



MTE Consultants
123 St. George St., London, Ontario N6A 3A1

July 13, 2020

MTE File No.: C45013-200

County of Middlesex
399 Ridout Street North
London, ON N6A 2P1

Attention: Durk Vanderwerff, Director of Planning

**RE: Preliminary Stormwater Management Report
For Vacant Land Condominium Development (Light Industrial Sites)
at 10919 Longwood Road, Delaware**

Introduction:

It is proposed to develop the property at 10919 Longwood Road, Delaware in the Municipality of Middlesex Center. The development property is 6.64 Ha in size and is located south of Longwoods Road on the east side of Delaware. The property is zoned for light industrial use. It is proposed to develop the property into 15 individual lots for light industrial use. The lots will range from 0.30 to 0.46 Ha in size. The lots will be created through a vacant land condominium which will contain a private internal roadway to provide access to the lots and a private stormwater management (SWM) basin which will provide a stormwater outlet for the lots. The private roadway and SWM basin will be common elements within the condo development.

Please refer to the attached Draft Plan of Vacant Land Condominium (DWG-1) which shows the proposed development. This letter report outlines the proposed storm drainage and stormwater management for the development in support of draft plan approval.

Pre-development Conditions:

The pre-development site is farmland. The pre-development drainage patterns are outlined below:

- The southerly 1.8 Ha of development drains to the south onto the adjacent farm.
- The remainder 4.85 Ha of the development drains to multiple low lying areas throughout the property where the runoff infiltrates into the ground.

MTE Consulting completed a detailed geotechnical investigation for the property. The existing soils are a mixture of sand and silt. (Reference: Geotechnical Investigation for Proposed Industrial Subdivision at 10919 Longwoods Road, MTE Consultants Inc., March 27, 2019).

Proposed Post-Development Site:

Please refer to the attached Draft Plan of Vacant Land Condominium (DWG-1) and the Preliminary Grading Plan (DWG-2). It is proposed to drain the development as follows:

- Each lot will be individually serviced with internal storm sewers and/or ditches which will discharge stormwater runoff to the ditching system located within the private roadway corridor.
- The private roadway corridor will contain roadside ditches on both sides of the asphalt road. The ditches will be approximately 0.80m deep with 4:1 side slopes and a 1m wide flat bottom. The ditches will be grassed with a minimum slope of 0.50% and will drain into the north portion of the proposed SWM basin. Culverts will be installed at the intersection and at future driveways.
- The rear of lots 8-15 will drain into a rear yard swale system, located at the south edge of the development. These swales will be grassed with a 0.50% minimum slope and will drain into the south portion of the proposed SWM basin.
- The roadway ditches and rear yard swales will all outlet a private SWM basin which will be located between lots 13 and 14. The SWM basin will be 0.51 Ha in size and will infiltrate stormwater runoff into the ground in order to match and mimic the pre-development condition.

Infiltration Basin Design:

MTE Consulting completed on-site infiltration testing and determined that the factored infiltration rate of the sandy soils at the infiltration basin location is 18mm/hr. The infiltration rate contains a factor of safety of 3. (Reference: Letter Results of In-situ Infiltration Testing, Proposed Industrial Subdivision, 10919 Longwoods Road, Middlesex Centre, MTE Consultants Inc., July 3, 2020). The following details outline the proposed design of the infiltration basin:

- Drainage Area = 6.65 Ha (including the area of the basin itself)
- Bottom Area of Basin = 0.28 Ha
- Top Area of Basin (to top of slope) = 0.43 Ha
- Block Size = 0.51 Ha
- Side slopes = 4:1 max
- Bottom and sides of infiltration basin will be topsoil and grassed
- Factored infiltration rate = 18mm/hr (contains a factor of safety of 3)
- Total infiltration rate for facility $0.28 \text{ Ha} \times 10,000\text{m}^2/\text{Ha} \times 18\text{mm}/\text{hr} / 1000 = 50.4\text{m}^3/\text{hr} = 0.014\text{m}^3/\text{sec}$
- Estimated maximum ground water table elevation = 233.60
- Proposed bottom of basin = 234.80
- Estimated clearance (bottom of basin to estimated ground water) = 1.20m

Hydraulic Modelling for Infiltration Basin:

The post-development tributary area to the infiltration basin is outlined below:

- Private Light Industrial Lots = 4.96 Ha (maximum impervious area = 60%)
- Private Roadway Corridor with ditches = 1.17 Ha (impervious area = 45%)
- Private SWM Facility = 0.51 Ha (equivalent impervious area = 50%)
- Total Area = 6.65 Ha, Composite Impervious = 58%
- To be conservative, we have used an overall Composite Impervious Ratio of 60%

As noted on the Preliminary Grading Plan (DWG-2), there appear to be areas from Longwood Road which drain onto the development lands. As shown on the plan, we anticipate and recommend the drainage from the road allowance area be conveyed to the east/west such that the road allowance runoff does not drain onto the private development.

We have completed hydraulic models for the inflow/outflow/ponding of the infiltration basin using SWMHYMO-99. The City of London IDF curves were used to model the following storm events:

- 25mm, 4 hour Chicago Storm
- 1:2 year, 4 hour Chicago Storm
- 1:5 year, 4 hour Chicago Storm
- 1:10 year, 4 hour Chicago Storm
- 1:50 year, 4 hour Chicago Storm
- 1:100 year, 4 hour Chicago Storm

To be conservative, we have used a 4 hour storm duration instead of a 3 hour duration.

As noted previously, the pond infiltration rate (outflow rate) was set at 0.014m³/s which contains a factor of safety of 3.

The attached Table 1 outlines the infiltration basin storage volumes and associated draw down times during each storm event. Detailed SWMHYMO-99 output is also attached.

Infiltration Basin Ponding Depths and Surface Outflow:

Please refer to Table 1 for the estimated ponding depths for each storm event. Please also refer to the attached Pond Cross Section (DWG-3).

The bottom of the basin has been set at 234.80.

1:2 year storm estimated ponding elevation is 235.40 (depth = 0.60m). Small amounts of ponding of 0.30m will occur in isolated areas in the adjacent roadside ditches to an elevation 235.40. To be conservative, storage volumes and infiltration for the roadside ditching has not been factored into this analysis.

