+00
01711> |----- .073 .8041E-01 | .086 .2485E+00
01712> |----- .075 .9693E-01 | .087 .2700E+00
01713> |----- .076 .1140E+00 | .099 .4003E+00
01714> |----- .078 .1316E+00 | .000 .0000E+00
01715>
01716> ROUTING RESULTS AREA QPEAK TPEAK R.V.
01717> (ha) (cms) (hrs) (mm)
01718> INFLOW>0: (POST ) 12.24 3.478 1.000 36.373
01719> OUTFLOW<01: (SWMF ) 12.24 .112 2.317 36.375
01720> OVERFLOW<02: (000003) .00 .000 .000 .000
01721>
01722> TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
01723> CUMULATIVE TIME OF OVERFLOWS (hours)= .00
01724> PERCENTAGE OF TIME OVERFLOWING (%)= .00
01725>
01726>
01727> PEAK FLOW REDUCTION [Qout/Qin](%)= 3.209
01728> TIME SHIFT OF PEAK FLOW (min)= 79.00
01729> MAXIMUM STORAGE USED (ha.m.)=.2851E+00
01730>
01731>
01732> 001:0077-----
01733>
01734> | DIVERT HYD |
01735> | INID=01 (SWMF ) |
01736>
01737> Outflow / Inflow Relationships
01738> Flow 03 + Flow 04 + Flow 05 = Total
01739> (cms) (cms) (cms)
01740> .000 .000 .000
01741> .000 .059 .000
01742> .007 .061 .000
01743> .007 .063 .000
01744> .008 .064 .000
01745> .008 .065 .000
01746> .008 .066 .000
01747> .009 .068 .000
01748> .009 .069 .000
01749> .009 .070 .000
01750> .009 .071 .000
01751> .010 .072 .000
01752> .010 .073 .000
01753> .010 .074 .000
01754> .010 .075 .000
01755> .011 .077 .000

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	01756>	.011	.078	.210	.299
01757>	NHYD	AREA	QPEAK	TpeakDate_hh:mm	R.V. NFE WetHrs
01758>	(ha)	(cms)			(mm) (hrs)
01759>	IDin= 01:SWMF	12.24	.112	No_date 2:19	36.375 1 158.
01760>	=====				
01761>	Ibowl= 03:Infilt	1	.011	No_date 2:19	36.375 1 12.
01762>	Input= 04:Orific	10.88	.07	No_date 2:19	36.375 1 158.
01763>	IDout= 05:Exurge	.31	.024	No_date 2:19	36.375 1 2.
01764>	=====				
01765>	001:0078-----				
01766>	******				
01767>	*#*****				
01768> #*					50-year
01769> #*					=====
01770> #*					
01771> #*					
01772> #*****					
01773> CHICAGO STORM IDF curve parameters: A=1499.060					
01774> ----- Ptotal= 66.11 mm					
01775>	B= 4.188				
01776>	C= .809				
01777>	used in: INTENSITY = A / (t + b)^c				
01778>	Duration of storm = 3.00 hrs				
01779>	Storm time step = 5.00 min				
01780>	Time to peak ratio = .33				
01781>	=====				
01782>	TIME RAIN TIME RAIN TIME RAIN TIME RAIN TIME RAIN				
01783>	hrs mm/hr hrs mm/hr hrs mm/hr hrs mm/hr hrs mm/hr				
01784>	.06 5.648 .82 21.93 1.58 14.045 2.33 6.561				
01785>	.08 5.648 .82 21.93 1.58 14.045 2.33 6.561				
01786>	.17 5.501 .92 68.75 1.67 12.381 2.42 6.216				
01787>	.25 6.054 1.00 249.214 1.75 11.088 2.50 5.909				
01788>	.33 6.747 1.08 19.168 1.83 10.056 2.58 5.633				
01789>	.42 7.643 1.17 47.427 1.92 9.210 2.67 5.384				
01790>	.50 8.846 1.25 31.940 2.00 8.506 2.75 5.158				
01791>	.58 10.555 1.33 24.094 2.08 7.909 2.83 4.952				
01792>	.67 13.195 1.42 19.393 2.17 7.396 2.92 4.763				
01793>	.75 17.800 1.50 16.269 2.25 6.951 3.00 4.590				
01794>	=====				
01795>	EXISTING CONDITIONS				
01796>	#*****				
01797> #*					
01798> #*					
01799> #*					
01800> #*					
01801> #*****					
01802>	CALIB NASHYD Area (ha)= 2.37 Curve Number (CN)=72.00				
01803> ----- Ia (mm)= 8.000 # of Linear Res.(N)= 3.00					
01804> ----- U.H. Tp(hrs)= .330					
01805>	=====				
01806>	Unit Hyd Qpeak (cms)= .274				
01807>	=====				
01808>	PEAK FLOW (cms)= .130 (i)				
01809>	TIME TO PEAK (hrs)= 1.433				
01810>	RUNOFF VOLUME (mm)= 21.525				
01811>	TOTAL RAINFALL (mm)= 66.112				
01812>	RUNOFF COEFFICIENT = .326				
01813>	=====				
01814>	(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.				
01815>	=====				
01816>	=====				
01817>	=====				
01818>	001:0080-----				
01819>	=====				
01820>	COMPUTE DUALHYD Average inlet capacities [CINLET] = .001 (cms)				
01821> ----- TotalHyd 01:EX-1 Number of inlets in system [NINLET] = 1					
01822> ----- Total minor system capacity = .001 (cms)					
01823> ----- Total major system storage [TMJSTO] = 99999. (cu.m.)					
01824>	=====				
01825>	ID: NYHD AREA QPEAK TPEAK R.V. DWF				
01826>	(ha) (cms) (hrs) (mm) (cms)				
01827>	TOTAL HYD. 01:EX-1 2.37 .130 1.433 21.525 .000				
01828>	=====				
01829>	MAJOR SYST 02:THAMES .00 .000 .000 .000 .000				
01830>	MINOR SYST 03:toDRAIN 2.37 .001 178.033 21.524 .000				
01831>	=====				
01832>	NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.				
01833>	=====				
01834>	Maximum MAJOR SYSTEM storage used = 500. (cu.m.)				
01835>	=====				
01836>	001:0081-----				
01837>	=====				
01838>	CALIB NASHYD Area (ha)= .19 Curve Number (CN)=74.00				
01839> ----- O1:EX-2 DT= 1.00 Ia (mm)= 5.000 # of Linear Res.(N)= 3.00					
01840> ----- U.H. Tp(hrs)= .090					
01841>	=====				
01842>	Unit Hyd Qpeak (cms)= .081				
01843>	=====				
01844>	PEAK FLOW (cms)= .027 (i)				
01845>	TIME TO PEAK (hrs)= 1.083				
01846>	RUNOFF VOLUME (mm)= 24.839				
01847>	TOTAL RAINFALL (mm)= 66.112				
01848>	RUNOFF COEFFICIENT = .376				
01849>	=====				
01850>	(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.				
01851>	=====				
01852>	=====				
01853>	=====				
01854> 001:0082-----					
01855>	=====				
01856>	CALIB STANDHYD Area (ha)= .45				
01857> ----- 04:EX-3 DT= 1.00 Total Imp(%)= 65.00 Dir. Conn.(%)= 1.00					
01858>	=====				
01859>	IMPERVIOUS PERVERIOUS (i)				
01860>	Surface Area (ha)= .29 .16				
01861>	Dep. Storage (mm)= 2.00 8.00				
01862>	Average Slope (%)= 1.00 20.00				
01863>	Length (m)= 5.00 25.00				
01864>	Manning's n = .013 .240				
01865>	Max.eff.Inten.(mm/hr)= 249.21 491.16				
01866>	over (min) 1.00 2.00				
01867>	Storage Coeff. (min)= .29 (ii) 1.67 (ii)				
01868>	Unit Hyd. Peak (min)= 1.00 2.00				
01869>	Unit Hyd. peak (cms)= 1.64 .62				
01870>	=====				
01871>	PEAK FLOW (cms)= .00 .19 .19 (iii)				
01872>	TIME TO PEAK (hrs)= .98 1.00 1.00				
01873>	RUNOFF VOLUME (mm)= 64.11 40.78 41.014				
01874>	TOTAL RAINFALL (mm)= 66.11 66.11 66.112				
01875>	RUNOFF COEFFICIENT = .97 .62 .620				
01876>	=====				
01877>	(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:				
01878>	CN* = 72.0 Ia = Dep. Storage (Above)				
01879>	(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL				
01880>	THAN THE STORAGE COEFFICIENT.				
01881>	(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.				
01882>	=====				
01883>	=====				
01884>	=====				
01885> 001:0083-----					
01886>	=====				
01887>	CALIB NASHYD Area (ha)= 2.59 Curve Number (CN)=67.00				
01888> ----- 05:EX-4 DT= 1.00 Ia (mm)= 8.000 # of Linear Res.(N)= 3.00					
01889>	=====				
01890>	U.H. Tp(hrs)= .230				

01891>	Unit Hyd Qpeak (cms)=	.430
01892>	PEAK FLOW (cms)=	.151 (i)
01893>	TIME TO PEAK (hrs)=	1.300
01894>	RUNOFF VOLUME (mm)=	18.432
01895>	TOTAL RAINFALL (mm)=	66.112
01896>	RUNOFF COEFFICIENT =	.279
01897>	(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.	
01898>		
01899>	001:0084-----	
01900>	-----	
01901>	-----	
01902>	001:0084-----	
01903>	-----	
01904>	I COMPUTE DUALHYD Average inlet capacities [CINLET] = .001 (cms)	
01905>	TotalHyd 05:EX-4 Number of inlets in system [NINLET] = 1	
01906>	----- Total major system capacity = .001 (cms)	
01907>	Total major system storage [TMJSTO] = 99999. (cu.m.)	
01893>	ID: NYHD AREA QPEAK TPEAK R.V. DWF	
01910>	(ha) (cms) (hrs) (mm) (cms)	
01911>	TOTAL HYD. 05:EX-4 2.59 .151 1.300 18.432 .000	
01912>	=====	
01913>	MAJOR SYST 06:BANNAN .00 .000 .000 .000 .000	
01914>	MINOR SYST 07:odRAI 2.59 .001 166.633 18.430 .000	
01915>		
01916>	NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.	
01917>		
01918>	Maximum MAJOR SYSTEM storage used = 469. (cu.m.)	
01919>		
01920>		
01921>	001:0085-----	
01922>	-----	
01923>	I CALIB NASHFD Area (ha)= 6.64 Curve Number (CN)=72.00	
01924>	05:C101 DT= 1.00 Ia (mm)= 8.000 # of Linear Res.(N)= 3.00	
01925>	U.H. Tp(hrs)= .310	
01926>		
01927>	Unit Hyd Qpeak (cms)= .818	
01928>		
01929>	PEAK FLOW (cms)= .379 (i)	
01930>	TIME TO PEAK (hrs)= 1.400	
01931>	RUNOFF VOLUME (mm)= 21.525	
01932>	TOTAL RAINFALL (mm)= 66.112	
01933>	RUNOFF COEFFICIENT = .326	
01934>	(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.	
01935>		
01936>		
01937>	001:0086-----	
01938>	-----	
01939>	-----	
01940>	I ADD HYD (PRE) ID: NYHD AREA QPEAK TPEAK R.V. DWF	
01941>	(ha) (cms) (hrs) (mm) (cms)	
01942>	ID1 01:EX-2 1.19 .027 1.08 24.84 .000	
01943>	+ID2 08:toDRAIN 2.37 .001 178.03 21.52 .000	
01944>	+ID3 04:EX-3 .45 .001 1.00 41.01 .000	
01945>	+ID4 05:C101 6.64 .379 1.40 21.52 .000	
01946>	+ID5 07:toDRAIN 2.59 .001 166.63 18.43 .000	
01947>	=====	
01948>	SUM 08:PRE 12.24 .410 1.38 21.64 .000	
01949>		
01950>	NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.	
01951>		
01952>		
01953>	001:0087-----	
01954>	-----	
01955>	I PRINT HYD AREA (ha)= 12.240	
01956>	ID=08 (PRE) QPEAK (cms)= .410 (i)	
01957>	DT= 1.00 PCYC= 5 TPEAK (hrs)= 1.383	
01958>	VOLUME (mm)= 21.640	
01959>		
01960>	(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.	
01961>	TIME FLOW TIME FLOW TIME FLOW TIME FLOW TIME FLOW TIME FLOW	
01962>	hrs cms hrs cms hrs cms hrs cms hrs cms hrs cms	
01963>	.00 .000 55.67 .002 71.33 .000 107.01 .002 146.58 .002	
01964>	.08 .000 35.75 .002 71.42 .000 107.09 .002 146.76 .002	
01965>	.00 .000 35.83 .002 71.50 .000 107.18 .002 146.84 .002	
01966>	.25 .000 35.92 .002 71.58 .000 107.26 .002 146.93 .002	
01967>	.33 .000 36.00 .002 71.67 .000 107.34 .002 143.01 .002	
01968>	.42 .000 36.08 .002 71.75 .000 107.43 .002 143.06 .002	
01969>	.50 .000 36.17 .002 71.83 .000 107.51 .002 143.18 .002	
01970>	.58 .001 36.25 .002 71.92 .000 107.59 .002 143.24 .002	
01971>	.67 .002 36.33 .002 72.00 .000 107.68 .002 143.34 .002	
01972>	.75 .004 36.42 .002 72.08 .000 107.76 .002 143.43 .002	
01973>	.83 .009 36.50 .002 72.17 .000 107.84 .002 143.51 .002	
01974>	.92 .000 36.58 .002 72.25 .000 107.93 .002 143.59 .002	
01975>	1.00 .000 238.67 .002 72.33 .000 108.01 .002 143.68 .002	
01976>	1.08 .000 36.75 .002 72.42 .000 108.09 .002 143.76 .002	
01977>	1.17 .000 36.83 .002 72.50 .000 108.18 .002 143.84 .002	
01978>	1.25 .000 36.92 .002 72.58 .000 108.26 .002 143.93 .002	
01979>	1.33 .000 37.00 .002 72.67 .000 108.34 .002 144.01 .002	
01980>	1.42 .008 37.08 .002 72.75 .000 108.43 .002 144.09 .002	
01981>	1.50 .000 37.17 .002 72.83 .000 108.51 .002 144.18 .002	
01982>	1.58 .000 37.25 .002 72.92 .000 108.59 .002 144.26 .002	
01983>	1.67 .000 37.33 .002 73.00 .000 108.68 .002 144.34 .002	
01984>	1.75 .000 37.42 .002 73.08 .000 108.76 .002 144.43 .002	
01985>	1.83 .000 245.50 .002 73.17 .000 108.84 .002 144.50 .002	
01986>	1.92 .000 245.57 .002 73.25 .000 108.93 .002 144.59 .002	
01987>	2.00 .000 188.37 .002 73.33 .000 109.01 .002 144.68 .002	
01988>	2.08 .000 166.11 .002 73.42 .000 109.09 .002 144.76 .002	
01989>	2.17 .000 148.37 .002 73.50 .000 109.18 .002 144.84 .002	
01990>	2.25 .000 133.37 .002 73.58 .000 109.26 .002 144.93 .002	
01991>	2.33 .000 121.38 .002 73.67 .000 109.34 .002 145.01 .002	
01992>	2.42 .000 111.38 .002 73.75 .000 109.43 .002 145.05 .002	
01993>	2.50 .000 102.38 .002 73.83 .000 109.51 .002 145.18 .002	
01994>	2.58 .095 38.25 .002 73.92 .000 109.59 .002 145.24 .002	
01995>	2.67 .089 38.33 .002 74.00 .000 109.68 .002 145.34 .002	
01996>	2.75 .083 38.32 .002 74.08 .000 109.76 .002 145.43 .002	
01997>	2.73 .081 38.30 .002 74.17 .000 109.84 .002 145.52 .002	
01998>	2.92 .075 38.58 .002 74.25 .000 109.93 .002 145.59 .002	
01999>	3.00 .071 38.67 .002 74.33 .000 110.01 .002 145.68 .002	
02000>	3.08 .062 38.75 .002 74.42 .000 110.09 .002 145.76 .002	
02001>	3.17 .055 38.83 .002 74.50 .000 110.18 .002 145.84 .002	
02002>	3.25 .046 38.92 .002 74.58 .000 110.26 .002 145.93 .002	
02003>	3.33 .037 39.00 .002 74.67 .000 110.34 .002 146.01 .002	
02004>	3.42 .029 39.08 .002 74.75 .000 110.43 .002 146.09 .002	
02005>	3.50 .022 39.17 .002 74.83 .000 110.51 .002 146.16 .002	
02006>	3.58 .016 39.25 .002 74.92 .000 110.59 .002 146.26 .002	
02007>	3.67 .010 39.33 .002 75.00 .000 110.68 .002 146.34 .002	
02008>	3.75 .009 39.32 .002 75.08 .000 110.66 .002 146.42 .002	
02009>	3.83 .007 39.30 .002 75.17 .000 110.84 .002 146.51 .002	
02010>	3.92 .005 39.58 .002 75.25 .000 110.93 .002 146.59 .002	
02011>	4.00 .004 39.67 .002 75.33 .000 111.01 .002 146.67 .002	
02012>	4.08 .003 39.75 .002 75.42 .000 111.09 .002 146.76 .002	
02013>	4.17 .003 39.83 .002 75.50 .000 111.18 .002 146.84 .002	
02014>	4.25 .002 39.92 .002 75.58 .000 111.26 .002 146.92 .002	
02015>	4.33 .002 40.00 .002 75.67 .000 111.34 .002 147.01 .002	
02016>	4.42 .002 40.08 .002 75.75 .000 111.43 .002 147.09 .002	
02017>	4.50 .002 40.17 .002 75.84 .000 111.51 .002 147.17 .002	
02018>	4.58 .002 40.25 .002 75.92 .000 111.59 .002 147.25 .002	
02019>	4.67 .002 40.33 .002 76.00 .000 111.68 .002 147.34 .002	
02020>	4.75 .002 40.42 .002 76.09 .000 111.66 .002 147.42 .002	
02021>	4.83 .002 40.50 .002 76.17 .000 111.84 .002 147.51 .002	
02022>	4.92 .002 40.58 .002 76.25 .000 111.93 .002 147.59 .002	
02023>	5.00 .002 40.67 .002 76.34 .000 112.01 .002 147.67 .002	
02024>	5.08 .002 40.75 .002 76.42 .000 112.09 .002 147.76 .002	
02025>	5.17 .002 40.83 .002 76.50 .000 112.18 .002 147.84 .002	
02026>	5.25 .002 40.92 .002 76.59 .000 112.26 .002 147.92 .002	
02027>	5.33 .002 41.00 .002 76.67 .000 112.34 .002 148.01 .002	
02028>	5.42 .002 41.08 .002 76.75 .000 112.43 .002 148.09 .002	
02029>	5.50 .002 41.17 .002 76.84 .000 112.51 .002 148.17 .002	
02030>	5.58 .002 41.25 .002 76.92 .000 112.59 .002 148.26 .002	
02031>	5.67 .002 41.33 .002 77.00 .000 112.68 .002 148.34 .002	
02032>	5.75 .002 41.42 .002 77.09 .000 112.76 .002 148.42 .002	
02033>	5.83 .002 41.50 .002 77.17 .000 112.84 .002 148.51 .002	
02034>	5.92 .002 41.58 .002 77.25 .000 112.93 .002 148.59 .002	
02035>	6.00 .002 41.67 .002 77.34 .000 113.01 .002 148.67 .002	
02036>	6.08 .002 41.75 .002 77.42 .000 113.09 .002 148.76 .002	
02037>	6.17 .002 41.83 .002 77.50 .000 113.17 .002 148.84 .002	
02038>	6.25 .002 41.92 .002 77.59 .000 113.24 .002 148.92 .002	
02039>	6.33 .002 42.00 .002 77.67 .000 113.34 .002 149.01 .002	
02040>	6.42 .002 42.08 .002 77.75 .000 113.43 .002 149.09 .002	
02041>	6.50 .002 42.17 .002 77.84 .000 113.51 .002 149.17 .002	
02042>	6.58 .002 42.25 .002 77.92 .000 113.59 .002 149.26 .002	
02043>	6.67 .002 42.33 .002 77.98 .000 113.67 .002 149.34 .002	
02044>	6.75 .002 42.42 .002 78.09 .000 113.76 .002 149.42 .002	
02045>	6.83 .002 42.50 .002 78.17 .000 113.84 .002 149.51 .002	
02046>	6.92 .002 42.58 .002 78.25 .000 113.93 .002 149.59 .002	
02047>	7.00 .002 42.67 .002 78.34 .000 114.01 .002 149.67 .002	
02048>	7.08 .002 42.75 .002 78.42 .000 114.09 .002 149.75 .002	
02049>	7.17 .002 42.83 .002 78.50 .000 114.18 .002 149.84 .002	
02050>	7.25 .002 42.92 .002 78.59 .000 114.26 .002 149.92 .002	
02051>	7.33 .002 43.00 .002 78.67 .000 114.34 .002 150.01 .002	
02052>	7.42 .002 43.08 .002 78.75 .000 114.43 .002 150.09 .002	
02053>	7.50 .002 43.17 .002 78.84 .000 114.50 .002 150.17 .002	
02054>	7.58 .002 43.25 .002 78.92 .000 114.59 .002 150.26 .002	
02055>	7.67 .002 43.33 .002 79.03 .000 114.67 .002 150.34 .002	
02056>	7.75 .002 43.42 .002 79.11 .000 114.75 .002 150.42 .002	
02057>	7.83 .002 43.50 .002 79.19 .000 114.83 .002 150.50 .002	
02058>	7.92 .002 43.58 .002 79.25 .000 114.91 .002 150.59 .002	
02059>	8.00 .002 43.67 .002 79.34 .000 114.99 .002 150.67 .002	
02060>	8.08 .002 43.75 .002 79.42 .000 115.09 .002 150.76 .002	
02061>	8.17 .002 43.83 .002 79.50 .000 115.18 .002 150.84 .002	
02062>	8.25 .002 43.92 .002 79.59 .000 115.26 .002 150.92 .002	
02063>	8.33 .002 44.00 .002 79.67 .000 115.34 .002 150.99 .002	
02064>	8.42 .002 44.08 .002 79.75 .000 115.43 .002 151.09 .002	
02065>	8.50 .002 44.17 .002 79.84 .000 115.50 .002 151.17 .002	
02066>	8.58 .002 44.25 .002 79.92 .000 115.59 .002 151.26 .002	
02067>	8.67 .002 44.33 .002 80.00 .000 115.68 .002 151.34 .002	
02068>	8.75 .002 44.42 .002 80.09 .000 115.76 .002 151.42 .002	
02069>	8.83 .002 44.50 .002 80.17 .000 115.84 .002 151.51 .002	
02070>	8.92 .002 44.58 .002 80.25 .000 115.93 .002 151.59 .002	
02071>	9.00 .002 44.67 .002 80.34 .000 116.01 .002 151.67 .002	
02072>	9.08 .002 44.75 .002 80.42 .000 116.09 .002 151.76 .002	
02073>	9.17 .002 44.83 .002 80.50 .000 116.18 .002 151.84 .002	
02074>	9.25 .002 44.92 .002 80.59 .000 116.26 .002 151.92 .002	
02075>	9.33 .002 45.00 .002 80.67 .000 116.34 .002 152.01 .002	
02076>	9.42 .002 45.08 .002 80.74 .000 116.43 .002 152.09 .002	
02077>	9.50 .002 45.17 .002	