The 1:100 year storm estimated ponding elevation is 235.95 (depth = 1.15m). The maximum grade around of the SWM basin is 236.40. As such there is 0.45m freeboard. Ponding of 0.85m will also occur in the roadside ditch to elevation 235.95. However, the majority of the ditch (average elevation of 359.90) will only have 0.05m ponding.

An emergency overflow to the south is provided at elevation 236.20, which is 0.25m higher than the facility storage level for the 1:100 year storm event.

The infiltration basin has been designed to infiltration upto the 1:100 year storm event. As such there should be no surface run-off onto adjacent properties, under normal operating conditions.

Quality Control:

As previously outlined, the development will consist of 15 light industrial lots. The development of each lot will be subject to future Site Plan approvals which will require detailed engineering, grading and stormwater management plans be provided for each lot. Each lot will need to provide an OGS unit such that quality control for the development is provided. The OGS units shall be designed for Level 1 protection. Depending on the end use of each lot, lots with less than 250m² of total asphalt area may be able to use swales and landscape treatment instead of an oil grit separator. This will be determined and assessed on an individual lot basis during the site plan process for each lot.

Construction Staging for Infiltration Basin:

The infiltration basin should be completed at the initial stages of the development. Active sediment and erosion controls shall be implemented to decrease sediment load into the basin during construction. After the overall site is 85% built out (i.e. 85% of the individual lots are completed including asphalt, vegetation and sodding), the pond will be sub-excavated to remove any accumulated silt. After 85% built-out the following will occur:

- MTE Consulting will inspect the pond bottom and take soil samples.
- The basin bottom including the bottom 2m of each side slope will be sub-excavated to 0.30m minimum depth. The excavated material shall be removed from the site and replaced with 0.30m depth of imported clean sand (no silt/clay). The purpose of this operation is to remove any contaminated sand, silt and sediment that has accumulated in the pond during development construction.
- A 150mm depth of sandy topsoil mix shall be installed on top of the new sand layer.
- The native sand and the imported 0.30m of sand should not be compacted and the top layers of both the native sand and the imported sand shall be scarified prior to the installation of the topsoil mix.

Topsoil and Seeding for Infiltration Basin:

Topsoil and seed shall be installed on the basin bottom and the 4:1 side slopes. It is important that the topsoil is very pervious and a 30/70 sand to topsoil mix shall be used for the topsoil layer within the basin. The topsoil layer will have a maximum thickness of 150mm and shall be seeded (not sodded). The seeding mix shall be Native Prairie Meadow Mix.

Initial Monitoring of the Infiltration Basin:

After the overall development is 85% built out and the basin seeding has been established, MTE Consulting will monitor the basin for a 1 year period. The purpose of the monitoring is to ensure the basin is functioning properly and within the design parameters. If the basin is not functioning properly MTE will provide recommendations for any remediation work.

On-going Maintenance of Infiltration Basin:

The infiltration basin will be privately owned and operated by the condo board. The condo board shall complete yearly monitoring and maintenance of the infiltration basin.

The condo board shall undertake the following maintenance and shall allow for the associated costs in the condo board reserve fund:

- The grass areas within the pond shall be cut on a regular basis and pond area shall be kept free of garbage and debris.
- Every five (5) years, the basin bottom and bottom 2m of the side slopes shall be fully excavated by 0.30m. The 0.15m thickness of topsoil and 0.15m thickness of sand below the topsoil shall be removed and replaced with new clean sand and topsoil (with no clay/silt content). The replacement of these materials every 5 years will be required in order to keep the infiltration basin functioning.

Conclusions

This letter report outlines the proposed storm drainage and stormwater management for the development in support of the draft plan approval. We anticipated an updated report will be prepared as a condition of draft plan approval.

In summary, the development consists 15 individual lots for light industrial use which will be development through a vacant land condominium. The stormwater drainage for the development will outlet to a stormwater infiltration basin. The infiltration basin is 0.51 Ha in size and has been designed to accommodate the 1:100 post-development flows from the development. The infiltration basin, private roadway and conveyance ditches will be privately owned and maintained by the condominium board.

Level 1 stormwater quality controls will be provided on the individual lots prior to discharge to the internal roadway ditch system. The development of the individual lots will be subject to future site plan approvals which will require detailed engineering, grading and stormwater management plans be provided for each lot.

Please contact us if you have any comments or questions.

Yours Truly,

MTE Consultants Inc.

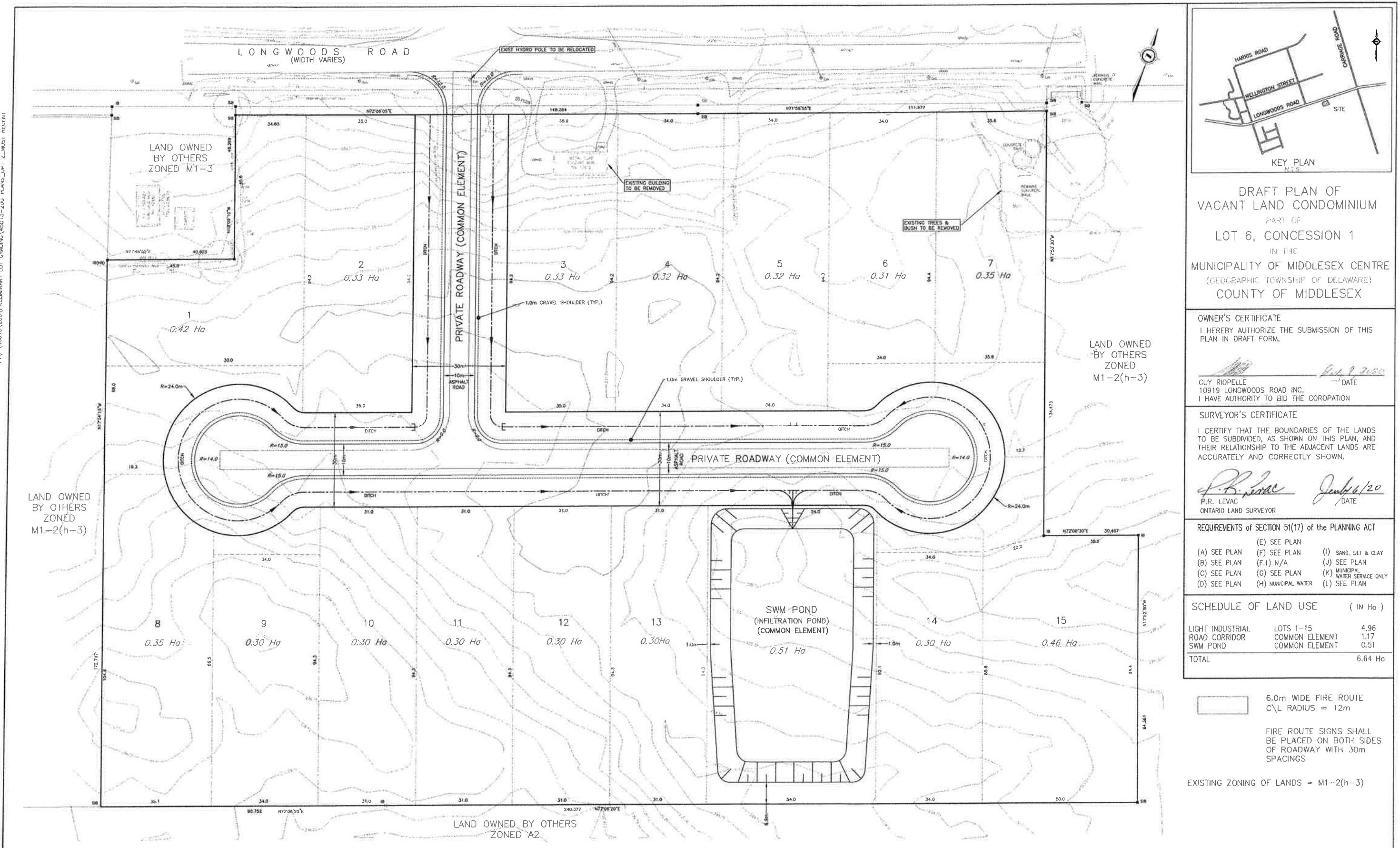


Kyle McIntosh, P. Eng.
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kmcintosh@mte85.com

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Table 1: Infiltration Basin Calculations

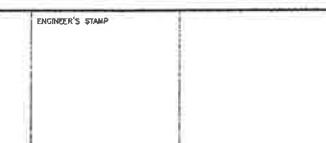
Design Storm	Runoff volume to infiltration basin (m ³)	Infiltration Basin Infiltration Rate (m ³ /hour)	Infiltration Amount During Storm (m ³)	Infiltration Basin Total Storage Required (m ³)	Drain down time after storm event (hours)	Infiltration Basin Estimated Ponding Depth (m)
25mm, 4 hours	918	50	202	716	14	0.35
1:2 year, 4 hours	1915	50	202	1713	34	0.6
1:5 year, 4 hours	2006	50	202	1804	36	0.7
1:10 year, 4 hours	2447	50	202	2245	45	0.8
1:50 year, 4 hours	3425	50	202	3223	64	0.95
1:100 year, 4 hours	3853	50	202	3651	72	1.15



EXISTING SERVICES	DRAWING # SOURCE	CONSTRUCTION DATE	CONSTRUCTED SERVICES	COMPLETION	DETAILS	No.	REVISIONS	DATE
					DESIGN: KAH			
					DRAWN BY: HSA			
					CHECKED: KAH			
					APPROVED: KAH			
					DATE: JULY 20			