02161>	16.50	.002	52.17	.002	87.84	.002	123.51	.002	159.17	.002	02296>	27.75	.002	63.42	.002	99.09	.002	134.76	.002	170.42	.001
02162>	16.58	.002	52.25	.002	87.92	.002	123.60	.002	159.26	.002	02298>	27.83	.002	63.50	.002	99.17	.002	134.84	.002	170.50	.001
02163>	16.67	.002	52.33	.002	88.00	.002	123.68	.002	159.34	.002	02299>	27.92	.002	63.58	.002	99.26	.002	134.93	.002	170.59	.001
02164>	16.75	.002	52.42	.002	88.09	.002	123.76	.002	159.42	.002	02300>	28.00	.002	63.67	.002	99.34	.002	135.01	.002	170.67	.001
02165>	16.83	.002	52.50	.002	88.17	.002	123.85	.002	159.51	.002	02301>	28.17	.002	63.75	.002	99.42	.002	135.09	.002	170.75	.001
02166>	16.92	.002	52.58	.002	88.25	.002	123.93	.002	159.59	.002	02302>	28.34	.002	63.83	.002	99.51	.002	135.18	.002	170.84	.001
02167>	17.00	.002	52.67	.002	88.34	.002	124.01	.002	159.67	.002	02303>	28.51	.002	63.92	.002	99.59	.002	135.26	.002	170.93	.001
02168>	17.08	.002	52.75	.002	88.42	.002	124.09	.002	159.75	.002	02304>	28.68	.002	64.00	.002	99.67	.002	135.34	.002	171.00	.001
02169>	17.17	.002	52.83	.002	88.50	.002	124.18	.002	159.84	.002	02305>	28.84	.002	64.17	.002	99.74	.002	135.51	.002	171.17	.001
02170>	17.25	.002	52.92	.002	88.59	.002	124.26	.002	159.92	.002	02306>	28.90	.002	64.25	.002	99.92	.002	135.59	.002	171.25	.001
02171>	17.33	.002	53.00	.002	88.67	.002	124.35	.002	160.01	.002	02307>	28.67	.002	64.33	.002	100.01	.002	135.68	.002	171.34	.001
02172>	17.42	.002	53.08	.002	88.75	.002	124.43	.002	160.01	.002	02308>	28.75	.002	64.42	.002	100.09	.002	135.76	.002	171.42	.001
02173>	17.50	.002	53.17	.002	88.84	.002	124.51	.002	160.17	.002	02309>	28.83	.002	64.50	.002	100.17	.002	135.84	.002	171.50	.001
02174>	17.58	.002	53.25	.002	88.92	.002	124.60	.002	160.25	.002	02310>	28.92	.002	64.58	.002	100.26	.002	135.93	.002	171.59	.001
02175>	17.67	.002	53.33	.002	89.00	.002	124.68	.002	160.34	.002	02311>	29.00	.002	64.67	.002	100.34	.002	136.01	.002	171.67	.001
02176>	17.75	.002	53.42	.002	89.09	.002	124.76	.002	160.42	.002	02312>	29.08	.002	64.75	.002	100.42	.002	136.09	.002	171.75	.001
02177>	17.83	.002	53.50	.002	89.17	.002	124.85	.002	160.50	.002	02313>	29.17	.002	64.83	.002	100.51	.002	136.17	.002	171.83	.001
02178>	17.92	.002	53.58	.002	89.25	.002	124.93	.002	160.58	.002	02314>	29.25	.002	64.92	.002	100.59	.002	136.26	.002	171.92	.001
02179>	18.00	.002	53.67	.002	89.34	.002	125.01	.002	160.67	.002	02315>	29.33	.002	65.00	.002	100.67	.002	136.34	.002	172.00	.001
02180>	18.08	.002	53.75	.002	89.42	.002	125.10	.002	160.75	.002	02316>	29.42	.002	65.08	.002	100.76	.002	136.43	.002	172.09	.001
02181>	18.17	.002	53.83	.002	89.50	.002	125.18	.002	160.84	.002	02317>	29.50	.002	65.17	.002	100.84	.002	136.51	.002	172.17	.001
02182>	18.25	.002	53.92	.002	89.59	.002	125.26	.002	160.92	.002	02318>	29.58	.002	65.25	.002	100.92	.002	136.59	.002	172.25	.001
02183>	18.33	.002	54.00	.002	89.67	.002	125.35	.002	161.00	.002	02319>	29.67	.002	65.33	.002	101.01	.002	136.68	.002	172.34	.001
02184>	18.42	.002	54.08	.002	89.75	.002	125.43	.002	161.09	.002	02320>	29.75	.002	65.42	.002	101.09	.002	136.78	.002	172.42	.001
02185>	18.50	.002	54.17	.002	89.84	.002	125.51	.002	161.17	.002	02321>	29.83	.002	65.50	.002	101.17	.002	136.84	.002	172.50	.001
02186>	18.58	.002	54.25	.002	89.92	.002	125.60	.002	161.25	.002	02322>	29.92	.002	65.58	.002	101.26	.002	136.93	.002	172.59	.001
02187>	18.67	.002	54.33	.002	90.00	.002	125.68	.002	161.33	.002	02323>	30.00	.002	65.67	.002	101.34	.002	137.01	.002	172.67	.001
02188>	18.75	.002	54.42	.002	90.09	.002	125.76	.002	161.42	.002	02324>	30.08	.002	65.75	.002	101.42	.002	137.09	.002	172.75	.001
02189>	18.83	.002	54.50	.002	90.17	.002	125.84	.002	161.50	.002	02325>	30.17	.002	65.83	.002	101.50	.002	137.18	.002	172.83	.001
02190>	18.92	.002	54.58	.002	90.25	.002	125.92	.002	161.59	.002	02326>	30.25	.002	65.92	.002	101.59	.002	137.26	.002	172.92	.001
02191>	19.00	.002	54.67	.002	90.34	.002	126.01	.002	161.67	.002	02327>	30.33	.002	66.00	.002	101.67	.002	137.34	.002	173.00	.001
02192>	19.08	.002	54.75	.002	90.42	.002	126.10	.002	161.75	.002	02328>	30.42	.002	66.08	.002	101.76	.002	137.43	.002	173.09	.001
02193>	19.17	.002	54.83	.002	90.50	.002	126.18	.002	161.84	.002	02329>	30.50	.002	66.17	.002	101.84	.002	137.51	.002	173.17	.001
02194>	19.25	.002	54.92	.002	90.59	.002	126.26	.002	161.92	.002	02330>	30.58	.002	66.25	.002	101.92	.002	137.59	.002	173.25	.001
02195>	19.33	.002	55.00	.002	90.67	.002	126.35	.002	162.00	.002	02331>	30.67	.002	66.33	.002	102.01	.002	137.68	.002	173.34	.001
02196>	19.42	.002	55.08	.002	90.75	.002	126.43	.002	162.08	.002	02332>	30.75	.002	66.42	.002	102.09	.002	137.76	.002	173.42	.001
02197>	19.50	.002	55.17	.002	90.84	.002	126.51	.002	162.17	.002	02333>	30.83	.002	66.50	.002	102.17	.002	137.84	.002	173.50	.001
02198>	19.58	.002	55.25	.002	90.92	.002	126.60	.002	162.25	.002	02334>	30.92	.002	66.58	.002	102.26	.002	137.93	.002	173.59	.001
02199>	19.67	.002	55.33	.002	91.00	.002	126.68	.002	162.34	.002	02335>	31.00	.002	66.67	.002	102.34	.002	138.01	.002	173.68	.001
02200>	19.75	.002	55.42	.002	91.09	.002	126.76	.002	162.42	.002	02336>	31.08	.002	66.75	.002	102.42	.002	138.09	.002	173.75	.001
02201>	19.83	.002	55.50	.002	91.17	.002	126.84	.002	162.50	.002	02337>	31.17	.002	66.83	.002	102.52	.002	138.18	.002	173.84	.001
02202>	20.00	.002	55.67	.002	91.34	.002	127.01	.002	162.67	.002	02338>	31.25	.002	66.92	.002	102.67	.002	138.34	.002	174.00	.001
02203>	20.18	.002	55.75	.002	91.42	.002	127.10	.002	162.75	.002	02339>	31.33	.002	67.00	.002	102.76	.002	138.43	.002	174.08	.001
02204>	20.26	.002	55.83	.002	91.51	.002	127.18	.002	162.84	.002	02340>	31.42	.002	67.08	.002	102.84	.002	138.51	.002	174.17	.001
02205>	20.34	.002	55.91	.002	91.59	.002	127.26	.002	162.92	.002	02341>	31.50	.002	67.17	.002	102.92	.002	138.59	.002	174.25	.001
02206>	20.42	.002	55.98	.002	91.67	.002	127.34	.002	163.00	.002	02342>	31.58	.002	67.25	.002	102.92	.002	138.68	.002	174.33	.001
02207>	20.50	.002	56.06	.002	91.75	.002	127.42	.002	163.08	.002	02343>	31.66	.002	67.33	.002	103.01	.002	138.76	.002	174.42	.001
02208>	20.58	.002	56.14	.002	91.83	.002	127.50	.002	163.16	.002	02344>	31.74	.002	67.42	.002	103.09	.002	138.84	.002	174.50	.001
02209>	20.66	.002	56.22	.002	91.91	.002	127.58	.002	163.24	.002	02345>	31.82	.002	67.50	.002	103.17	.002	138.93	.002	174.58	.001
02210>	20.74	.002	56.30	.002	91.99	.002	127.66	.002	163.32	.0											