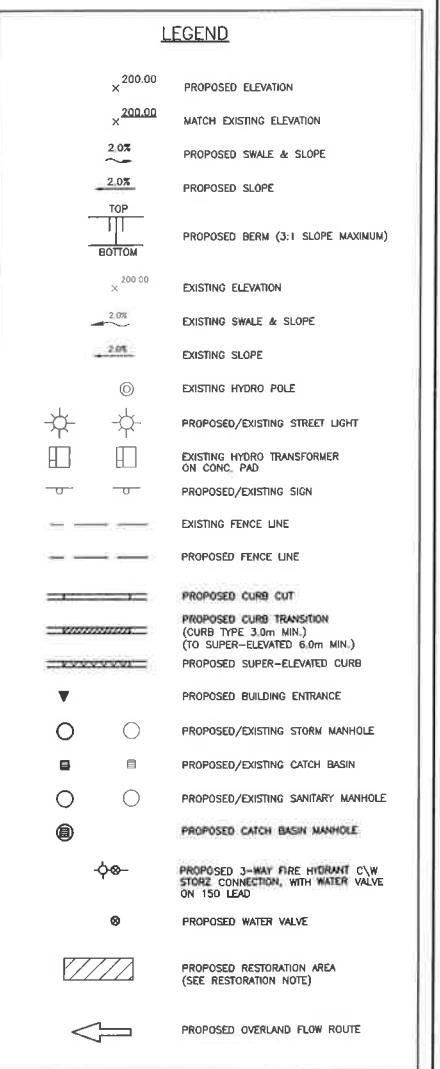
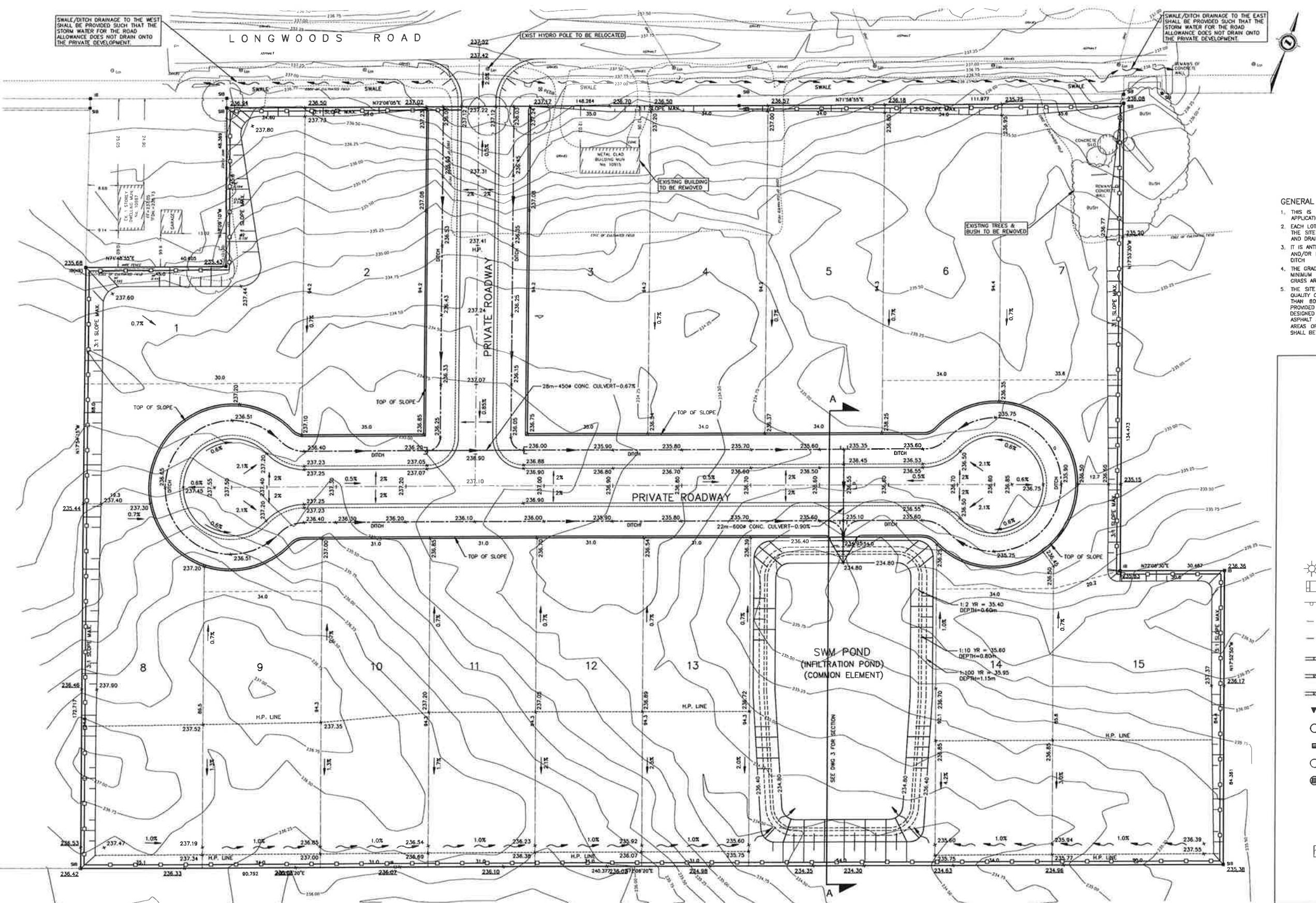


Engineers, Scientists, Surveyors



SCALE 1 : 500
5m 0 10m

LOT 6, CONCESSION 1 MUNICIPALITY OF MIDDLESEX CENTRE	PROJECT NO. 45013-200
DRAFT PLAN OF VACANT LAND CONDOMINIUM	SHEET NO. 1
	PUR FILE NO.



EXISTING SERVICES	DRAWING #, SOURCE	CONSTRUCTION DATE	CONSTRUCTED SERVICES	COMPLETION	DETAILS	No.	REVISIONS	DATE	CONSULTANT
					DESIGN KMM DRAWN BY KMM CHECKED KMM APPROVED KMM DATE JULY/20				

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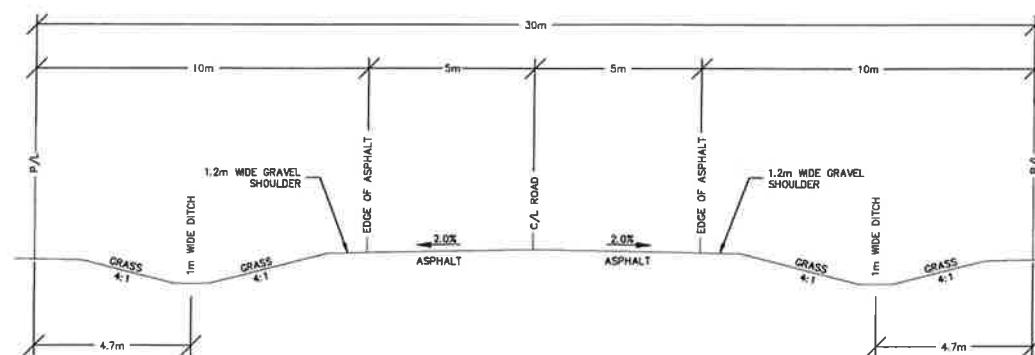
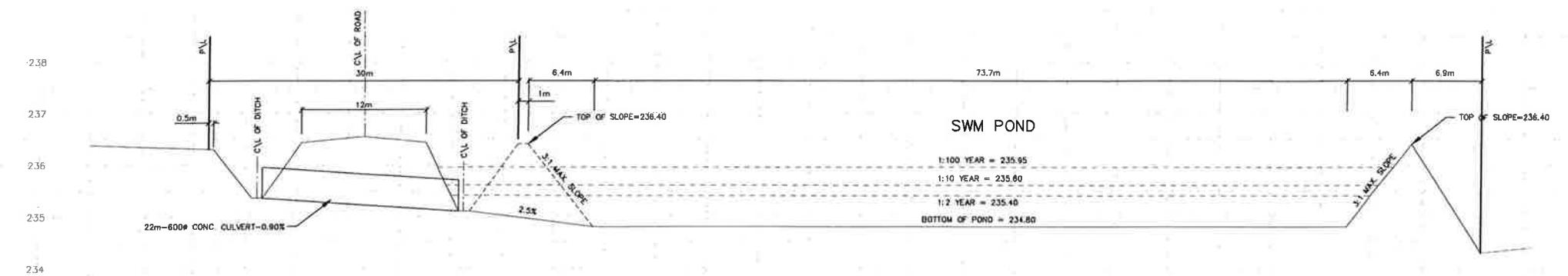
ENGINEER'S STAMP

SCALE

SCALE - 1:500
5 0 10m

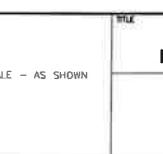
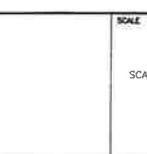
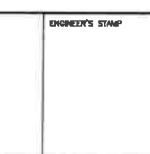
TITLE
LOT 6, CONCESSION 1
MUNICIPALITY OF MIDDLESEX CENTRE
PRELIMINARY GRADING PLAN

PROJECT No. 45013-200
SHEET No.
2
FILE No.

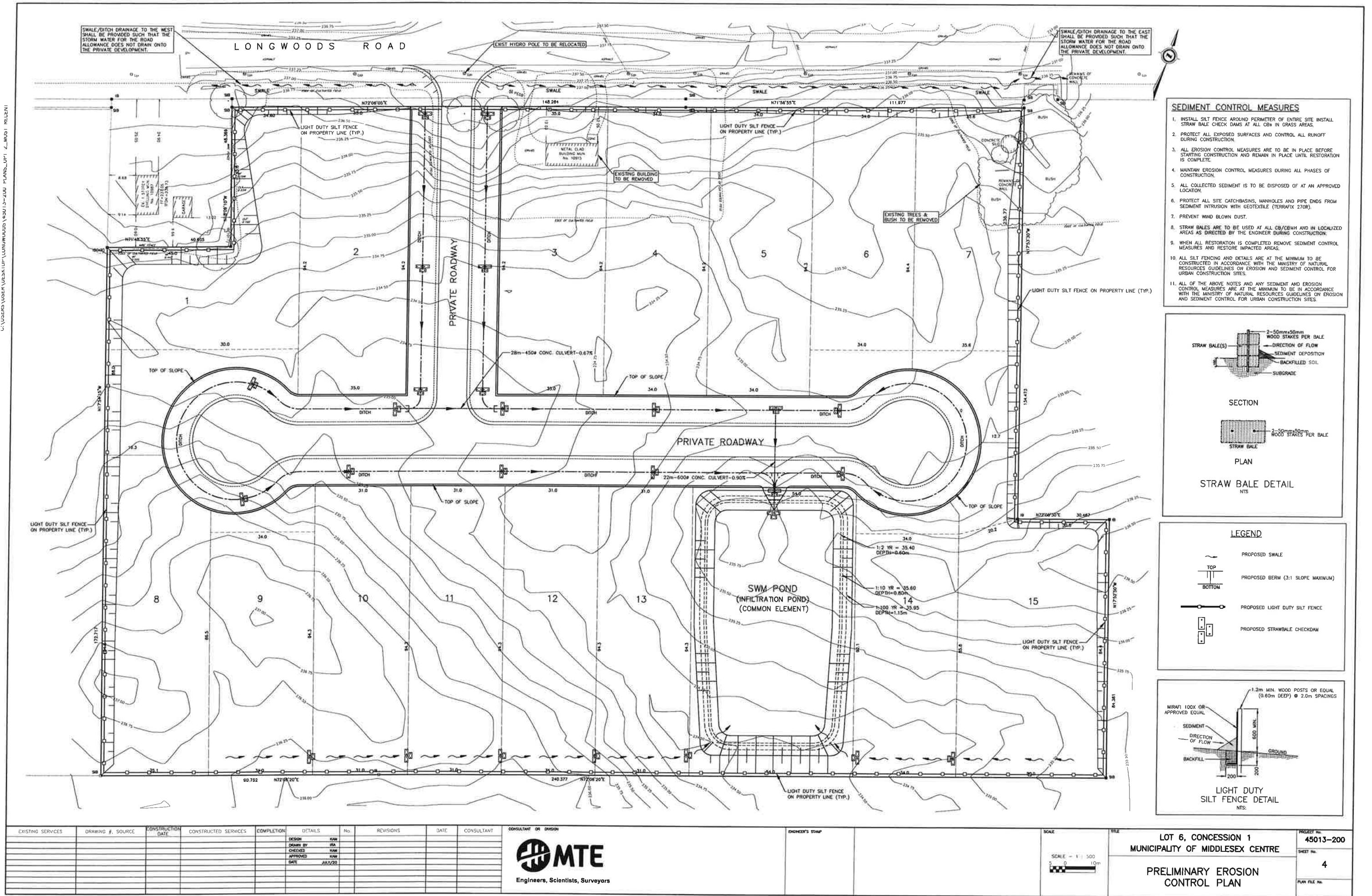


EXISTING SERVICES	DRAWING #, SOURCE	CONSTRUCTION DATE	CONSTRUCTED SERVICES	COMPLETION	DETAILS	No.	REVISIONS	DATE	CONSULTANT	CONSULTANT OR DIVISION	
										DESIGN	DRAWN BY
					KAW					CHEKED	KAW
										APPROVED	KAW
										DATE	JUN/20

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LOT 6, CONCESSION 1
MUNICIPALITY OF MIDDLESEX CENTRE
PROJECT No.
45013-200
SHEET No.
3
DETAILS
PLAN FILE No.



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***** A single event and continuous hydrologic simulation model
***** based on the principles of HYMO and its successors
***** OTHYMO-83 and OTHYMO-82
*****
***** Distributed by:
J.F. Sabourin and Associates Inc.
Ottawa, Ontario: (613) 836-3884
Gatineau, Quebec: (819) 243-6858
E-Mail: smhymo@jisa.com
*****
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***** PROGRAM ARRAY DIMENSIONS *****
Maximum value for ID numbers : 10
Max. number of rainfall points: 105408
Max. number of flow points: 105408
```

DETAILED OUTPUT

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DATE: 2020-06-25 TIME: 20:05:39 RUN COUNTER: 000932
Input filename: Q:\45013\200\SMH\HYMO60%TINP.dat
Output filename: Q:\45013\200\SMH\HYMO60%TINP.out
Summary filename: Q:\45013\200\SMH\HYMO60%TINP.sum
User comments:
 1;
 2;
 3;
```

```
Project Name: [10919 LONGWOODS ROAD INDUSTRIAL SUBDIVISION] Project Number:
Date: MARCH 2020
Modeler: [NAME]
Company: MTE CONSULTANTS INC.
License #: [NAME]
```

```
START Project dir.: Q:\45013\200\SMH\HYMO60%TINP\
Rainfall dir.: Q:\45013\200\SMH\HYMO60%TINP\
TZERO = 200 hrs on 0
METCUT= 2 (output = METRIC)
NRUN = 001
NSTORM= 1
# 1=25mm.HYT
```

```
READ STORM Ptotal= 24.87 mm
TIME RAIN TIME RAIN TIME RAIN
hrs mm/hr hrs mm hr hrs mm hr
.06 1.326 1.17 3.776 2.25 5.139 3.33 1.856
.08 1.391 1.25 4.485 2.33 4.685 3.42 1.774
```