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02431>
02432> -----
02433> 001:0090-----
02434> -----
02435> | CALIB NASHYD | Area (ha)= .19 Curve Number (CN)=74.00
02436> | 01:EX-2 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res.(N)= 3.00
02437> -----
02438> U.H. Tp(hrs)= .090
02439> Unit Hyd Ppeak (cms)= .081
02440>
02441> PEAK FLOW (cms)= .027 (i)
02442> TIME TO PEAK (hrs)= 1.083
02443> RUNOFF VOLUME (mm)= 24.839
02444> TOTAL RAINFALL (mm)= 66.112
02445> RUNOFF COEFFICIENT = .376
02446>
02447> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02448>
02449> -----
02450> 001:0091-----
02451> -----
02452> | CALIB STANDHYD | Area (ha)= .45
02453> | 04:EX-3 DT= 1.00 | Total Imp(%)= 65.00 Dir. Conn. (%)= 1.00
02454>
02455> IMPERVIOUS PERVIOUS (i)
02456> Surface Area (ha)= .29 .16
02457> Dep. Storage (mm)= 2.00 8.00
02458> Average Slope (%)= 1.00 20.00
02459> Length (m)= 5.00 25.00
02460> Mannings n = .013 .240
02461>
02462> Max.eff.Inten.(mm/hr)= 249.21 491.16
02463> over (min)= 1.00 2.00
02464> Storage Coeff. (min)= .29 (ii) 1.67 (ii)
02465> Unit Hyd. Tpeak (min)= 1.00 2.00
02466> Unit Hyd. peak (cms)= 1.64 .62
02467> *TOTALS*
02468> PEAK FLOW (cms)= .00 .19 .191 (iii)
02469> TIME TO PEAK (hrs)= .98 1.00 1.000
02470> RUNOFF VOLUME (mm)= 64.11 40.78 41.04
02471> TOTAL RAINFALL (mm)= 66.11 66.11 66.112
02472> RUNOFF COEFFICIENT = .97 .62 .620
02473>
02474> (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:
02475> CN* = 72.0 Ia = Dep. Storage (Above)
02476> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
02477> THAN THE STORAGE COEFFICIENT.
02478> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02479>
02480>
02481> -----
02482> 001:0092-----
02483> -----
02484> | CALIB NASHYD | Area (ha)= 2.59 Curve Number (CN)=67.00
02485> | 05:EX-4 DT= 1.00 | Ia (mm)= 8.000 # of Linear Res.(N)= 3.00
02486> U.H. Tp(hrs)= .230
02487> Unit Hyd Ppeak (cms)= .430
02488>
02489> PEAK FLOW (cms)= .151 (i)
02490> TIME TO PEAK (hrs)= 1.300
02491> RUNOFF VOLUME (mm)= 18.432
02492> TOTAL RAINFALL (mm)= 66.112
02493> RUNOFF COEFFICIENT = .279
02494>
02495> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02496>
02497> -----
02498> 001:0093-----
02499> -----
02500> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .001 (cms)
02501> | TotalHyd 05:EX-4 | Number of inlets in system [NINLET] = 1
02502> -----
02503> Total minor system capacity = .001 (cms)
02504> Total major system storage [TMJSTO] = 99999.0(cu.m.)
02505> ID: NYHD AREA QPEAK TPPEAK R.V. DWF
02506> (ha) (cms) (hrs) (mm) (cms)
02507> TOTAL HYD 05:EX-4 2.59 151 1.300 18.432 .000
02508> =====
02509> MAJOR SYST 06:BANMAN .00 .000 .000 .000
02510> MINOR SYST 07:toDRAI 2.59 .001 166.633 18.430 .000
02511>
02512> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
02513>
02514> Maximum MAJOR SYSTEM storage used = 469.0(cu.m.)
02515>
02516>
02517> 001:0094-----
02518> -----
02519> | CALIB STANDHYD | Area (ha)= 6.64
02520> | 05:C201 DT= 1.00 | Total Imp(%)= 90.00 Dir. Conn. (%)= 80.00
02521>
02522> IMPERVIOUS PERVIOUS (i)
02523> Surface Area (ha)= 5.98 .66
02524> Dep. Storage (mm)= 2.00 5.00
02525> Average Slope (%)= 1.00 2.00
02526> Length (m)= 50.00 25.00
02527> Mannings n = .013 .250
02528>
02529> Max.eff.Inten.(mm/hr)= 249.21 191.11
02530> over (min)= 1.00 5.00
02531> Storage Coeff. (min)= 1.17 (ii) 5.28 (ii)
02532> Unit Hyd. Tpeak (min)= 1.00 5.00
02533> Unit Hyd. peak (cms)= .98 .22
02534> *TOTALS*
02535> PEAK FLOW (cms)= 3.64 .22 3.786 (iii)
02536> TIME TO PEAK (hrs)= 1.00 1.07 1.000
02537> RUNOFF VOLUME (mm)= 64.11 27.94 56.879
02538> TOTAL RAINFALL (mm)= 66.11 66.11 66.112
02539> RUNOFF COEFFICIENT = .97 .42 .860
02540>
02541> (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:
02542> CN* = 61.0 Ia = Dep. Storage (Above)
02543> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
02544> THAN THE STORAGE COEFFICIENT.
02545> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
02546>
02547>
02548> 001:0095-----
02549> -----
02550> | ADD HYD (POST ) | ID: NYHD AREA QPEAK TPPEAK R.V. DWF
02551> | (ha) (cms) (hrs) (mm) (cms)
02552> | ID1 01:EX-2 .19 .027 1.08 24.84 .000
02553> | +ID2 03:toDRAIN 2.37 .001 178.03 21.52 .000
02554> | +ID3 04:EX-3 .45 .191 1.00 41.01 .000
02555> | +ID4 05:C201 6.64 3.786 1.00 56.88 .000
02556> | +ID5 07:toDRAIN 2.59 .001 166.63 18.43 .000
02557> -----
02558> SUM 09:POST 12.24 3.994 1.00 40.80 .000
02559>
02560> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
02561>
02562>
02563> 001:0096-----
02564>
02565> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.

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(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

02701>
 02702>-----
 02703> 001:0101-----
 02704>
 02705> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .001 (cms)
 02706> | TotalHyd 01:EX-1 | Number of inlets in system [NINLET] = 1
 02707>-----
 02708> Total minor system capacity = .001 (cms)
 02709> Total major system storage [TMJSTO] = 99999. (cu.m.)
 02709>
 02710> ID: NYHD AREA QPEAK TPEAK R.V. DWF
 02711> (ha) (cms) (hrs) (mm) (cms)
 02712> TOTAL HYD. 01:EX-1 2.37 .151 1.417 25.031 .000
 02713>=====-----
 02714> MAJOR SYST 02:THAMES .00 .000 .000 .000 .000
 02715> MINOR SYST 03:todRAI 2.37 .001 206.867 25.031 .000
 02716>
 02717> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
 02718>
 02719> Maximum MAJOR SYSTEM storage used = 583. (cu.m.)
 02720>
 02721>-----
 02722> 001:0102-----
 02723>-----
 02724> | CALIB NASHYD | Area (ha)= .19 Curve Number (CN)=74.00
 02725> | 01:EX-2 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res.(N)= 3.00
 02726> U.H. Tp(hrs)= .090
 02727>
 02728> Unit Hyd Qpeak (cms)= .081
 02729>
 02730> PEAK FLOW (cms)= .032 (i)
 02731> TIME TO PEAK (hrs)= 1.083
 02732> RUNOFF VOLUME (mm)= 28.589
 02733> TOTAL RAINFALL (mm)= 71.791
 02734> RUNOFF COEFFICIENT = .398
 02735>
 02736> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
 02737>
 02738>-----
 02739> 001:0103-----
 02740>
 02741> | CALIB STANDHYD | Area (ha)= .45
 02742> | 04:EX-3 DT= 1.00 | Total Imp(%)= 65.00 Dir. Conn. (%)= 1.00
 02743>
 02744> IMPERVIOUS PERVIOUS (i)
 02745> Surface Area (ha)= .29 .16
 02746> Dep. Storage (mm)= 2.00 8.00
 02747> Average Slope (%)= 1.00 20.00
 02748> Length (m)= 5.00 25.00
 02749> Mannings n = .013 .240
 02750>
 02751> Max.eff.Inten.(mm/hr)= 279.47 571.98
 02752> Depth (mm) over (min)= 1.00 2.00
 02753> Storage Coeff. (min)= .28 (ii) 1.58 (iii)
 02754> Unit Hyd. Tpeak (min)= 1.00 2.00
 02755> Unit Hyd. peak (cms)= 1.65 .65
 02756> *TOTALS*
 02757> PEAK FLOW (cms)= .00 .22 .225 (iii)
 02758> TIME TO PEAK (hrs)= .98 1.00 1.000
 02759> RUNOFF VOLUME (mm)= 69.79 45.78 46.020
 02760> TOTAL RAINFALL (mm)= 71.79 71.791 71.791
 02761> RUNOFF COEFFICIENT = .97 .64 .641
 02762>
 02763> (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:
 02764> CN* = 72.0 Ia = Dep. Storage (Above)
 02765> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 02766> THAN THE STORAGE COEFFICIENT
 02767> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
 02768>
 02769>-----
 02770> 001:0104-----
 02771>
 02772> | CALIB NASHYD | Area (ha)= 2.59 Curve Number (CN)=67.00
 02773> | 05:EX-4 DT= 1.00 | Ia (mm)= 8.000 # of Linear Res.(N)= 3.00
 02774> U.H. Tp(hrs)= .230
 02775>
 02776> Unit Hyd Qpeak (cms)= .430
 02777>
 02778> PEAK FLOW (cms)= .177 (i)
 02779> TIME TO PEAK (hrs)= 1.283
 02780> RUNOFF VOLUME (mm)= 21.542
 02781> TOTAL RAINFALL (mm)= 71.791
 02782> RUNOFF COEFFICIENT = .300
 02783>
 02784> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
 02785>
 02786>
 02787> 001:0105-----
 02788>-----
 02789> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .001 (cms)
 02790> | TotalHyd 05:EX-4 | Number of inlets in system [NINLET] = 1
 02791>-----
 02792> Total minor system capacity = .001 (cms)
 02793> Total major system storage [TMJSTO] = 99999. (cu.m.)
 02794>
 02795> ID: NYHD AREA QPEAK TPEAK R.V. DWF
 02796> (ha) (cms) (hrs) (mm) (cms)
 02797> TOTAL HYD. 05:EX-4 2.59 .177 1.283 21.542 .000
 02798>
 02799> MAJOR SYST 06:BANNMAN .00 .000 .000 .000 .000
 02800> MINOR SYST 07:todRAI 2.59 .001 194.583 21.541 .000
 02801>
 02802> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
 02803>
 02804>-----
 02805> 001:0106-----
 02806>
 02807> | CALIB NASHYD | Area (ha)= 6.64 Curve Number (CN)=72.00
 02808> | 05:C101 DT= 1.00 | Ia (mm)= 8.000 # of Linear Res.(N)= 3.00
 02809> U.H. Tp(hrs)= .310
 02810>
 02811> Unit Hyd Qpeak (cms)= .818
 02812>
 02813> PEAK FLOW (cms)= .440 (i)
 02814> TIME TO PEAK (hrs)= 1.400
 02815> RUNOFF VOLUME (mm)= 25.031
 02816> TOTAL RAINFALL (mm)= 71.791
 02817> RUNOFF COEFFICIENT = .349
 02818>
 02819> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
 02820>
 02821>
 02822>-----
 02823> 001:0107-----
 02824>
 02825> | ADD HYD (PRE) | ID: NYHD AREA QPEAK TPEAK R.V. DWF
 02826> (ha) (cms) (hrs) (mm) (cms)
 02827> ID1 01:EX-2 .19 .032 1.08 28.59 .000
 02828> ID2 03:REINRAIN 2.37 .001 206.867 25.031 .000
 02829> ID3 04:EX-3 .45 .224 1.00 46.02 .000
 02830> ID4 05:C101 6.64 .440 1.40 25.03 .000
 02831> ID5 07:todRAIN 2.59 .001 194.58 21.54 .000
 02832>-----
 02833> SUM 08:PRE 12.24 .474 1.37 25.12 .000
 02834>
 02835> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

02836>
 02837>-----
 02838> 001:0108-----
 02839>
 02840> | PRINT HYD | AREA (ha)= 12.240
 02841> | ID=08 (PRE) | QPEAK (cms)= .474 (i)
 02842> | DT= 1.00 PCYC= 5 | TPEAK (hrs)= 1.367
 02843> |-----| VOLUME (mm)= 25.122
 02844>
 02845> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
 02846> TIME FLOW | TIME FLOW | TIME FLOW | TIME FLOW
 02847> hrs cms | hrs cms | hrs cms | hrs cms
 02848> .00 .000 41.42 .002 82.84 .002 124.26 .002 165.67 .002
 02849> .08 .000 41.50 .002 82.92 .002 124.35 .002 165.75 .002
 02850> .17 .000 41.58 .002 83.00 .002 124.43 .002 165.84 .002
 02851> .25 .000 41.67 .002 83.09 .002 124.50 .002 165.92 .002
 02852> .33 .000 41.75 .002 83.17 .002 124.60 .002 166.00 .002
 02853> .42 .000 41.83 .002 83.25 .002 124.68 .002 166.17 .002
 02854> .50 .000 41.92 .002 83.34 .002 124.76 .002 166.25 .002
 02855> .58 .001 42.00 .002 83.42 .002 124.84 .002 166.34 .002
 02856> .67 .003 42.08 .002 83.50 .002 124.93 .002 166.42 .002
 02857> .75 .005 42.17 .002 83.59 .002 125.01 .002 166.50 .002
 02858> .83 .011 42.25 .002 83.67 .002 125.10 .002 166.50 .002
 02859> .92 .024 42.33 .002 83.75 .002 125.18 .002 166.59 .002
 02860> 1.00 .0281 42.42 .002 83.84 .002 125.25 .002 166.67 .002
 02861> 1.08 .02881 42.50 .002 83.92 .002 125.35 .002 166.75 .002
 02862> 1.17 .0361 42.58 .002 84.00 .002 125.43 .002 166.84 .002
 02863> 1.25 .04371 42.67 .002 84.09 .002 125.51 .002 166.92 .002
 02864> 1.33 .05147 42.75 .002 84.17 .002 125.60 .002 167.00 .002
 02865> 1.42 .05914 42.83 .002 84.25 .002 125.68 .002 167.09 .002
 02866> 1.50 .06649 42.92 .002 84.34 .002 125.76 .002 167.17 .002
 02867> 1.58 .07407 43.00 .002 84.42 .002 125.85 .002 167.25 .002
 02868> 1.67 .08163 43.08 .002 84.50 .002 125.93 .002 167.34 .002
 02869> 1.75 .08919 43.17 .002 84.59 .002 126.01 .002 167.42 .002
 02870> 1.83 .09679 43.25 .002 84.67 .002 126.10 .002 167.50 .002
 02871> 1.92 .10441 43.33 .002 84.75 .002 126.18 .002 167.59 .002
 02872> 2.00 .11205 43.42 .002 84.84 .002 126.26 .002 167.67 .002
 02873> 2.09 .11960 43.50 .002 84.92 .002 126.34 .002 167.75 .002
 02874> 2.17 .12717 43.58 .002 85.00 .002 126.43 .002 167.83 .002
 02875> 2.25 .13472 43.67 .002 85.09 .002 126.51 .002 167.91 .002
 02876> 2.33 .14226 43.75 .002 85.17 .002 126.60 .002 168.00 .002
 02877> 2.42 .14980 43.83 .002 85.25 .002 126.68 .002 168.09 .002
 02878> 2.50 .15734 43.92 .002 85.34 .002 126.76 .002 168.17 .002
 02879> 2.58 .16488 43.99 .002 85.42 .002 126.85 .002 168.25 .002
 02880> 2.67 .17242 44.08 .002 85.50 .002 126.93 .002 168.34 .002
 02881> 2.75 .17996 44.17 .002 85.59 .002 127.01 .002 168.42 .002
 02882> 2.83 .18750 44.25 .002 85.67 .002 127.10 .002 168.50 .002
 02883> 2.92 .19504 44.33 .002 85.75 .002 127.18 .002 168.59 .002
 02884> 3.00 .20258 44.42 .002 85.84 .002 127.26 .002 168.67 .002
 02885> 3.08 .21012 44.50 .002 85.92 .002 127.35 .002 168.75 .002
 02886> 3.17 .21766 44.58 .002 86.00 .002 127.43 .002 168.83 .002
 02887> 3.25 .22520 44.67 .002 86.09 .002 127.51 .002 168.92 .002
 02888> 3.33 .23274 44.75 .002 86.17 .002 127.60 .002 168.99 .002
 02889> 3.42 .24028 44.83 .002 86.25 .002 127.68 .002 169.09 .002
 02890> 3.50 .24782 44.92 .002 86.34 .002 127.76 .002 169.17 .002
 02891> 3.58 .25536 45.00 .002 86.42 .002 127.85 .002 169.25 .002
 02892> 3.67 .26290 45.08 .002 86.50 .002 127.93 .002 169.34 .002
 02893> 3.75 .27044 45.17 .002 86.59 .002 128.01 .002 169.42 .002
 02894> 3.83 .27798 45.25 .002 86.67 .002 128.10 .002 169.50 .002
 02895> 3.92 .28552 45.33 .002 86.75 .002 128.18 .002 169.59 .002
 02896> 4.00 .29306 45.42 .002 86.84 .002 128.26 .002 169.67 .002
 02897> 4.08 .30060 45.50 .002 86.92 .002 128.34 .002 169.75 .002
 02898> 4.17 .30814 45.58 .002 86.99 .002 128.43 .002 169.82 .002
 02899> 4.25 .31568 45.67 .002 87.09 .002 128.51 .002 169.92 .002
 02900> 4.33 .32322 45.75 .002 87.17 .002 128.60 .002 170.00 .002
 02901> 4.42 .33076 45.83 .002 87.25 .002 128.68 .002 170.09 .002
 02902> 4.50 .33830 45.92 .002 87.34 .002 128.76 .002 170.17 .002
 02903> 4.58 .34584 46.00 .002 87.42 .002 128.85 .002 170.25 .002
 02904> 4.67 .35338 46.08 .002 87.50 .002 128.93 .002 170.34 .002
 02905> 4.75 .36092 46.17 .002 87.59 .002 129.01 .002 170.42 .002
 02906> 4.83 .36846 46.25 .002 87.67 .002 129.11 .002 170.50 .002
 02907> 4.92 .37600 46.33 .002 87.75 .002 129.18 .002 170.59 .002
 02908> 5.00 .38354 46.42 .002 87.83 .002 129.26 .002 170.68 .002
 02909> 5.08 .39108 46.50 .002 87.92 .002 129.35 .002 170.75 .002
 02910> 5.17 .39862 46.58 .002 88.00 .002 129.43 .002 170.84 .002
 02911> 5.25 .40616 46.67 .002 88.09 .002 129.51 .002 170.92 .002
 02912> 5.33 .41370 46.75 .002 88.17 .002 129.60 .002 171.00 .002
 02913> 5.42 .42124 46.83 .002 88.25 .002 129.68 .002 171.09 .002
 02914> 5.50 .42878 46.92 .002 88.34 .002 129.76 .002 171.17 .002
 02915> 5.58 .43632 47.00 .002 88.42 .002 129.85 .002 171.25 .002
 02916> 5.67 .44386 47.08 .002 88.50 .002 129.93 .002 171.34 .002
 02917> 5.75 .45140 47.17 .002 88.59 .002 130.01 .002 171.42 .002
 02918> 5.83 .45894 47.25 .002 88.67 .002 130.10 .002 171.50 .002
 02919> 5.92 .46648 47.33 .002 88.75 .002 130.18 .002 171.59 .002
 02920> 6.00 .47402 47.42 .002 88.84 .002 130.26 .002 171.67 .002
 02921> 6.08 .48156 47.50 .002 88.92 .002 130.35 .002 171.75 .002
 02922> 6.17 .48910 47.58 .002 88.99 .002 130.43 .002 171.84 .002
 02923> 6.25 .49664 47.67 .002 89.09 .002 130.51 .002 171.92 .002
 02924> 6.33 .50418 47.75 .002 89.17 .002 130.60 .002 172.00 .002
 02925> 6.42 .51172 47.83 .002 89.25 .002 130.68 .002 172.09 .002
 02926> 6.50 .51926 47.92 .002 89.34 .002 130.76 .002 172.17 .002
 02927> 6.58 .52680 48.00 .002 89.42 .002 130.85 .002 172.25 .002
 02928> 6.67 .53434 48.08 .002 89.50 .002 130.93 .002 172.34 .002
 02929> 6.75 .54188 48.17 .002 89.59 .002 131.01 .002 172.42 .002
 02930> 6.83 .54942 48.25 .002 89.67 .002 131.09 .002 172.50 .002
 02931> 6.92 .55696 48.33 .002 89.75 .002 131.18 .002 172.59 .002
 02932> 7.00 .56450 48.42 .002 89.84 .002 131.26 .002 172.67 .002
 02933> 7.08 .57204 48.50 .002 89.92 .002 131.35 .002 172.75 .002
 02934> 7.17 .57958 48.58 .002 90.00 .002 131.43 .002 172.84 .002
 02935> 7.25 .58712 48.67 .002 90.09 .002 131.51 .002 172.92 .002
 02936> 7.33 .59466 48.75 .002 90.17 .002 131.60 .002 173.00 .002
 02937> 7.42 .60220 48.83 .002 90.25 .002 131.68 .002 173.09 .002
 02938> 7.50 .60974 48.92 .002 90.34 .002 131.76 .002 173.17 .002
 02939> 7.58 .61728 49.00 .002 90.42 .002 131.85 .002 173.25 .002
 02940> 7.67 .62482 49.08 .002 90.50 .002 131.93 .002 173.34 .002
 02941> 7.75 .63236 49.17 .002 90.58 .002 132.01 .002 173.42 .002
 02942> 7.83 .64000 49.25 .002 90.67 .002 132.10 .002 173.50 .002
 02943> 7.92 .64754 49.33 .002 90.75 .002 132.18 .002 173.59 .002
 02944> 8.00 .65508 49.42 .002 90.84 .002 132.26 .002 173.67 .002
 02945> 8.08 .66262 49.50 .002 90.92 .002 132.35 .002 173.75 .002
 02946> 8.17 .67016 49.58 .002 91.00 .002 132.43 .002 173.84 .002
 02947> 8.25 .67770 49.67 .002 91.09 .002 132.51 .002 173.92 .002
 02948> 8.33 .68524 49.75 .002 91.17 .002 132.60 .002 174.00 .002
 02949> 8.42 .69278 49.83 .002 91.26 .002 132.68 .002 174.08 .002
 02950> 8.50 .70032 49.92 .002 91.34 .002 132.75 .002 174.17 .002
 02951> 8.58 .70786 50.00 .002 91.42 .002 132.85 .002 174.25 .002
 02952> 8.67 .71540 50.08 .002 91.50 .002 132.93 .002 174.33 .002
 02953> 8.75 .72294 50.16 .002 91.58 .002 133.01 .002 174.42 .002
 02954> 8.83 .73048 50.25 .002 91.67 .002 133.09 .002 174.50 .002
 02955> 8.92 .73792 50.33 .002 91.76 .002 133.18 .002 174.58 .002
 02956> 9.00 .74546 50.42 .002 91.84 .002 133.26 .002 174.67 .002
 02957> 9.08 .75299 50.50 .002 91.92 .002 133.34 .002 174.75 .002
 02958> 9.17 .76053 50.58 .002 92.01 .002 133.43 .002 174.83 .002
 02959> 9.25 .76807 50.67 .002 92.09 .002 133.51 .002 174.92 .002
 02960> 9.33 .77561 50.75 .002 92.17 .002 133.59 .002 175.00 .002
 02961> 9.42 .78315 50.83 .002 92.26 .002 133.66 .002 175.08 .002
 02962> 9.50 .79069 50.92 .002 92.34 .002 133.76 .002 175.17 .002
 02963> 9.58 .79823 51.00 .002 92.42 .002 133.84 .002 175.25 .002
 02964> 9.67 .80577 51.08 .002 92.51 .002 133.92 .002 175.33 .002
 02965> 9.75 .81331 51.17 .002 92.59 .002 133.99 .002 175.42 .002
 02966> 9.83 .82085 51.25 .002 92.67 .002 134.07 .002 175.50 .002
 02967> 9.92 .82839 51.33 .002 92.76 .002 134.18 .002 175.58 .002
 02968> 10.00 .83593 51.42 .002 92.84 .002 134.26 .002 175.67 .002
 02969> 10.08 .84347 51.50 .002 92.92 .