PROPOSED SITE		PROPOSED LONGWOODS ROAD INDUSTRIAL SUBDIVISION	
		CALIB:201 DT: 5.00	Area (ha) = 6.65 Total Imp(%) = 60.00 Dir. Conn. (%) = 50.00
			PREVIOUS PREVIOUS
			Surface Area (ha) = 3.99
			Dep Storage (mm) = 2.00
			Average Slope (%) = 1.00
			Length (m) = 80.00
			Mannings n = .015
			Max.eff.Inten.(mm/hr) = 71.32
			Storage Coeff. (min) = 5.00
			Unit Hyd.-T.Pk (min) = 2.79
			Unit Hyd. Peak (cms) = .28
			TOTALS
			PEAK FLOW (cms) = .58
			TIME TO PEAK (hrs) = 1.67
			RUNOFF VOLUME (mm) = 22.87
			TOTAL RAINFALL (mm) = 24.87
			RUNOFF COEFFICIENT = .92
			*** WARNING: Storage Coefficient is smaller than DT!
			Use a smaller DT or a larger area.
(i)	CN PROCEDURE SELECTED FOR PREVIOUS LOSSES:		
	CN* = 74.0 Ia = Dep. Storage (Above)		
	(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL		
	THAN THE STORAGE COEFFICIENT.		
	(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.		
001:0004	COMPUTE VOLUME		
	ID: 01 (201)	DISCHARGE	TIME
		(cms)	(hrs)
		START CONTROLLING AT	
		INFLOW HYD. PEAKS AT	.000
		STOP CONTROLLING AT	.594
			.017
		REQUIRED STORAGE VOLUME (ha.m.) =	.0817
		TOTAL HYDROGRAPH VOLUME (ha.m.) =	.0918
		% OF HYDROGRAPH TO STORE =	.890146
		NOTE: Storage was computed to reduce the Inflow	
		peak to -017 (cms).	
001:0005	** END OF RUN : 1		

Page 4
Q:\450\13200\SWI\HYMO\60%_TMM Model\POST.out
Printed at 13:01 on 15-JUN-2020

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-----| START |-----| Project dir: Q:\45013\200\SMNHYNO\60TIN-1 \
-----| Rainfall dir: Q:\45013\200\SMNHTMO\60TIN-1 \
-----| TZERO = 0.00 hrs on 0
-----| MEOUT= 002 (output = MEIRIC)
-----| NRIN = 1
-----| NSIORM= 1
-----| 1=2YR.HYT

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Project Name: [10919 LONGWOODS ROAD INDUSTRIAL SUBDIVISION]		Project Number																																																																																																																	
Date: MARCH 2020	Modeler: [MEM]																																																																																																																		
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*AREA 201 -> PROPOSED LONGWOODS ROAD INDUSTRIAL SUBDIVISION																																																																																																																			
CALIB STANDHYD		Area, (ha) =																																																																																																																	
01:201	DI = 5.00	Total Imp (%) =	6.65																																																																																																																
		Dir. Conn. (%) =	50.00																																																																																																																
		PREVIOUS																																																																																																																	
IMPERVIOUS		PREVIOUS (i)																																																																																																																	
Surface Area (ha) = 3.99		2.66																																																																																																																	
Dep. Storage (mm) = 2.00		5.00																																																																																																																	
Average Slope (%) = 1.00		2.50																																																																																																																	
Length (m) = 80.00		8.00																																																																																																																	
Manning's n		.015 * .035																																																																																																																	
Max.eff.Inten.(mm/hr) = 131.99		45.94																																																																																																																	
Storage Coeff. (min) = 5.00		5.00																																																																																																																	
Unit Hyd. Tpeak (min) = 2.18		(i.i)																																																																																																																	
Unit Hyd. peak (cms) = .31		5.00																																																																																																																	
		.18																																																																																																																	
		TOTALS																																																																																																																	
PEAK FLOW (cms) = 1.13		1.25																																																																																																																	
TIME TO PEAK (hrs) = 1.67		1.75																																																																																																																	
RUNOFF VOLUME (mm) = 42.77		44.77																																																																																																																	
TOTAL RAINFALL (mm) = 44.77		44.77																																																																																																																	
RUNOFF COEFFICIENT = .95		.95																																																																																																																	

1.00	\$ 0.68	2.08	13.772		3.17	3.492
1.08	5.795	2.17	11.219		3.25	3.309

PROPOSED SITE

* AREA 201 -> PROPOSED LONGGOODS ROAD INDUSTRIAL SUBDIVISION

CALIB STANDBY	Area (ha) =	6.65
01:201 DT= 5.00	Total Imp (%) =	60.00
	Dir. Conn. (%) =	50.00
	PREVIOUS (i)	
Surface Area (ha) =	3.99	2.66
Dep. Storage (mm) =	2.00	5.00
Average Slope (%) =	1.00	2.00
Length (m) =	80.00	80.00
Manning's n =	.015	.035
Max-eff. Inten. (mm/hr) =	134.79	48.90
Storage Coeff. (min) =	5.00	5.00
Unit Hyd. Peak (min) =	2.16 (ii)	6.26 (ii)
Unit Hyd. Peak (cms) =	5.00	5.00
Unit Hyd. Peak (hrs) =	.31	.19
PEAK FLOW (cms) =	1.16	.26
TIME TO PEAK (hrs) =	1.07	1.75
RUNOFF VOLUME (mm) =	44.18	15.84
TOTAL RAINFALL (mm) =	46.18	46.18
RUNOFF COEFFICIENT =	.96	.34
*** WARNING: Storage Coefficient is smaller than DT!		.649
(i) CN PROCEDURE SELECTED FOR PREVIOUS LOSSES;		
(ii) CN* = 74.0		
(iii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.		
(iv) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.		

Use a smaller DT or a larger area.

(i) CN PROCEDURE SELECTED FOR PREVIOUS LOSSES;

(ii) CN* = 74.0

(iii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.

(iv) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

003:0004

COMPUTE VOLUME DT:01 (201)	DISCHARGE (cms)	TIME (hrs)
START CONTROLLING AT INFLOW HYD. PEAKS AT STOP CONTROLLING AT	.000 1.371 .017	.667 4.136
REQUIRED STORAGE VOLUME (ha.m.) = TOTAL HYDROGRAPH VOLUME (ha.m.) = % OF HYDROGRAPH TO STORE	.1896 .2006 94.5331	
NOTE: Storage was computed to reduce the inflow peak to .017 (cms).		

003:0005		
003:0002		
003:0002 *		
END OF RUN : 3		

Project Name: [10919 LONGWOODS ROAD INDUSTRIAL SUBDIVISION] Project Number: MARCH 2020

Modeler : [MEM]

Company : MTE CONSULTANTS INC.

License #: []

Comments: 10YR Chicago 4-hr duration

TIME	RAIN mm/hr	TIME	RAIN mm hr	TIME	RAIN mm hr	TIME	RAIN mm hr
0.08	2.343	1.17	7.804	2.25	9.514	3.42	3.267
0.17	2.473	1.25	9.514	2.33	9.514	3.42	3.267
0.25	2.616	1.33	12.124	2.42	8.304	3.50	3.112
0.33	2.783	1.42	16.521	2.50	7.361	3.58	2.971
0.42	2.971	1.50	25.144	2.58	6.607	3.67	2.843
0.50	3.187	1.58	47.356	2.67	5.991	3.75	2.726
0.58	3.439	1.67	156.469	2.75	5.481	3.83	2.618
0.67	3.735	1.75	93.617	2.83	5.050	3.92	2.519
0.75	4.089	1.83	47.356	2.92	4.682	4.00	2.428
0.83	4.518	1.92	3.00	4.385	4.08	4.189	3.631
0.92	5.025	2.00	2.499	3.08	4.089	4.08	2.343
1.00	5.125	2.08	16.521	3.17	3.846	3.25	3.631
1.08	6.607	2.17	13.321	3.25			

Comments: 10YR Chicago 4-hr duration

Protocol = 54.60 mm |

004:0002

File Name: 10YR Chicago 4-hr duration

Comments: 10YR Chicago 4-hr duration

TIME

TIME	RAIN mm hr	TIME	RAIN mm hr	TIME	RAIN mm hr
0.08	2.343	1.17	7.804	2.25	9.514
0.17	2.473	1.25	9.514	2.33	9.514
0.25	2.616	1.33	12.124	2.42	8.304
0.33	2.783	1.42	16.521	2.50	7.361
0.42	2.971	1.50	25.144	2.58	6.607
0.50	3.187	1.58	47.356	2.67	5.991
0.58	3.439	1.67	156.469	2.75	5.481
0.67	3.735	1.75	93.617	2.83	5.050
0.75	4.089	1.83	47.356	2.92	4.682
0.83	4.518	1.92	3.00	4.385	4.08
0.92	5.025	2.00	2.499	3.08	4.089
1.00	5.125	2.08	16.521	3.17	3.846
1.08	6.607	2.17	13.321	3.25	3.631

Comments: 10YR Chicago 4-hr duration

Protocol = 54.60 mm |

004:0002

File Name: 10YR Chicago 4-hr duration

Comments: 10YR Chicago 4-hr duration

TIME

TIME	RAIN mm hr	TIME	RAIN mm hr	TIME	RAIN mm hr
0.08	2.343	1.17	7.804	2.25	9.514
0.17	2.473	1.25	9.514	2.33	9.514
0.25	2.616	1.33	12.124	2.42	8.304
0.33	2.783	1.42	16.521	2.50	7.361
0.42	2.971	1.50	25.144	2.58	6.607
0.50	3.187	1.58	47.356	2.67	5.991
0.58	3.439	1.67	156.469	2.75	5.481
0.67	3.735	1.75	93.617	2.83	5.050
0.75	4.089	1.83	47.356	2.92	4.682
0.83	4.518	1.92	3.00	4.385	4.08
0.92	5.025	2.00	2.499	3.08	4.089
1.00	5.125	2.08	16.521	3.17	3.846
1.08	6.607	2.17	13.321	3.25	3.631

Comments: 10YR Chicago 4-hr duration

Protocol = 54.60 mm |

004:0002

File Name: 10YR Chicago 4-hr duration

Comments: 10YR Chicago 4-hr duration

TIME

TIME	RAIN mm hr	TIME	RAIN mm hr	TIME	RAIN mm hr
0.08	2.343	1.17	7.804	2.25	9.514
0.17	2.473	1.25	9.514	2.33	9.514
0.25	2.616	1.33	12.124	2.42	8.304
0.33	2.783	1.42	16.521	2.50	7.361
0.42	2.971	1.50	25.144	2.58	6.607
0.50	3.187	1.58	47.356	2.67	5.991
0.58	3.439	1.67	156.469	2.75	5.481
0.67	3.735	1.75	93.617	2.83	5.050
0.75	4.089	1.83	47.356	2.92	4.682
0.83	4.518	1.92	3.00	4.385	4.08
0.92	5.025	2.00	2.499	3.08	4.089
1.00	5.125	2.08	16.521	3.17	3.846
1.08	6.607	2.17	13.321	3.25	3.631