02971>	10.25	.002	51.67	.002	93.09	.002	134.51	.002	175.92	.002	03106>	21.50	.002	62.92	.002	104.34	.002	145.76	.002	187.17	.002
02972>	10.33	.002	51.75	.002	93.17	.002	134.59	.002	176.00	.002	03107>	21.58	.002	63.00	.002	104.42	.002	145.84	.002	187.25	.002
02973>	10.42	.002	51.83	.002	93.26	.002	134.68	.002	176.08	.002	03108>	21.67	.002	63.08	.002	104.51	.002	145.93	.002	187.33	.002
02974>	10.50	.002	51.92	.002	93.34	.002	134.76	.002	176.17	.002	03109>	21.75	.002	63.17	.002	104.59	.002	146.01	.002	187.42	.002
02975>	10.58	.002	52.00	.002	93.42	.002	134.84	.002	176.25	.002	03110>	21.83	.002	63.25	.002	104.67	.002	146.09	.002	187.50	.002
02976>	10.67	.002	52.08	.002	93.51	.002	134.93	.002	176.33	.002	03111>	21.92	.002	63.33	.002	104.76	.002	146.18	.002	187.58	.002
02977>	10.75	.002	52.16	.002	93.59	.002	135.01	.002	176.42	.002	03112>	22.01	.002	63.42	.002	104.84	.002	146.26	.002	187.65	.002
02978>	10.83	.002	52.25	.002	93.67	.002	135.09	.002	176.50	.002	03113>	22.08	.002	63.50	.002	104.92	.002	146.35	.002	187.75	.002
02979>	10.92	.002	52.33	.002	93.76	.002	134.18	.002	176.58	.002	03114>	22.17	.002	63.58	.002	105.01	.002	146.43	.002	187.83	.002
02980>	11.00	.002	52.42	.002	93.84	.002	135.26	.002	176.67	.002	03115>	22.25	.002	63.67	.002	105.09	.002	146.51	.002	187.91	.002
02981>	11.08	.002	52.50	.002	93.92	.002	135.34	.002	176.75	.002	03116>	22.33	.002	63.75	.002	105.17	.002	146.59	.002	188.00	.002
02982>	11.17	.002	52.58	.002	94.01	.002	135.43	.002	176.83	.002	03117>	22.42	.002	63.83	.002	105.26	.002	146.67	.002	188.08	.002
02983>	11.25	.002	52.67	.002	94.09	.002	135.51	.002	176.92	.002	03118>	22.50	.002	63.92	.002	105.34	.002	146.75	.002	188.16	.002
02984>	11.33	.002	52.75	.002	94.17	.002	135.59	.002	177.00	.002	03119>	22.58	.002	64.00	.002	105.42	.002	146.84	.002	188.25	.002
02985>	11.42	.002	52.83	.002	94.26	.002	135.68	.002	177.00	.002	03120>	22.67	.002	64.08	.002	105.51	.002	146.92	.002	188.33	.002
02986>	11.50	.002	52.92	.002	94.34	.002	135.76	.002	177.17	.002	03121>	22.75	.002	64.17	.002	105.59	.002	147.01	.002	188.41	.002
02987>	11.58	.002	53.00	.002	94.42	.002	135.84	.002	177.25	.002	03122>	22.83	.002	64.25	.002	105.67	.002	147.09	.002	188.50	.002
02988>	11.67	.002	53.08	.002	94.51	.002	135.93	.002	177.33	.002	03123>	22.91	.002	64.33	.002	105.75	.002	147.18	.002	188.58	.002
02989>	11.75	.002	53.17	.002	94.59	.002	135.99	.002	177.42	.002	03124>	23.00	.002	64.42	.002	105.84	.002	147.26	.002	188.66	.002
02990>	11.83	.002	53.25	.002	94.67	.002	136.09	.002	177.50	.002	03125>	23.08	.002	64.50	.002	105.92	.002	147.34	.002	188.75	.002
02991>	11.92	.002	53.33	.002	94.76	.002	136.18	.002	177.58	.002	03126>	23.17	.002	64.58	.002	106.01	.002	147.42	.002	188.83	.002
02992>	12.00	.002	53.42	.002	94.84	.002	136.26	.002	177.67	.002	03127>	23.25	.002	64.67	.002	106.09	.002	147.51	.002	188.91	.002
02993>	12.08	.002	53.50	.002	94.92	.002	136.34	.002	177.75	.002	03128>	23.33	.002	64.75	.002	106.17	.002	147.59	.002	188.99	.002
02994>	12.17	.002	53.58	.002	95.01	.002	136.43	.002	177.83	.002	03129>	23.42	.002	64.83	.002	106.26	.002	147.67	.002	189.08	.002
02995>	12.25	.002	53.67	.002	95.09	.002	136.51	.002	177.92	.002	03130>	23.50	.002	64.92	.002	106.34	.002	147.75	.002	189.16	.002
02996>	12.33	.002	53.75	.002	95.17	.002	136.59	.002	178.00	.002	03131>	23.58	.002	65.00	.002	106.42	.002	147.84	.002	189.25	.002
02997>	12.42	.002	53.83	.002	95.26	.002	136.68	.002	178.08	.002	03132>	23.67	.002	65.08	.002	106.51	.002	147.92	.002	189.33	.002
02998>	12.50	.002	53.92	.002	95.34	.002	136.76	.002	178.17	.002	03133>	23.75	.002	65.17	.002	106.59	.002	148.00	.002	189.41	.002
02999>	12.58	.002	54.00	.002	95.42	.002	136.84	.002	178.25	.002	03134>	23.83	.002	65.25	.002	106.67	.002	148.09	.002	189.50	.002
03000>	12.67	.002	54.08	.002	95.51	.002	136.93	.002	178.33	.002	03135>	23.92	.002	65.33	.002	106.76	.002	148.17	.002	189.58	.002
03001>	12.75	.002	54.17	.002	95.59	.002	137.01	.002	178.42	.002	03136>	24.00	.002	65.42	.002	106.84	.002	148.26	.002	189.66	.002
03002>	12.83	.002	54.25	.002	95.67	.002	137.09	.002	178.50	.002	03137>	24.08	.002	65.50	.002	106.93	.002	148.34	.002	189.75	.002
03003>	12.92	.002	54.33	.002	95.76	.002	137.18	.002	178.58	.002	03138>	24.17	.002	65.58	.002	107.01	.002	148.42	.002	189.83	.002
03004>	13.00	.002	54.42	.002	95.84	.002	137.26	.002	178.67	.002	03139>	24.25	.002	65.67	.002	107.09	.002	148.51	.002	189.91	.002
03005>	13.08	.002	54.50	.002	95.92	.002	137.34	.002	178.75	.002	03140>	24.33	.002	65.75	.002	107.18	.002	148.59	.002	190.00	.002
03006>	13.17	.002	54.58	.002	96.01	.002	137.43	.002	178.83	.002	03141>	24.42	.002	65.83	.002	107.26	.002	148.67	.002	190.08	.002
03007>	13.25	.002	54.67	.002	96.09	.002	137.51	.002	178.92	.002	03142>	24.50	.002	65.92	.002	107.34	.002	148.75	.002	190.16	.002
03008>	13.33	.002	54.75	.002	96.17	.002	137.59	.002	179.00	.002	03143>	24.58	.002	66.00	.002	107.43	.002	148.83	.002	190.25	.002
03009>	13.42	.002	54.83	.002	96.26	.002	137.68	.002	179.08	.002	03144>	24.67	.002	66.08	.002	107.51	.002	148.92	.002	190.33	.002
03010>	13.50	.002	54.92	.002	96.34	.002	137.76	.002	179.16	.002	03145>	24.75	.002	66.17	.002	107.59	.002	148.99	.002	190.42	.002
03011>	13.58	.002	55.00	.002	96.42	.002	137.84	.002	179.24	.002	03146>	24.83	.002	66.25	.002	107.68	.002	149.09	.002	190.50	.002
03012>	13.67	.002	55.08	.002	96.51	.002	137.92	.002	179.32	.002	03147>	24.92	.002	66.33	.002	107.76	.002	149.17	.002	190.58	.002
03013>	13.75	.002	55.17	.002	96.59	.002	138.01	.002	179.40	.002	03148>	25.00	.002	66.42	.002	107.84	.002	149.26	.002	190.66	.002
03014>	13.83	.002	55.25	.002	96.67	.002	138.09	.002	179.50	.002	03149>	25.08	.002	66.50	.002	107.93	.002	149.34	.002	190.75	.002
03015>	13.92	.002	55.33	.002	96.76	.002	138.18	.002	179.58	.002	03150>	25.17	.002	66.58	.002	108.01	.002	149.42	.002	190.83	.002
03016>	14.00	.002	55.42	.002	96.84	.002	138.26	.002	179.67	.002	03151>	25.25	.002	66.67	.002	108.09	.002	149.51	.002	190.91	.002
03017>	14.08	.002	55.50	.002	96.92	.002	138.34	.002	179.75	.002	03152>	25.33	.002	66.75	.002	108.18	.002	149.59	.002	191.00	.002
03018>	14.17	.002	55.58	.002	97.01	.002	138.43	.002	179.83	.002	03153>	25.42	.002	66.83	.002	108.26	.002	149.67	.002	191.08	.002
03019>	14.25	.002	55.67	.002	97.09	.002	138.51	.002	179.92	.002	03154>	25.50	.002	66.92	.002	108.34	.002	149.75	.002	191.16	.002
03020>	14.33	.002	55.75	.002	97.17	.002	138.59	.002	179.98	.002	03155>	25.58	.002	67.00	.002	108.43	.002	149.84	.002	191.25	.002
03021>	14.42	.002	55.83	.002	97.26	.002	138.68	.002	180.07	.002	03156>	25.65	.002	67.08	.002	108.51	.002	149.92	.002	191.33	.002
03022>	14.50	.002	55.92	.002	97.34	.002	138.76	.002	180.15	.002	03157>	25.									

03241>	32.75	.002	74.17	.002	115.59	.002	157.01	.002	198.41	.001	03376>		(ha)	(cms)	(hrs)	(mm)	(cms)	
03242>	32.83	.002	74.25	.002	115.68	.002	157.09	.002	198.50	.001	03377>	TOTAL HYD.	01:EX-1	2.37	.151	1.417	25.031	
03243>	32.92	.002	74.33	.002	115.76	.002	157.17	.002	198.58	.001	03378>	=====	=====	=====	=====	=====	=====	
03244>	33.00	.002	74.42	.002	115.84	.002	157.26	.002	198.66	.001	03379>	MAJOR SYST	02:THAMES	.00	.000	.000	.000	
03245>	33.08	.002	74.50	.002	115.93	.002	157.34	.002	198.75	.001	03380>	MINOR SYST	03:tdRAI	2.37	.001	206.867	25.031	.000
03246>	33.17	.002	74.58	.002	116.01	.002	157.42	.002	198.83	.001	03381>	=====	=====	=====	=====	=====	=====	
03247>	33.25	.002	74.67	.002	116.09	.002	157.51	.002	198.91	.001	03382>	NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.						
03248>	33.33	.002	74.75	.002	116.18	.002	157.59	.002	198.99	.001	03383>	=====	=====	=====	=====	=====	=====	
03249>	33.42	.002	74.83	.002	116.26	.002	157.67	.002	199.08	.001	03384>	Maximum MAJOR SYSTEM storage used =	583. (cu.m.)					
03250>	33.50	.002	74.92	.002	116.34	.002	157.76	.002	199.16	.001	03385>	=====	=====	=====	=====	=====	=====	
03251>	33.58	.002	75.00	.002	116.43	.002	157.84	.002	199.25	.001	03386>	=====	=====	=====	=====	=====	=====	
03252>	33.67	.002	75.08	.002	116.51	.002	157.92	.002	199.33	.001	03387>	001:0111--						
03253>	33.75	.002	75.17	.002	116.59	.002	158.01	.002	199.41	.001	03389>	CALIB NASHYD	Area (ha)= .19 Curve Number (CN)=74.00					
03254>	33.83	.002	75.25	.002	116.68	.002	158.09	.002	199.50	.001	03390>	01:EX-2 DT= 1.00 Ia (mm)= 5.000 # of Linear Res.(N)= 3.00						
03255>	33.92	.002	75.33	.002	116.76	.002	158.17	.002	199.58	.001	03391>	U.H. Tp(hrs)= .090						
03256>	34.00	.002	75.42	.002	116.84	.002	158.26	.002	199.66	.001	03392>	=====	=====	=====	=====	=====	=====	
03257>	34.08	.002	75.50	.002	116.93	.002	158.34	.002	199.75	.001	03393>	Unit Hyd Opeak (cms)= .081						
03258>	34.17	.002	75.58	.002	117.01	.002	158.42	.002	199.83	.001	03394>	=====	=====	=====	=====	=====	=====	
03259>	34.25	.002	75.67	.002	117.09	.002	158.51	.002	199.91	.001	03395>	PEAK FLOW (cms)= .032 (i)						
03260>	34.33	.002	75.75	.002	117.18	.002	158.59	.002	200.00	.001	03396>	TIME TO PEAK (hrs)= 1.083						
03261>	34.42	.002	75.84	.002	117.26	.002	158.67	.002	200.08	.001	03397>	RUNOFF VOLUME (mm)= 28.589						
03262>	34.50	.002	75.92	.002	117.34	.002	158.76	.002	200.16	.001	03398>	TOTAL RAINFALL (mm)= 71.791						
03263>	34.58	.002	76.00	.002	117.43	.002	158.84	.002	200.25	.001	03399>	RUNOFF COEFFICIENT = .398						
03264>	34.67	.002	76.09	.002	117.51	.002	158.92	.002	200.33	.001	03400>	=====	=====	=====	=====	=====	=====	
03265>	34.75	.002	76.17	.002	117.59	.002	159.01	.002	200.41	.001	03401>	(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.						
03266>	34.83	.002	76.25	.002	117.68	.002	159.09	.002	200.50	.001	03402>	=====	=====	=====	=====	=====	=====	
03267>	34.92	.002	76.33	.002	117.76	.002	159.17	.002	199.17	.001	03403>	=====	=====	=====	=====	=====	=====	
03268>	35.00	.002	76.42	.002	117.84	.002	159.26	.002	200.66	.001	03404>	001:0112--						
03269>	35.08	.002	76.50	.002	117.93	.002	159.34	.002	200.74	.001	03405>	=====	=====	=====	=====	=====	=====	
03270>	35.17	.002	76.59	.002	118.01	.002	159.42	.002	200.83	.001	03406>	CALIB STANDHYD Area (ha)= .45						
03271>	35.25	.002	76.67	.002	118.09	.002	159.51	.002	200.91	.001	03407>	04:EX-3 DT= 1.00 Total Imp(%)= 65.00 Dir. Conn.(%)= 1.00						
03272>	35.33	.002	76.75	.002	118.18	.002	159.59	.002	201.00	.001	03408>	U.H. Tp(hrs)= .090						
03273>	35.42	.002	76.84	.002	118.26	.002	159.67	.002	201.08	.001	03409>	IMPERVIOUS PERVIOUS (i)						
03274>	35.50	.002	76.92	.002	118.34	.002	159.76	.002	201.16	.001	03410>	Surface Area (ha)= .29	.16					
03275>	35.58	.002	77.00	.002	118.43	.002	159.84	.002	201.24	.001	03411>	Dep. Storage (mm)= 2.00	8.00					
03276>	35.67	.002	77.09	.002	118.51	.002	159.92	.002	201.33	.001	03412>	Average Slope (%)= 1.00	20.00					
03277>	35.75	.002	77.17	.002	118.59	.002	160.01	.002	201.41	.001	03413>	Length (m)= 5.00	25.00					
03278>	35.83	.002	77.25	.002	118.68	.002	160.09	.002	201.49	.001	03414>	Mannings n = .013	.240					
03279>	35.92	.002	77.34	.002	118.76	.002	160.17	.002	201.57	.001	03415>	=====	=====	=====	=====	=====	=====	
03280>	36.00	.002	77.42	.002	118.84	.002	160.25	.002	201.65	.001	03416>	Max.eff. Inten.(mm/hr)= 279.47	571.98					
03281>	36.08	.002	77.50	.002	118.93	.002	160.34	.002	201.74	.001	03417>	over (min)= 1.00	2.00					
03282>	36.17	.002	77.59	.002	119.01	.002	160.42	.002	201.83	.001	03418>	Storage Coeff. (min)= 1.28	1.58 (ii)					
03283>	36.25	.002	77.67	.002	119.09	.002	160.50	.002	201.91	.001	03419>	Unit Hyd. Tpeak (min)= 1.00	2.00					
03284>	36.33	.002	77.75	.002	119.18	.002	160.59	.002	201.99	.001	03420>	Unit Hyd. peak (cms)= 1.65	.65					
03285>	36.42	.002	77.84	.002	119.26	.002	160.67	.002	202.08	.001	03421>	=====	*TOTALS*	=====	=====	=====	=====	
03286>	36.50	.002	77.92	.002	119.34	.002	160.75	.002	202.16	.001	03422>	PEAK FLOW (cms)= .00	.22	.225	(iii)			
03287>	36.58	.002	78.00	.002	119.43	.002	160.84	.002	202.24	.001	03423>	TIME TO PEAK (hrs)= .98	1.00	1.00				
03288>	36.67	.002	78.09	.002	119.51	.002	160.92	.002	202.33	.001	03424>	RUNOFF VOLUME (mm)= 69.79	45.78	46.020				
03289>	36.75	.002	78.17	.002	119.59	.002	161.00	.002	202.41	.001	03425>	TOTAL RAINFALL (mm)= 71.79	71.79	71.791				
03290>	36.83	.002	78.25	.002	119.68	.002	161.09	.002	202.49	.001	03426>	RUNOFF COEFFICIENT = .97	.64	.641				
03291>	36.90	.002	78.33	.002	119.76	.002	161.17	.002	202.57	.001	03427>	=====	=====	=====	=====	=====	=====	
03292>	36.98	.002	78.42	.002	119.84	.002	161.25	.002	202.65	.001	03428>	(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:						
03293>	37.06	.002	78.50	.002	119.93	.002	161.34	.002	202.74	.001	03429>	CN* = 72.0 Ia = Dep. Storage (Above)						
03294>	37.17	.002	78.59	.002	120.01	.002	161.42	.002	202.83	.001	03430>	(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.						
03295>	37.25	.002	78.67	.002	120.09	.002	161.50	.002	202.91	.001	03431>	(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.						
03296>	37.33	.002	78.75	.002	120.18	.002	161.59	.002	202.99	.001	03432>	=====	=====	=====	=====	=====	=====	
03297>	37.42	.002	78.84	.002	120.26	.002	161.67	.002	203.08	.001	03433>	=====	=====	=====	=====	=====	=====	
03298>	37.50	.002	78.92	.002	120.34	.002	161.75	.002	203.16	.001	03434>	=====	=====	=====	=====	=====	=====	
03299>	37.58	.002	79.00	.002	120.43	.002	161.84	.002	203.24	.001	03435>	001:0113--						
03300>	37.67	.002	79.17	.002	120.59	.002	162.00	.002	203.41	.001	03436>	=====	=====	=====	=====	=====	=====	
03301>	37.75	.002	79.25	.002	120.68	.002	162.08	.002	203.49	.001	03437>	CALIB NASHYD	Area (ha)= 2.59 Curve Number (CN)=67.00					
03302>	37.83	.002	79.34	.002	120.76	.002	162.16	.002	203.58	.001	03438>	05:EX-4 DT= 1.00 Ia (mm)= 8.000 # of Linear Res.(N)= 3.00						
03303>	37.92	.002	79.42	.002	120.84	.002	162.25	.002	203.66	.001	03439>	U.H. Tp(hrs)= .230						
03304>	38.00	.002	79.50	.002	120.93	.002	162.34	.002	203.74	.001	03440>	=====	=====	=====	=====	=====	=====	
03305>	38.08	.002	79.58	.002	120.99	.002	162.42	.002	203.82	.001	03441>	Unit Hyd Opeak (cms)= .430						
03306>	38.17	.002	79.67	.002	121.09	.002	162.50	.002	203.90	.001	03442>	PEAK FLOW (cms)= .177 (i)						
03307>	38.25	.002	79.75	.002	121.18	.002	162.58	.002	203.99	.001	03443></td							

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03511> =====
03512> SUM 09:POST 12.24 4.514 1.00 45.27 .000
03513>
03514> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
03515>
03516> -----
03517> 001:0117 -----
03518> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
03520> | IN>09:(POST ) |
03521> | OUT<01:(SWMF ) |
03522> ===== OUTFLOW STORAGE TABLE =====
03523> | OUTFLOW | STORAGE | OUTFLOW | STORAGE |
03524> | (cms) | (ha.m.) | (cms) | (ha.m.) |
03525> | .000 .0000E+00 | .079 .1497E+00 |
03526> | .059 .1884E-01 | .080 .1683E+00 |
03527> | .069 .3388E-01 | .082 .1875E+00 |
03528> | .070 .4889E-01 | .083 .203E+00 |
03529> | .072 .638E-01 | .084 .227E+00 |
03530> | .073 .8041E-01 | .085 .2485E+00 |
03531> | .075 .9633E-01 | .087 .2700E+00 |
03532> | .076 .1140E+00 | .089 .3003E+00 |
03533> | .078 .1316E+00 | .090 .0000E+00 |
03534> ROUTING RESULTS
03535> | AREA | QPEAK | TPEAK | R.V.
03536> | (ha) | (cms) | (hrs) | (mm) |
03537> INFLOW >09: (POST ) 12.24 4.514 1.000 45.274
03538> OUTFLOW<01: (SWMF ) 12.24 .181 1.983 45.276
03539> OVERFLOW<02: (000003) .000 .000 .000 .000
03540>
03541> TOTAL NUMBER OF SIMULATED OVERRUNS = 0
03542> CUMULATIVE TIME OF OVERRUNS (hours)= .00
03543> PERCENTAGE OF TIME OVERRUNNING (%)= .00
03544>
03545> PEAK FLOW REDUCTION [Qout/Qin] (%)= 4.017
03546> TIME SHIFT OF PEAK FLOW (min)= 59.00
03547> MAXIMUM STORAGE USED (ha.m.)=.3280E+00
03548>
03549>
03550> 001:0118 -----
03551> | DIVERT HYD |
03552> | INID=01 (SWMF ) |
03553>
03554> Outflow / Inflow Relationships
03555> Flow 03 + Flow 04 + Flow 05 = Total
03556> | (cms) | (cms) | (cms) | (cms) |
03557> | .000 .000 .000 .000 |
03558> | .000 .059 .000 .059 |
03559> | .000 .059 .000 .059 |
03560> | .007 .061 .000 .069 |
03561> | .007 .068 .000 .070 |
03562> | .008 .064 .000 .072 |
03563> | .008 .065 .000 .073 |
03564> | .008 .066 .000 .075 |
03565> | .009 .068 .000 .076 |
03566> | .009 .069 .000 .078 |
03567> | .009 .070 .000 .079 |
03568> | .009 .071 .000 .080 |
03569> | .010 .072 .000 .082 |
03570> | .010 .073 .000 .083 |
03571> | .010 .074 .000 .085 |
03572> | .010 .075 .000 .086 |
03573> | .011 .077 .000 .087 |
03574> | .011 .078 .210 .299 |
03575>
03576> NYHD AREA QPEAK TpeakDate_hh:mm R.V. NFE WetHrs
03577> | (ha) | (cms) | | (hrs) | (mm) | (hrs) |
03578> IDIn = 01:SWMF 12.24 .181 No_date 1:59 45.276 1 215.
03579> =====
03580> IDout= 03:Infiltrat .91 .011 No_date 1:59 45.276 1 13.
03581> IDout= 04:Orific 9.92 .077 No_date 1:59 45.276 1 215.
03582> IDout= 05:Emerge 1.42 .093 No_date 1:59 45.276 1 3.
03583>
03584> 001:0119 -----
03585> | PRINT HYD | AREA (ha)= 1.416
03586> | ID=05 (Emerge) | QPEAK (cms)= .093 (i)
03587> | DT= 1.00 PCYC= 5 | TPEAK (hrs)= 1.983
03588> | VOLUME (mm)= 45.276
03589>
03590>
03591> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
03592> TIME FLOW | TIME FLOW
03593> hrs cms | hrs cms
03594> .0 .000 | .83 .000 | 1.67 .087 | 2.50 .085 | 3.33 .044
03595> .08 .0001 | .92 .000 | 1.75 .090 | 2.58 .083 | 3.42 .038
03596> .17 .0001 | 1.00 .000 | 1.83 .092 | 2.67 .080 | 3.50 .032
03597> .25 .0001 | 1.08 .000 | 1.92 .093 | 2.75 .078 | 3.58 .027
03598> .33 .0001 | 1.17 .000 | 2.00 .093 | 2.83 .075 | 3.67 .021
03599> .42 .0001 | 1.25 .032 | 2.08 .093 | 2.92 .072 | 3.75 .016
03600> .50 .0001 | 1.33 .053 | 2.17 .092 | 3.00 .070 | 3.83 .011
03601> .58 .0001 | 1.42 .066 | 2.25 .091 | 3.08 .064 | 3.92 .007
03602> .67 .0001 | 1.50 .076 | 2.33 .089 | 3.17 .057 | 4.00 .003
03603> .75 .0001 | 1.58 .083 | 2.42 .087 | 3.25 .051 |
03604>
03605> 001:0120 -----
03606> *#*****
03607> *#
03608> *# 250-year
03609> *#
03610> *#
03611> *#*****
03612> -----
03613> | CHICAGO STORM | IDF curve parameters: A=3048.220
03614> | Ptotal= 86.60 mm | B= 10.030
03615> | C= .888
03616> used in: INTENSITY = A / (t + B)^C
03617>
03618> Duration of storm = 3.00 hrs
03619> Storm time step = 5.00 min
03620> Time to peak ratio = .33
03621>
03622> TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
03623> hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
03624> .08 5.146 | .83 43.789 | 1.58 19.207 | 2.33 7.218
03625> .17 5.748 | .92 106.492 | 1.67 16.378 | 2.42 6.730
03626> .25 6.505 | 1.00 274.730 | 1.75 14.228 | 2.50 6.302
03627> .33 7.406 | 1.04 327.400 | 1.87 12.178 | 2.58 5.925
03628> .42 8.399 | 1.17 76.628 | 1.92 11.204 | 2.57 5.299
03629> .50 10.637 | 1.25 50.754 | 2.00 10.107 | 2.75 2.289
03630> .58 13.366 | 1.33 36.943 | 2.08 9.197 | 2.83 5.020
03631> .67 17.763 | 1.42 28.579 | 2.17 8.431 | 2.92 4.776
03632> .75 25.782 | 1.50 23.067 | 2.25 7.779 | 3.00 4.554
03633>
03634>
03635> 001:0121 -----
03636> *#*****
03637> *#
03638> *# EXISTING CONDITIONS
03639> *#
03640> *#*****
03641>
03642> | CALIB NASHYD | Area (ha)= 2.37 Curve Number (CN)=72.00
03643> | 01:EX-1 DT= 1.00 | Ia (mm)= 8.000 # of Linear Res.(N)= 3.00
03644> | U.H. Tp(hrs)= .330
03645>
03646> =====
03647> Unit Hyd Qpeak (cms)= .274
03648> PEAK FLOW (cms)= .223 (i)
03649> TIME TO PEAK (hrs)= 1.433
03650> RUNOFF VOLUME (mm)= 34.829
03651> TOTAL RAINFALL (mm)= 86.599
03652> RUNOFF COEFFICIENT = .402
03653>
03654> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
03655>
03656> -----
03657> 001:0122 -----
03658> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .001 (cms)
03659> | TotalHyd 01:EX-1 | Number of inlets in system [NINLET] = 1
03660> | Total minor system capacity = .001 (cms)
03661> | Total major system storage [TMJSTO] = 99999. (cu.m.)
03662>
03663> ID: NYHY AREA QPEAK TPEAK R.V. DWF
03664> | (ha) | (cms) | (hrs) | (mm) | (cms) |
03665> | 2.37 | .223 | 1.433 | 34.829 | .000
03666> TOTAL HYD. 01:EX-1 2.37 .223 1.433 34.829 .000
03667> =====
03668> MAJOR SYST 02:THAMES .00 .000 .000 .000 .000
03669> MINOR SYST 03:toDRAI 2.37 .001 287.433 34.829 .000
03670>
03671> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
03672>
03673> Maximum MAJOR SYSTEM storage used = 816. (cu.m.)
03674>
03675>
03676> 001:0123 -----
03677>
03678> | CALIB NASHYD | Area (ha)= .19 Curve Number (CN)=74.00
03679> | 01:EX-2 DT= 1.00 | Ia (mm)= 5.000 # of Linear Res.(N)= 3.00
03680> | U.H. Tp(hrs)= .090
03681>
03682> Unit Hyd Qpeak (cms)= .081
03683>
03684> PEAK FLOW (cms)= .041 (i)
03685> TIME TO PEAK (hrs)= 1.100
03686> RUNOFF VOLUME (mm)= 38.973
03687> TOTAL RAINFALL (mm)= 86.599
03688> RUNOFF COEFFICIENT = .450
03689>
03690> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
03691>
03692>
03693> 001:0124 -----
03694>
03695> | CALIB STANDHYD | Area (ha)= .45
03696> | 04:EX-3 DT= 1.00 | Total Imp=% 65.00 Dir. Conn.%= 1.00
03697>
03698> IMPERVIOUS PERVIOUS (i)
03699> Surface Area (ha)= .29 .16
03700> Dep. Storage (mm)= 2.00 8.00
03701> Average Slope (%)= 1.00 20.00
03702> Length (m)= 5.00 25.00
03703> Mannings n = .013 .240
03704>
03705> Max.eff.Inten. (mm/hr)= 274.73 590.27
03706> over (min)= 1.00 2.00
03707> Storage Coeff. (min)= .28 (ii) 1.56 (ii)
03708> Unit Hyd. Tpeak (min)= 1.00 2.00
03709> Unit Hyd. peak (cms)= 1.65 .65
03710> *TOTALS*
03711> PEAK FLOW (cms)= .00 .23 .238 (iii)
03712> TIME TO PEAK (hrs)= .98 1.00 1.00
03713> RUNOFF VOLUME (mm)= 84.60 59.12 59.379
03714> TOTAL RAINFALL (mm)= 86.60 86.60 86.599
03715> RUNOFF COEFFICIENT = .98 .68 .686
03716>
03717> (i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:
03718> CN= 72.0 Ia= Dep. Storage (Above)
03719> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
03720> THAN THE STORAGE COEFFICIENT.
03721> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
03722>
03723>
03724> 001:0125 -----
03725>
03726> | CALIB NASHYD | Area (ha)= 2.59 Curve Number (CN)=67.00
03727> | 05:EX-4 DT= 1.00 | Ia (mm)= 8.000 # of Linear Res.(N)= 3.00
03728> | U.H. Tp(hrs)= .230
03729>
03730> Unit Hyd Qpeak (cms)= .430
03731>
03732> PEAK FLOW (cms)= .262 (i)
03733> TIME TO PEAK (hrs)= 1.317
03734> RUNOFF VOLUME (mm)= 30.328
03735> TOTAL RAINFALL (mm)= 86.599
03736> RUNOFF COEFFICIENT = .350
03737>
03738> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
03739>
03740>
03741> 001:0126 -----
03742>
03743> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .001 (cms)
03744> | TotalHyd 05:EX-4 | Number of inlets in system [NINLET] = 1
03745> | Total minor system capacity = .001 (cms)
03746> | Total major system storage [TMJSTO] = 99999. (cu.m.)
03747>
03748> ID: NYHY AREA QPEAK TPEAK R.V. DWF
03749> | (ha) | (cms) | (hrs) | (mm) | (cms) |
03750> TOTAL HYD. 05:EX-4 2.59 .262 1.317 30.328 .000
03751>
03752>
03753> Unit Hyd Qpeak (cms)= .430
03754>
03755> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
03756>
03757> Maximum MAJOR SYSTEM storage used = 777. (cu.m.)
03758>
03759>
03760> 001:0127 -----
03761>
03762> | COMPUTE DUALHYD | Average inlet capacities [CINLET] = .001 (cms)
03763> | TotalHyd 05:EX-4 | Number of inlets in system [NINLET] = 1
03764> | Total minor system capacity = .001 (cms)
03765> | Total major system storage [TMJSTO] = 99999. (cu.m.)
03766>
03767> ID: NYHY AREA QPEAK TPEAK R.V. DWF
03768> | (ha) | (cms) | (hrs) | (mm) | (cms) |
03769> | 2.59 | .262 | 1.317 | 30.328 | .000
03770>
03771> MAJOR SYST 06:BANNAN .00 .000 .000 .000 .000
03772> MINOR SYST 07:toDRAI 2.59 .001 273.550 30.329 .000
03773>
03774>
03775> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
03776>
03777> 001:0128 -----
03778>
03779> | ADD HYD (PRE) | ID: NYHY AREA QPEAK TPEAK R.V. DWF
03780> | (ha) | (cms) | (hrs) | (mm) | (cms) |

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03781>	ID1 01:EX-2	.19	.041	1.10	38.97	.000		03916>	9.50	.002	67.00	.002	124.51	.002	182.00	.002	239.49	.002
03782>	+ID2 03:toDRAIN	2.37	.001	287.43	34.83	.000		03917>	9.58	.002	67.08	.002	124.60	.002	182.08	.002	239.57	.002
03783>	+ID3 04:EX-3	.45	.238	1.00	59.38	.000		03918>	9.67	.002	67.17	.002	124.68	.002	182.17	.002	239.65	.002
03784>	+ID4 05:C101	6.64	.651	1.42	34.83	.000		03919>	9.75	.002	67.25	.002	124.76	.002	182.25	.002	239.74	.002
03785>	+ID5 07:toDRAIN	2.59	.001	273.55	30.33	.000		03920>	9.83	.002	67.33	.002	124.85	.002	182.33	.002	239.82	.002
03786>	=====							03921>	9.92	.002	67.42	.002	124.93	.002	182.42	.002	239.90	.002
03787>	SUM 08:PRE	12.24	.700	1.40	34.83	.000		03922>	1.00	.002	67.50	.002	125.01	.002	182.50	.002	240.07	.002
03788>	=====							03923>	1.08	.002	67.58	.002	125.10	.002	182.58	.002	240.07	.002
03789>	NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.							03924>	10.17	.002	67.67	.002	126.18	.002	182.67	.002	240.15	.002
03790>	=====							03925>	10.25	.002	67.75	.002	125.26	.002	182.75	.002	240.24	.002
03791>	=====							03926>	10.33	.002	67.83	.002	125.35	.002	182.83	.002	240.32	.002
03792>	001:0129-----							03927>	10.42	.002	67.92	.002	125.43	.002	182.92	.002	240.40	.002
03793>	=====							03928>	10.50	.002	68.00	.002	125.51	.002	183.00	.002	240.49	.002
03794>	PRINT HYD AREA (ha)= 12.240							03929>	10.58	.002	68.08	.002	125.60	.002	183.08	.002	240.57	.002
03795>	ID=08 (PRE) QPEAK (cms)= .700 (i)							03930>	10.67	.002	68.17	.002	125.68	.002	183.17	.002	240.65	.002
03796>	DT= 1.00 PCYC= 5 TPEAK (hrs)= 1.400							03931>	10.75	.002	68.25	.002	125.76	.002	183.25	.002	240.74	.002
03797>	VOLUME (mm)= 34.834							03932>	10.83	.002	68.33	.002	125.85	.002	183.33	.002	240.82	.002
03798>	(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.							03933>	10.92	.002	68.42	.002	125.93	.002	183.40	.002	240.89	.002
03800>	TIME FLOW TIME FLOW TIME FLOW TIME FLOW TIME FLOW TIME FLOW TIME							03934>	11.00	.002	68.50	.002	126.10	.002	183.58	.002	241.07	.002
03801>	hrs cms hrs cms hrs cms hrs cms hrs cms hrs cms							03935>	11.17	.002	68.67	.002	126.18	.002	183.67	.002	241.15	.002
03802>	.000 .0001 57.50 .002 115.01 .002 172.50 .002 229.99 .002							03936>	11.25	.002	68.75	.002	126.26	.002	183.75	.002	241.24	.002
03803>	.08 .0001 57.58 .002 115.09 .002 172.59 .002 230.07 .002							03937>	11.33	.002	68.83	.002	126.35	.002	183.83	.002	241.32	.002
03804>	.17 .0001 57.67 .002 115.18 .002 172.67 .002 230.15 .002							03938>	11.42	.002	68.92	.002	126.43	.002	183.90	.002	241.40	.002
03805>	.25 .0001 57.75 .002 115.26 .002 172.75 .002 230.24 .002							03940>	11.50	.002	69.00	.002	126.51	.002	184.00	.002	241.49	.002
03806>	.33 .0001 57.83 .002 115.34 .002 172.84 .002 230.32 .002							03941>	11.58	.002	69.08	.002	126.60	.002	184.08	.002	241.57	.002
03807>	.42 .0001 57.92 .002 115.43 .002 172.92 .002 230.40 .002							03942>	11.67	.002	69.17	.002	126.68	.002	184.17	.002	241.65	.002
03808>	.50 .0001 58.00 .002 115.51 .002 173.00 .002 230.49 .002							03943>	11.75	.002	69.25	.002	126.76	.002	184.25	.002	241.74	.002
03809>	.58 .0001 58.08 .002 115.59 .002 173.08 .002 230.57 .002							03944>	11.83	.002	69.33	.002	126.85	.002	184.33	.002	241.80	.002
03810>	.67 .0001 58.17 .002 115.66 .002 173.17 .002 230.65 .002							03945>	11.92	.002	69.42	.002	126.93	.002	184.42	.002	241.89	.002
03811>	.75 .0001 58.25 .002 115.76 .002 173.25 .002 230.74 .002							03946>	12.00	.002	69.50	.002	127.01	.002	184.50	.002	241.99	.002
03812>	.83 .0001 58.33 .002 115.84 .002 173.34 .002 230.82 .002							03947>	12.08	.002	69.58	.002	127.10	.002	184.58	.002	242.07	.002
03813>	.92 .0791 58.42 .002 115.93 .002 173.42 .002 230.90 .002							03948>	12.17	.002	69.67	.002	127.18	.002	184.67	.002	242.15	.002
03814>	1.00 .3261 58.50 .002 116.01 .002 173.50 .002 230.98 .002							03949>	12.25	.002	69.75	.002	127.26	.002	184.75	.002	242.23	.002
03815>	1.08 .4021 58.58 .002 116.09 .002 173.59 .002 231.07 .002							03950>	12.33	.002	69.83	.002	127.35	.002	184.83	.002	242.32	.002
03816>	1.17 .5201 58.67 .002 116.18 .002 173.67 .002 231.15 .002							03951>	12.42	.002	69.92	.002	127.43	.002	184.92	.002	242.40	.002
03817>	1.25 .6291 58.75 .002 116.26 .002 173.75 .002 231.24 .002							03952>	12.50	.002	70.00	.002	127.51	.002	185.00	.002	242.48	.002
03818>	1.33 .6901 58.83 .002 116.34 .002 173.84 .002 231.33 .002							03953>	12.67	.002	70.17	.002	127.68	.002	185.17	.002	242.56	.002
03819>	1.42 .6991 58.92 .002 116.43 .002 173.92 .002 231.40 .002							03954>	12.75	.002	70.25	.002	127.76	.002	185.25	.002	242.64	.002
03820>	1.50 .6861 59.00 .002 116.51 .002 173.98 .002 231.49 .002							03955>	12.83	.002	70.33	.002	127.85	.002	185.33	.002	242.72	.002
03821>	1.58 .6831 59.08 .002 116.59 .002 174.04 .002 231.56 .002							03956>	12.90	.002	70.42	.002	127.93	.002	185.42	.002	242.80	.002
03822>	1.67 .6541 59.17 .002 116.58 .002 174.11 .002 231.55 .002							03957>	12.98	.002	70.50	.002	127.99	.002	185.50	.002	242.89	.002
03823>	1.75 .4781 59.25 .002 116.67 .002 174.16 .002 231.51 .002							03958>	13.00	.002	70.50	.002	128.01	.002	185.58	.002	242.98	.002
03824>	1.83 .4141 59.33 .002 116.84 .002 174.33 .002 231.82 .002							03959>	13.08	.002	70.58	.002	128.10	.002	185.68	.002	243.07	.002
03825>	1.92 .3361 59.42 .002 116.93 .002 174.42 .002 231.91 .002							03960>	13.17	.002	70.67	.002	128.18	.002	185.67	.002	243.15	.002
03826>	2.00 .3061 59.50 .002 117.01 .002 174.50 .002 231.99 .002							03961>	13.25	.002	70.75	.002	128.26	.002	185.75	.002	243.23	.002
03827>	2.08 .2641 59.58 .002 117.09 .002 174.58 .002 232.07 .002							03962>	13.33	.002	70.83	.002	128.35	.002	185.83	.002	243.32	.002
03828>	2.17 .2291 59.67 .002 117.18 .002 174.67 .002 232.15 .002							03963>	13.42	.002	70.92	.002	128.43	.002	185.92	.002	243.40	.002
03829>	2.25 .2001 59.75 .002 117.26 .002 174.75 .002 232.24 .002							03964>	13.50	.002	71.00	.002	128.50	.002	186.00	.002	243.48	.002
03830>	2.33 .1771 59.83 .002 117.34 .002 174.83 .002 232.32 .002							03965>	13.58	.002	71.08	.002	128.58	.002	186.08	.002	243.57	.002
03831>	2.42 .1541 59.92 .002 117.43 .002 174.92 .002 232.40 .002							03966>	13.66	.002	71.17	.002	128.66	.002	186.16	.002	243.65	.002
03832>	2.50 .1334 60.00 .002 117.51 .002 175.00 .002 232.48 .002							03967>	13.75	.002	71.25	.002	128.76	.002	186.25	.002	243.73	.002
03833>	2.58 .1281 60.08 .002 117.59 .002 175.08 .002 232.52 .002							03968>	13.83	.002	71.33	.002	128.85	.002	186.33	.002	243.82	.002
03834>	2.67 .1171 60.17 .002 117.68 .002 175.17 .002 232.65 .002							03969>	13.92	.002	71.42	.002	128.93	.002	186.42	.002	243.90	.002
03835>	2.75 .1071 60.25 .002 117.76 .002 175.25 .002 232.74 .002							03970>	14.00	.002	71.50	.002	129.01	.002	186.50	.002	243.98	.002
03836>	2.83 .0991 60.33 .002 117.84 .002 175.33 .002 232.82 .002							03971>	14.08	.002	71.58	.002	129.10	.002	186.67	.002	244.07	.002
03837>	2.92 .0921 60.42 .002 117.93 .002 175.42 .002 232.90 .002							03972>	14.17	.002	71.67	.002	129.18	.002	186.75	.002	244.23	.002
03838>	3.00 .0871 60.50 .002 118.01 .002 175.50 .002 232.98 .002							03973>	14.25	.002	71.75	.002	129.26	.002	186.83	.002	244.32	.002
03839>	3.08 .0751 60.58 .002 118.09 .002 175.58 .002 233.07 .002							03974>	14.33	.002	71.83	.002	129.35	.002	186.83	.002	244.32	.002
03840>	3.17 .0651 61.42 .002 1																	

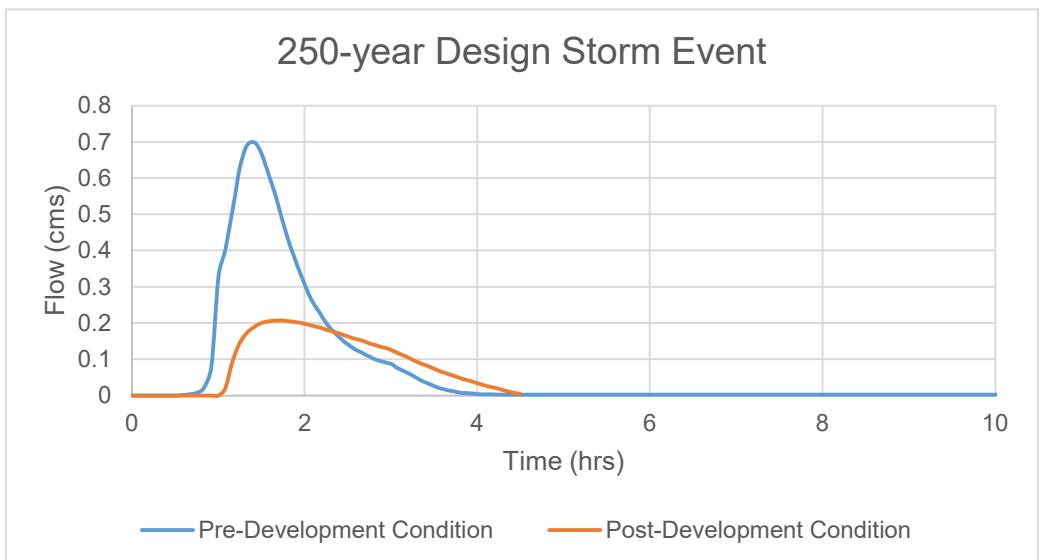
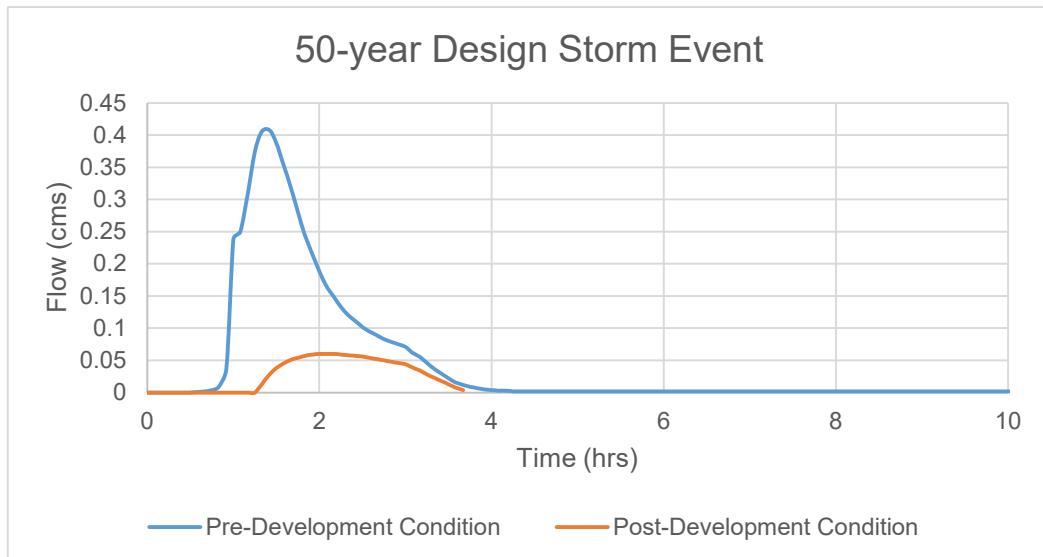
04051>	20.75	.002	78.25	.002	135.76	.002	193.25	.002	250.73	.002	04186>	32.00	.002	89.50	.002	147.01	.002	204.49	.002	261.98	.002
04052>	20.83	.002	78.34	.002	135.84	.002	193.33	.002	250.82	.002	04187>	32.08	.002	89.59	.002	147.09	.002	204.58	.002	262.06	.002
04053>	20.92	.002	78.42	.002	135.93	.002	193.41	.002	250.90	.002	04188>	32.17	.002	89.67	.002	147.17	.002	204.66	.002	262.15	.002
04054>	21.00	.002	78.50	.002	136.01	.002	193.50	.002	250.98	.002	04189>	32.25	.002	89.75	.002	147.26	.002	204.74	.002	262.23	.002
04055>	21.08	.002	78.59	.002	136.09	.002	193.58	.002	251.07	.002	04190>	32.33	.002	89.84	.002	147.34	.002	204.83	.002	262.31	.002
04056>	21.17	.002	78.67	.002	136.18	.002	193.66	.002	251.15	.002	04191>	32.42	.002	89.92	.002	147.42	.002	204.91	.002	262.40	.002
04057>	21.25	.002	78.75	.002	136.26	.002	193.75	.002	251.23	.002	04192>	32.50	.002	90.00	.002	147.51	.002	204.98	.002	262.48	.002
04058>	21.33	.002	78.84	.002	136.34	.002	193.83	.002	251.32	.002	04193>	32.58	.002	90.09	.002	147.59	.002	205.08	.002	262.56	.002
04059>	21.42	.002	78.92	.002	136.43	.002	193.91	.002	251.40	.002	04194>	32.67	.002	90.17	.002	147.67	.002	205.16	.002	262.65	.002
04060>	21.50	.002	79.00	.002	136.51	.002	194.00	.002	251.48	.002	04195>	32.75	.002	90.25	.002	147.76	.002	205.24	.002	262.73	.002
04061>	21.58	.002	79.09	.002	136.59	.002	194.08	.002	251.57	.002	04196>	32.83	.002	90.34	.002	147.84	.002	205.33	.002	262.81	.002
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04064>	21.83	.002	79.34	.002	136.84	.002	194.33	.002	251.82	.002	04199>	33.08	.002	90.59	.002	148.09	.002	205.58	.002	263.06	.002
04065>	21.92	.002	79.42	.002	136.93	.002	194.41	.002	251.90	.002	04200>	33.17	.002	90.67	.002	148.17	.002	205.63	.002	263.15	.002
04066>	22.00	.002	79.50	.002	137.01	.002	194.50	.002	251.98	.002	04201>	33.25	.002	90.75	.002	148.26	.002	205.74	.002	263.23	.002
04067>	22.08	.002	79.59	.002	137.09	.002	194.58	.002	252.07	.002	04202>	33.33	.002	90.84	.002	148.34	.002	205.83	.002	263.31	.002
04068>	22.17	.002	79.67	.002	137.18	.002	194.66	.002	252.15	.002	04203>	33.42	.002	90.92	.002	148.42	.002	205.91	.002	263.40	.002
04069>	22.25	.002	79.75	.002	137.26	.002	194.75	.002	252.23	.002	04204>	33.50	.002	90.99	.002	148.51	.002	205.99	.002	263.49	.002
04070>	22.33	.002	79.84	.002	137.34	.002	194.83	.002	252.32	.002	04205>	33.58	.002	91.09	.002	148.59	.002	206.08	.002	263.56	.002
04071>	22.42	.002	79.92	.002	137.43	.002	194.91	.002	252.40	.002	04206>	33.67	.002	91.17	.002	148.67	.002	206.16	.002	263.65	.002
04072>	22.50	.002	80.00	.002	137.51	.002	195.00	.002	252.48	.002	04207>	33.75	.002	91.26	.002	148.76	.002	206.24	.002	263.73	.002
04073>	22.58	.002	80.09	.002	137.59	.002	195.08	.002	252.57	.002	04208>	33.83	.002	91.34	.002	148.84	.002	206.33	.002	263.81	.002
04074>	22.67	.002	80.17	.002	137.68	.002	195.16	.002	252.65	.002	04209>	33.92	.002	91.42	.002	148.92	.002	206.41	.002	263.90	.002
04075>	22.75	.002	80.25	.002	137.76	.002	195.25	.002	252.73	.002	04210>	34.00	.002	91.51	.002	149.01	.002	206.49	.002	263.98	.002
04076>	22.83	.002	80.34	.002	137.84	.002	195.33	.002	252.82	.002	04211>	34.08	.002	91.59	.002	149.09	.002	206.58	.002	264.06	.002
04077>	22.92	.002	80.42	.002	137.93	.002	195.41	.002	252.90	.002	04212>	34.17	.002	91.67	.002	149.17	.002	206.66	.002	264.15	.002
04078>	23.00	.002	80.50	.002	138.01	.002	195.50	.002	252.98	.002	04213>	34.25	.002	91.76	.002	149.26	.002	206.74	.002	264.23	.002
04079>	23.08	.002	80.59	.002	138.09	.002	195.58	.002	253.06	.002	04214>	34.33	.002	91.84	.002	149.34	.002	206.83	.002	264.30	.002
04080>	23.17	.002	80.67	.002	138.18	.002	195.66	.002	253.15	.002	04215>	34.42	.002	91.92	.002	149.42	.002	206.91	.002	264.39	.002
04081>	23.25	.002	80.75	.002	138.26	.002	195.75	.002	253.23	.002	04216>	34.50	.002	92.01	.002	149.51	.002	206.99	.002	264.48	.002
04082>	23.33	.002	80.84	.002	138.34	.002	195.83	.002	253.32	.002	04217>	34.58	.002	92.09	.002	149.59	.002	207.08	.002	264.56	.002
04083>	23.42	.002	80.92	.002	138.43	.002	195.91	.002	253.40	.002	04218>	34.67	.002	92.17	.002	149.67	.002	207.16	.002	264.65	.002
04084>	23.50	.002	81.00	.002	138.51	.002	196.00	.002	253.48	.002	04219>	34.75	.002	92.26	.002	149.76	.002	207.24	.002	264.73	.002
04085>	23.58	.002	81.09	.002	138.59	.002	196.08	.002	253.57	.002	04220>	34.83	.002	92.34	.002	149.84	.002	207.33	.002	264.81	.002
04086>	23.67	.002	81.17	.002	138.68	.002	196.16	.002	253.65	.002	04221>	34.92	.002	92.42	.002	149.92	.002	207.41	.002	264.90	.002
04087>	23.75	.002	81.25	.002	138.76	.002	196.25	.002	253.73	.002	04222>	35.00	.002	92.51	.002	150.01	.002	207.49	.002	264.98	.002
04088>	23.83	.002	81.34	.002	138.84	.002	196.33	.002	253.81	.002	04223>	35.08	.002	92.59	.002	150.09	.002	207.57	.002	265.06	.002
04089>	23.92	.002	81.42	.002	138.93	.002	196.41	.002	253.90	.002	04224>	35.17	.002	92.67	.002	150.17	.002	207.66	.002	265.15	.002
04090>	24.00	.002	81.50	.002	138.99	.002	196.48	.002	253.98	.002	04225>	35.25	.002	92.76	.002	150.26	.002	207.74	.002	265.23	.002
04091>	24.08	.002	81.59	.002	139.07	.002	196.56	.002	254.06	.002	04226>	35.34	.002	92.84	.002	150.34	.002	207.83	.002	265.31	.002
04092>	24.17	.002	81.67	.002	139.16	.002	196.64	.002	254.14	.002	04227>	35.42	.002	92.93	.002	150.42	.002	207.91	.002	265.39	.002
04093>	24.25	.002	81.75	.002	139.24	.002	196.72	.002	254.23	.002	04228>	35.50	.002	93.01	.002	150.51	.002	207.99	.002	265.48	.002
04094>	24.33	.002	81.84	.002	139.32	.002	196.83	.002	254.32	.002	04229>	35.58	.002	93.09	.002	150.59	.002	208.08	.002	265.56	.002
04095>	24.42	.002	81.92	.002	139.43	.002	196.91	.002	254.40	.002	04230>	35.67	.002	93.17	.002	150.67	.002	208.16	.002	265.65	.002
04096>	24.50	.002	82.00	.002	139.51	.002	197.00	.002	254.48	.002	04231>	35.75	.002	93.26	.002	150.76	.002	208.24	.002	265.73	.002
04097>	24.58	.002	82.09	.002	139.59	.002	197.08	.002	254.57	.002	04232>	35.83	.002	93.34	.002	150.84	.002	208.33	.002	265.81	.002
04098>	24.67	.002	82.17	.002	139.68	.002	197.16	.002	254.65	.002	04233>	35.92	.002	93.42	.002	150.92	.002	208.41	.002	265.90	.002
04099>	24.75	.002	82.25	.002	139.76	.002	197.25	.002	254.73	.002	04234>	36.00	.002	93.51	.002	151.01	.002	208.49	.002	265.98	.00

04321>	43.25	.002	100.76	.002	158.26	.002	215.74	.002	273.23	.002	04456>	54.50	.002	112.01	.002	169.50	.002	226.99	.002	284.47	.001
04322>	43.33	.002	100.84	.002	158.34	.002	215.82	.002	273.31	.002	04457>	54.58	.002	112.09	.002	169.59	.002	227.07	.002	284.56	.001
04323>	43.42	.002	100.92	.002	158.42	.002	215.91	.002	273.39	.002	04458>	54.67	.002	112.18	.002	169.67	.002	227.16	.002	284.64	.001
04324>	43.50	.002	101.01	.002	158.51	.002	215.99	.002	273.48	.002	04459>	54.75	.002	112.26	.002	169.75	.002	227.24	.002	284.72	.001
04325>	43.58	.002	101.09	.002	158.59	.002	216.07	.002	273.56	.001	04460>	54.83	.002	112.34	.002	169.84	.002	227.32	.002	284.81	.001
04326>	43.67	.002	101.17	.002	158.67	.002	216.16	.002	273.64	.001	04461>	54.92	.002	112.43	.002	169.92	.002	227.41	.002	284.89	.001
04327>	43.75	.002	101.25	.002	158.76	.002	216.24	.002	273.73	.001	04462>	55.00	.002	112.51	.002	170.00	.002	227.49	.002	284.97	.001
04328>	43.83	.002	101.34	.002	158.84	.002	216.32	.002	273.81	.001	04463>	55.08	.002	112.59	.002	170.09	.002	227.57	.002	285.06	.001
04329>	43.92	.002	101.42	.002	158.92	.002	216.41	.002	273.89	.001	04464>	55.17	.002	112.68	.002	170.17	.002	227.66	.002	285.14	.001
04330>	43.99	.002	101.51	.002	159.01	.002	216.49	.002	273.98	.001	04465>	55.25	.002	112.76	.002	170.25	.002	227.74	.002	285.22	.001
04331>	44.08	.002	101.59	.002	159.09	.002	216.57	.002	274.06	.001	04466>	55.33	.002	112.84	.002	170.34	.002	227.82	.002	285.31	.001
04332>	44.17	.002	101.67	.002	159.17	.002	216.66	.002	274.14	.001	04467>	55.42	.002	112.93	.002	170.42	.002	227.91	.002	285.39	.001
04333>	44.25	.002	101.76	.002	159.26	.002	216.74	.002	274.23	.001	04468>	55.50	.002	113.01	.002	170.50	.002	227.99	.002	285.47	.001
04334>	44.33	.002	101.84	.002	159.34	.002	216.82	.002	274.31	.001	04469>	55.58	.002	113.09	.002	170.59	.002	228.07	.002	285.56	.001
04335>	44.42	.002	101.92	.002	159.42	.002	216.91	.002	274.39	.001	04470>	55.67	.002	113.18	.002	170.67	.002	228.15	.002	285.64	.001
04336>	44.50	.002	102.01	.002	159.51	.002	216.99	.002	274.48	.001	04471>	55.75	.002	113.26	.002	170.75	.002	228.24	.002	285.72	.001
04337>	44.58	.002	102.09	.002	159.59	.002	217.07	.002	274.56	.001	04472>	55.83	.002	113.34	.002	170.84	.002	228.32	.002	285.81	.001
04338>	44.67	.002	102.17	.002	159.67	.002	217.15	.002	274.64	.001	04473>	55.92	.002	113.43	.002	170.92	.002	228.40	.002	285.89	.001
04339>	44.75	.002	102.26	.002	159.76	.002	217.23	.002	274.72	.001	04474>	56.00	.002	113.51	.002	171.00	.002	228.49	.002	285.97	.001
04340>	44.83	.002	102.34	.002	159.84	.002	217.32	.002	274.81	.001	04475>	56.08	.002	113.59	.002	171.09	.002	228.57	.002	286.06	.001
04341>	44.92	.002	102.42	.002	159.92	.002	217.41	.002	274.89	.001	04476>	56.17	.002	113.68	.002	171.17	.002	228.65	.002	286.14	.001
04342>	45.00	.002	102.51	.002	160.01	.002	217.49	.002	274.98	.001	04477>	56.25	.002	113.76	.002	171.25	.002	228.74	.002	286.22	.001
04343>	45.08	.002	102.59	.002	160.09	.002	217.57	.002	275.06	.001	04478>	56.33	.002	113.84	.002	171.34	.002	228.82	.002	286.31	.001
04344>	45.17	.002	102.67	.002	160.17	.002	217.66	.002	275.14	.001	04479>	56.42	.002	113.93	.002	171.42	.002	228.91	.002	286.39	.001
04345>	45.25	.002	102.74	.002	160.25	.002	217.74	.002	275.23	.001	04480>	56.50	.002	114.01	.002	171.50	.002	228.99	.002	286.47	.001
04346>	45.33	.002	102.84	.002	160.34	.002	217.82	.002	275.31	.001	04481>	56.58	.002	114.09	.002	171.59	.002	229.07	.002	286.56	.001
04347>	45.42	.002	102.92	.002	160.42	.002	217.91	.002	275.39	.001	04482>	56.67	.002	114.18	.002	171.67	.002	229.15	.002	286.64	.001
04348>	45.50	.002	103.01	.002	160.50	.002	217.99	.002	275.48	.001	04483>	56.75	.002	114.26	.002	171.75	.002	229.24	.002	286.72	.001
04349>	45.58	.002	103.09	.002	160.58	.002	218.07	.002	275.56	.001	04484>	56.83	.002	114.34	.002	171.84	.002	229.32	.002	286.80	.001
04350>	45.67	.002	103.17	.002	160.67	.002	218.16	.002	275.64	.001	04485>	56.92	.002	114.43	.002	171.92	.002	229.40	.002	286.89	.001
04351>	45.75	.002	103.26	.002	160.75	.002	218.24	.002	275.73	.001	04486>	57.00	.002	114.51	.002	172.00	.002	229.49	.002	286.97	.001
04352>	45.83	.002	103.34	.002	160.84	.002	218.32	.002	275.81	.001	04487>	57.08	.002	114.59	.002	172.09	.002	229.57	.002	287.06	.001
04353>	45.92	.002	103.42	.002	160.92	.002	218.41	.002	275.89	.001	04488>	57.17	.002	114.68	.002	172.17	.002	229.65	.002	287.14	.001
04354>	45.99	.002	103.51	.002	161.00	.002	218.49	.002	275.96	.001	04489>	57.25	.002	114.76	.002	172.25	.002	229.74	.002	287.22	.001
04355>	46.08	.002	103.59	.002	161.09	.002	218.57	.002	276.04	.001	04490>	57.33	.002	114.84	.002	172.34	.002	229.82	.002	287.31	.001
04356>	46.17	.002	103.67	.002	161.17	.002	218.66	.002	276.14	.001	04491>	57.42	.002	114.93	.002	172.42	.002	229.90	.002	287.39	.001
04357>	46.25	.002	103.76	.002	161.25	.002	218.74	.002	276.23	.001	04492>	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
04358>	46.33	.002	103.84	.002	161.34	.002	218.82	.002	276.31	.001	04493>	001:01:030-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
04359>	46.42	.002	103.92	.002	161.42	.002	218.91	.002	276.39	.001	04494>	-----#*****-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
04360>	46.50	.002	104.01	.002	161.50	.002	218.99	.002	276.46	.001	04495>	#*****-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
04361>	46.58	.002	104.09	.002	161.58	.002	219.07	.002	276.54	.001	04496>	-----#*****-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
04362>	46.67	.002	104.17	.002	161.67	.002	219.16	.002	276.62	.001	04497>	-----#*****-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
04363>	46.75	.002	104.26	.002	161.75	.002	219.24	.002	276.70	.001	04498>	-----#*****-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
04364>	46.83	.002	104.34	.002	161.84	.002	219.32	.002	276.78	.001	04499>	-----#*****-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
04365>	46.92	.002	104.42	.002	161.92	.002	219.41	.002	276.86	.001	04500>	CALIB NASHYD	Area (ha)=	.27	Curve Number (CN)=72.00						
04366>	47.00	.002	104.51	.002	162.00	.002	219.49	.002	276.94	.001	04501>	01:EX-1 DT= 1.00	Ia (mm)=	8.000	# of Linear Res.(N)= 3.00						
04367>	47.08	.002	104.59	.002	162.09	.002	219.57	.002	277.00	.001	04502>	U.H. Tp(hrs)=	.330								
04368>	47.17	.002	104.67	.002	162.17	.002	219.66	.002	277.14	.001	04503>	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----
04369>	47.25	.002	104.75	.002	162.25	.002	219.73	.002	277.23	.001	04504>	Unit Hyd Opeak (cms)=	.274								
04370>	47.33	.002	104.84	.002	162.34	.002	219.81	.002	277.31	.001	04505>	PEAK FLOW (cms)=	.223 (i)								
04371>	47.50	.002	104.92	.002	162.50	.002	219.99	.002	277.56	.001	04506>	TIME TO PEAK (hrs)=	1.00								
04372>	47.58	.002	105.01	.002	162.59	.002	220.07	.002	277.64	.001	04507>	RUNOFF VOLUME (mm)=	34.829								
04373>	47.67	.002	105.17	.002	162.67	.002	220.16	.002	277.71	.001	04508>	TOTAL RAINFALL (mm)=	86.599								
04374>	47.75	.002	105.26	.002	162.75	.002	220.24	.002	277.73												

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04591> TIME TO PEAK (hrs)= 1.317
04592> RUNOFF VOLUME (mm)= 30.328
04593> TOTAL RAINFALL (mm)= 86.599
04594> RUNOFF COEFFICIENT = .350
04595>
04596> (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
04597>
04598> 001:0135-----
04600> | COMPUTE DURALHYD | Average inlet capacities [CINLET] = .001 (cms)
04601> | TotalHyd 05:EX-4 | Number of inlets in system [NINLET] = 1
04602> | Total minor system capacity = .001 (cms)
04603> Total major system storage [TMJSTO] = 99999. (cu.m.)
04604> ID: NHYD AREA QPEAK TPEAK R.V. DWF
04605> (ha) (cms) (hrs) (mm) (cms)
04607> TOTAL HYD. 05:EX-4 2.59 .262 1.317 30.328 .000
04609> -----
04610> MAJOR SYST 06:BANMAN .00 .000 .000 .000
04611> MINOR SYST 07:toDRAI 2.59 .001 273.550 30.329 .000
04612>
04613> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
04614>
04615> Maximum MAJOR SYSTEM storage used = 777. (cu.m.)
04616>
04617> 001:0136-----
04618> -----
04620> | CALIB STANDHYD | Area (ha)= 6.64
04621> | 05:C201 DT= 1.00 | Total Imp(%)= 90.00 Dir. Conn. (%)= 80.00
04622>
04623> IMPERVIOUS PEROVIOUS (i)
04624> Surface Area (ha)= 5.98 .66
04625> Dep. Storage (mm)= 2.00 5.00
04626> Average Slope (%)= 1.00 2.00
04627> Length (m)= 50.00 25.00
04628> Mannings n = .013 .250
04629>
04630> Max.eff.Inten.(mm/hr)= 274.73 252.84
04631> TIME TO PEAK over (min)= 1.00 5.00
04632> Storage Coeff. (min)= 1.13 (ii) 4.80 (iii)
04633> Unit Hyd. Tpeak (min)= 1.00 5.00
04634> Unit Hyd. peak (cms)= 1.00 .23
04635> *TOTALS*
04636> PEAK FLOW (cms)= 4.02 .33 4.250 (iii)
04637> TIME TO PEAK (hrs)= 1.00 1.07 1.000
04638> RUNOFF VOLUME (mm)= 84.60 42.79 76.237
04639> TOTAL RAINFALL (mm)= 86.60 86.60 86.599
04640> RUNOFF COEFFICIENT = .98 .49 .880
04641>
04642> (i) CN PROCEDURE SELECTED FOR PEROVIOUS LOSSES:
04643> CN* = 61.0 Ia = Dep. Storage (Above)
04644> (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
04645> THAN THE STORAGE COEFFICIENT.
04646> (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
04647>
04648> 001:0137-----
04649> -----
04651> | ADD HYD (POST ) ID: NHYD AREA QPEAK TPEAK R.V. DWF
04652> |----- (ha) (cms) (hrs) (mm) (cms)
04653> | ID1 01:EX-2 .19 .041 1.10 38.97 .000
04654> | ID2 03:toDRAIN 2.37 .001 287.43 34.83 .000
04655> | ID3 04:EX-3 .45 .238 1.00 59.38 .000
04656> | ID4 05:C201 6.64 4.250 1.00 76.24 .000
04657> | ID5 07:toDRAIN 2.59 .001 273.55 30.33 .000
04658> -----
04659> SUM 09:POST 12.24 4.514 1.00 57.28 .000
04660>
04661> NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
04662>
04663>
04664> 001:0138-----
04665> -----
04666> | ROUTE RESERVOIR | Requested routing time step = 1.0 min.
04667> | IN>0:(POST ) | ===== OUTFLOW STORAGE TABLE =====
04668> | OUT<01:(SWMF ) | ===== OUTFLOW STORAGE TABLE =====
04669> -----
04670> OUTFLOW STORAGE OUTFLOW STORAGE
04671> (cms) (ha.m.) (cms) (ha.m.)
04672> .000 .0000E+00 .079 .1497E+00
04673> .059 .1884E-01 .080 .1683E+00
04674> .069 .3388E-01 .082 .1855E+00
04675> .070 .4885E-01 .083 .2077E+00
04676> .072 .6383E-01 .085 .2276E+00
04677> .073 .8041E-01 .086 .2485E+00
04678> .075 .9693E-01 .087 .2700E+00
04679> .076 .1140E+00 .089 .4003E+00
04679> .078 .1316E+00 .000 .0000E+00
04680>
04681> ROUTING RESULTS AREA QPEAK TPEAK R.V.
04682> ----- (ha) (cms) (hrs) (mm)
04683> INFLOW >09: (POST ) 12.24 4.514 1.000 57.283
04684> OUTFLOW<01: (SWMF ) 12.24 .296 1.683 57.285
04685> OVERFLOW<02: (000003) .00 .000 .000 .000
04686>
04687> TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
04688> CUMULATIVE TIME OF OVERFLOWS (hours)= .00
04689> PERCENTAGE OF TIME OVERFLOWING (%)= .00
04690>
04691>
04692> PEAK FLOW REDUCTION [Qout/Qin] (%)= 6.568
04693> TIME SHIFT OF PEAK FLOW (min)= 41.00
04694> MAXIMUM STORAGE USED (ha.m.)=.3988E+00
04695>
04696>
04697> 001:0139-----
04698> -----
04699> | DIVERT HYD |
04700> | INID=01 (SWMF ) |
04701> -----
04702> Outflow / Inflow Relationships
04703> Flow 03 + Flow 04 + Flow 05 = Total
04704> (cms) (cms) (cms) (cms)
04705> .000 .000 .000 .000
04706> .000 .059 .000 .059
04707> .007 .061 .000 .069
04708> .007 .063 .000 .070
04709> .008 .064 .000 .072
04710> .008 .065 .000 .073
04711> .008 .066 .000 .075
04712> .009 .068 .000 .076
04713> .009 .069 .000 .078
04714> .009 .070 .000 .079
04715> .009 .071 .000 .080
04716> .010 .072 .000 .082
04717> .010 .073 .000 .083
04718> .010 .074 .000 .085
04719> .010 .075 .000 .086
04720> .011 .077 .000 .087
04721> .011 .078 .210 .299
04722>
04723> NHYD AREA QPEAK TpeakDate_hh:mm R.V. NFE WetHrs
04724> (ha) (cms) (hrs) (mm) (hrs)
04725> IDIn = 01:SWMF 12.24 .296 No_date 1:41 57.285 1 295.

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APPENDIX C

SUPPORTING CALCULATIONS

Upstream of Maintenance Hole R20

Pipe Storage			
Description	Pipe Size (mm)	Length (m)	Volume (m³)
R20 - R9	750	42.9	18.95
R9 - CB	300	21.5	1.52
R9 - R8	600	28.3	8.00
R8 - R7	600	32.8	9.27
R7 - R6	600	37.0	10.46
R6 - RYCB	300	52.3	3.70
R6 - R5	600	8.3	2.35
R5 - R4	525	25.5	5.52
R4 - R3	525	35.0	7.58
R3 - R2	450	41.6	6.62
R2 - R1	300	25.9	1.83
R20 - R19	750	28.0	12.37
R19 - R18	750	32.5	14.36
R18 - R17	750	71.6	31.63
R17 - R16	750	35.9	15.86
R16 - R15	750	30.6	13.52
R15 - CB	300	17.8	1.26
R15 - R14	600	45.0	12.72
R14 - R13	525	31.6	6.84
R13 - R12	525	11.5	2.49
R12 - R11	450	52.9	8.41
R12 - RYCB	300	77.2	5.46
R11 - R10	300	8.3	0.59
TOTAL			146

Structure Storage					
Structures	Diameter (mm)	Invert (m)	Lid (m)	Height (m)	Vol @ Max Ponding
R1	1200	234.42	236.69	2.23	2.52
R2	1200	234.25	236.80	2.40	2.71
R3	1200	234.07	236.59	2.52	2.85
R4	1200	233.94	236.41	2.47	2.79
R5	1200	233.83	236.55	2.72	3.08
R6	1200	233.78	236.61	2.83	3.20
R7	1200	233.64	236.53	2.89	3.27
R8	1200	233.45	236.37	2.92	3.30
R9	1500	233.28	236.50	3.22	5.69
R10	1200	234.06	236.81	2.59	2.93
R11	1200	233.99	236.74	2.66	3.01
R12	1200	233.77	236.47	2.70	3.05
R13	1200	233.70	236.41	2.71	3.06
R14	1200	233.56	236.57	3.01	3.40
R15	1800	233.37	236.57	3.20	8.14
R16	1500	233.28	236.37	3.09	5.46
R17	1500	233.18	236.54	3.36	5.94
R18	1500	233.05	236.48	3.43	6.06
R19	1500	232.93	236.32	3.39	5.99
R20	1800	232.83	236.52	3.69	9.39
TOTAL					86

Max Ponding (m)	236.65	Total Storage Volume Available (m³)	232
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Stage (m)	Depth (m)	Main Pond			Underground Storage		Surface Ponding	Total Pond Volume (m³)	Comments	Stage (m)
		Area (m²)	Volume (m³)	Cumulative Volume (m³)	Incremental Volume (m³)	Cumulative Volume (m³)				
235.00	0.00	0	0	0	188	188	0	188		235.00
235.20	0.20	1447	145	145	6	194	0	339	Bottom of Dry Pond	235.20
235.30	0.30	1497	147	292	3	197	0	489		235.30
235.40	0.40	1547	152	444	3	200	0	644		235.40
235.50	0.50	1598	157	601	3	203	0	804		235.50
235.60	0.60	1650	162	764	3	206	0	969		235.60
235.70	0.70	1702	168	931	3	208	0	1140		235.70
235.80	0.80	1756	173	1104	3	211	0	1316		235.80
235.90	0.90	1810	178	1283	3	214	0	1497		235.90
236.00	1.00	1864	184	1466	3	217	0	1683		236.00
236.10	1.10	1920	189	1655	3	220	0	1875		236.10
236.20	1.20	1976	195	1850	3	223	0	2073		236.20
236.30	1.30	2033	200	2051	3	226	0	2276		236.30
236.40	1.40	2090	206	2257	3	228	0	2485		236.40
236.50	1.50	2166	213	2470	2	230	0	2700	Top of Pond	236.50
236.65	1.65	0	0	2470	1	232	1302	4003		236.65
									Emergency Overland Spill Point	

SWMF
Stage-Storage-Discharge
Information

10919 Longwoods Road Light Industrial

Project Number: LD-00318

2023-11-20

Orifice Calculation			
$Q_o = C_d A \sqrt{2gH_o}$			
	Orifice 1	Orifice 2	Orifice 3
C_d	0.63	0.63	-
Invert (m)	232.83	236.55	-
Diameter/Height (m)	0.135	0.55	-
Area(m^2)	0.014	0.238	-

Infiltration Rate	
Infiltration Rate (mm/hr)	18
Bottom Contact Area (m^2)	1447
Top Contact Area (m^2)	2166

Stage	Infiltration	Orifice 1		Orifice 2		Total Flow (m^3/s)	Active Volume	
		Flow (m^3/s)	H_o (m)	Flow (m^3/s)	H_o (m)		(m^3)	(ha-m)
235.00	0.000	2.17	0.059	0.00	0.000	0.059	188	0.01884
235.20	0.007	2.37	0.061	0.00	0.000	#REF!	339	0.03388
235.30	0.007	2.47	0.063	0.00	0.000	0.070	489	0.04889
235.40	0.008	2.57	0.064	0.00	0.000	0.072	644	0.06439
235.50	0.008	2.67	0.065	0.00	0.000	0.073	804	0.08041
235.60	0.008	2.77	0.066	0.00	0.000	0.075	969	0.09693
235.70	0.009	2.87	0.068	0.00	0.000	0.076	1140	0.11398
235.80	0.009	2.97	0.069	0.00	0.000	0.078	1316	0.13156
235.90	0.009	3.07	0.070	0.00	0.000	0.079	1497	0.14967
236.00	0.009	3.17	0.071	0.00	0.000	0.080	1683	0.16833
236.10	0.010	3.27	0.072	0.00	0.000	0.082	1875	0.18753
236.20	0.010	3.37	0.073	0.00	0.000	0.083	2073	0.20730
236.30	0.010	3.47	0.074	0.00	0.000	0.085	2276	0.22762
236.40	0.010	3.57	0.075	0.00	0.000	0.086	2485	0.24850
236.50	0.011	3.67	0.077	0.00	0.000	0.087	2700	0.26999
236.65	0.011	3.82	0.078	0.10	0.210	0.299	4003	0.40033

APPENDIX D
OGS SIZING SHEET



ADS OGS Sizing Summary

Project Name: 10919 Longwoods Rd

Consulting Engineer: LDS Consultants Inc.

Location: Delaware, ON

Sizing Completed By: C. Neath **Email:** cody.neath@ads-pipe.com

Treatment Requirements	
Treatment Goal:	Enhanced (MOE)
Selected Parameters:	80% TSS 90% Volume
Selected Unit:	FD-8HC

Summary of Results		
Model	TSS Removal	Volume Treated
FD-4HC	70.0%	83.6%
FD-5HC	74.0%	>90%
FD-6HC	76.0%	>90%
FD-8HC	80.0%	>90%
FD-10HC	83.0%	>90%

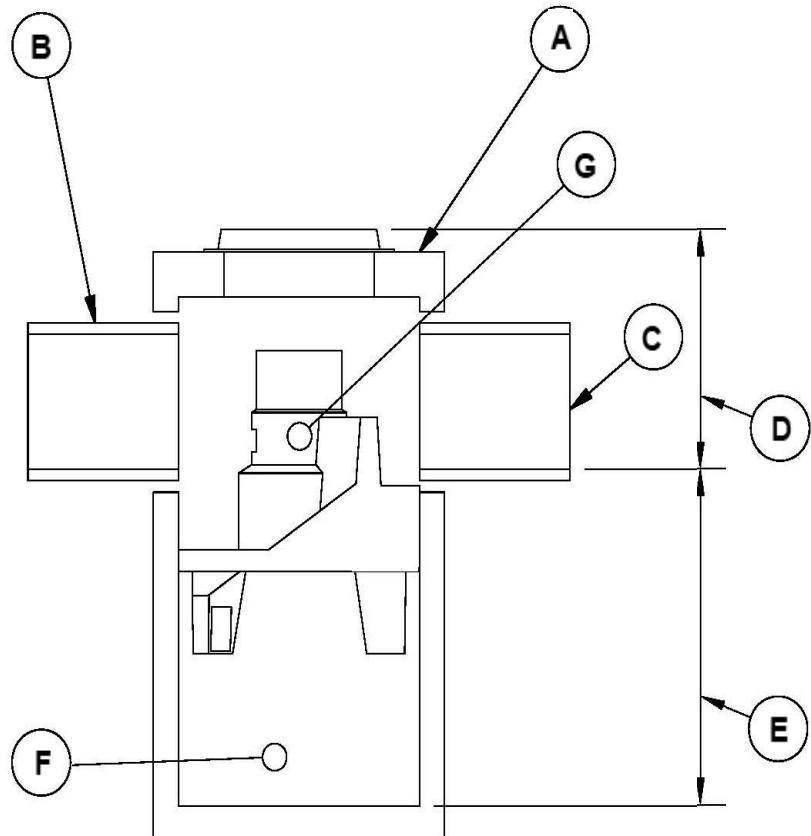
FD-8HC Specification	
Unit Diameter (A):	2,400 mm
Inlet Pipe Diameter (B):	600 mm
Outlet Pipe Diameter (C):	600 mm
Height, T/G to Outlet Invert (D):	2500 mm
Height, Outlet Invert to Sump (E):	2260 mm
Sediment Storage Capacity (F):	3.47 m ³
Oil Storage Capacity (G):	4,239 L
Recommended Sediment Depth for Maintenance:	465 mm
Max. Pipe Diameter:	1,200 mm
Peak Flow Capacity:	1,415 L/s

Site Elevations:	
Rim Elevation:	100.00
Inlet Pipe Elevation:	97.50
Outlet Pipe Elevation:	97.50

Notes:

Removal efficiencies are based on NJDEP Test Protocols and independently verified.

All units supplied by ADS have numerous local, provincial, and international certifications (copies of which can be provided upon request). The design engineer is responsible for ensuring compliance with applicable regulations.





Project Name: 10929 Longwoods Rd
 Consulting Engineer: LDS Consultants Inc.
 Location: Delaware, ON

Net Annual Removal Efficiency Summary: FD-8HC

Rainfall Intensity ⁽¹⁾	Fraction of Rainfall ⁽¹⁾	FD-8HC Removal Efficiency ⁽²⁾	Weighted Net-Annual Removal Efficiency
mm/hr	%	%	%
0.50	0.2%	95.5%	0.2%
1.00	13.7%	89.5%	12.3%
1.50	17.3%	86.2%	14.9%
2.00	13.5%	83.9%	11.4%
2.50	2.7%	82.2%	2.2%
3.00	2.3%	80.8%	1.8%
3.50	8.5%	79.7%	6.8%
4.00	4.7%	78.7%	3.7%
4.50	1.5%	77.8%	1.1%
5.00	5.2%	77.1%	4.0%
6.00	4.1%	75.8%	3.1%
7.00	4.4%	74.7%	3.3%
8.00	3.3%	73.8%	2.4%
9.00	2.4%	73.0%	1.8%
10.00	2.3%	72.3%	1.7%
20.00	9.2%	67.7%	6.2%
30.00	2.5%	65.2%	1.6%
40.00	1.1%	63.5%	0.7%
50.00	0.4%	62.2%	0.3%
100.00	0.6%	58.3%	0.4%
150.00	0.1%	56.2%	0.1%
200.00	0.0%	54.7%	0.0%
Total Net Annual Removal Efficiency:			79.9%
Total Runoff Volume Treated:			>90%

Notes:

- (1) Rainfall Data: 1960:2002, HLY03, London AP, ONT, 6144475.
- (2) Based on third party verified data and approximating the removal of a PSD similar to the STC Fine distribution
- (3) Rainfall adjusted to 5 min peak intensity based on hourly average.

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