Comments: 10YR Chicago 4-hr duration

Protocol = 54.60 mm |

004:0002

File Name: 10YR Chicago 4-hr duration

Comments: 10YR Chicago 4-hr duration

TIME

TIME	RAIN mm hr	TIME	RAIN mm hr	TIME	RAIN mm hr
0.08	2.343	1.17	7.804	2.25	9.514
0.17	2.473	1.25	9.514	2.33	9.514
0.25	2.616	1.33	12.124	2.42	8.304
0.33	2.783	1.42	16.521	2.50	7.361
0.42	2.971	1.50	25.144	2.58	6.607
0.50	3.187	1.58	47.356	2.67	5.991
0.58	3.439	1.67	156.469	2.75	5.481
0.67	3.735	1.75	93.617	2.83	5.050
0.75	4.089	1.83	47.356	2.92	4.682
0.83	4.518	1.92	3.00	4.385	4.08
0.92	5.025	2.00	2.499	3.08	4.089
1.00	5.125	2.08	16.521	3.17	3.846
1.08	6.607	2.17	13.321	3.25	3.631

Comments: 10YR Chicago 4-hr duration

Protocol = 54.60 mm |

004:0002

File Name: 10YR Chicago 4-hr duration

Comments: 10YR Chicago 4-hr duration

TIME

TIME	RAIN mm hr	TIME	RAIN mm hr	TIME	RAIN mm hr
0.08	2.343	1.17	7.804	2.25	9.514
0.17	2.473	1.25	9.514	2.33	9.514
0.25	2.616	1.33	12.124	2.42	8.304
0.33	2.783	1.42	16.521	2.50	7.361
0.42	2.971	1.50	25.144	2.58	6.607
0.50	3.187	1.58	47.356	2.67	5.991
0.58	3.439	1.67	156.469	2.75	5.481
0.67	3.735	1.75	93.617	2.83	5.050
0.75	4.089	1.83	47.356	2.92	4.682
0.83	4.518	1.92	3.00	4.385	4.08
0.92	5.025	2.00	2.499	3.08	4.089
1.00	5.125	2.08	16.521	3.17	3.846
1.08	6.607	2.17	13.321	3.25	3.631

Comments: 10YR Chicago 4-hr duration

Protocol = 54.60 mm |

004:0002

File Name: 10YR Chicago 4-hr duration

Comments: 10YR Chicago 4-hr duration

TIME

TIME	RAIN mm hr	TIME	RAIN mm hr	TIME	RAIN mm hr
0.08	2.343	1.17	7.804	2.25	9.514
0.17	2.473	1.25	9.514	2.33	9.514
0.25	2.616	1.33	12.124	2.42	8.304
0.33	2.783	1.42	16.521	2.50	7.361
0.42	2.971	1.50	25.144	2.58	6.607
0.50	3.187	1.58	47.356	2.67	5.991
0.58	3.439	1.67	156.469	2.75	5.481
0.67	3.735	1.75	93.617	2.83	5.050
0.75	4.089	1.83	47.356	2.92	4.682
0.83	4.518	1.92	3.00	4.385	4.08
0.92	5.025	2.00	2.499	3.08	4.089
1.00	5.125	2.08	16.521	3.17	3.846
1.08	6.607	2.17	13.321	3.25	3.631

Comments: 10YR Chicago 4-hr duration

Protocol = 54.60 mm |

004:0002

File Name: 10YR Chicago 4-hr duration

Comments: 10YR Chicago 4-hr duration

TIME

TIME	RAIN mm hr	TIME	RAIN mm hr	TIME	RAIN mm hr
0.08	2.343	1.17	7.804	2.25	9.514
0.17	2.473	1.25	9.514	2.33	9.514
0.25	2.616	1.33	12.124	2.42	8.304
0.33	2.783	1.42	16.521	2.50	7.361
0.42	2.971	1.50	25.144	2.58	6.607
0.50	3.187	1.58	47.356	2.67	5.991
0.58	3.439	1.67	156.469	2.75	5.481
0.67	3.735	1.75	93.617	2	

- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
004:0004 ****
**** COMPUTE VOLUME ****
| ID:1 (201) | DISCHARGE | TIME
|             | (cms)    | (hrs)
| START CONTROLLING AT | .000 | .000
| INFLOW HYD. PEAKS AT | 1.666 | .667
| STOP CONTROLLING AT | .017 | 1.40
|                 |          | 4.140

REQUIRED STORAGE VOLUME (ha.m.)= .2338
TOTAL HYDROGRAPH VOLUME (ha.m.)= .2447
% OF HYDROGRAPH TO STORE = 95.5222

NOTE: Storage was computed to reduce the Inflow
Peak To .017 (cms).
```

```
004:0005 ****
004:0002 ****
004:0002 ****
* END OF RUN : 4
*****
```

```
005:0002 ****
| START | Project dir.: Q:\45013\200\SWMM\HYDRO\60% TMRP-1\
|       | Rainfall dir.: Q:\45013\200\SWMM\HYDRO\60% TMRP-1\
| TZERO = .00 hrs on 0
| METOUT= 2 (output = METRIC)
| NRUN = 005
| NSTORM= 1
# 1=25YR.HYT
*****
```

```
005:0002 ****
| READ STORM | Filename: 25YR Chicago 4-hr duration
| Ptotal= 64.33 mm | Comments: 25YR Chicago 4-hr duration
|                 | TIME RAIN TIME RAIN TIME RAIN TIME RAIN
|                 | hrs mm/hr hrs mm/hr hrs mm hr hrs mm hr hrs mm hr hrs mm hr
|                 | 0.8 2.569 1.17 9.034 2.25 13.050 2.25 13.050 3.33 3.336
|                 | .17 2.718 1.25 11.103 2.33 11.103 3.42 3.336
|                 | .25 2.885 1.33 14.280 2.42 9.637 3.42 3.336
|                 | .33 3.075 1.42 19.656 2.50 8.499 3.50 3.456
|                 | .42 3.292 1.50 30.223 2.58 7.593 3.58 3.292
|                 | .50 3.543 1.58 57.277 2.67 6.856 3.67 3.144
|                 | .58 3.836 1.67 184.478 2.75 6.246 3.75 3.009
|                 | .67 4.183 1.75 112.342 2.83 5.731 3.92 2.771
|                 | .75 4.598 1.83 57.277 2.92 5.298 4.00 2.666
|                 | .83 5.104 1.92 36.251 3.00 4.923 4.08 2.569
|                 | .92 5.734 2.00 25.756 3.08 4.598
|                 | 1.00 6.537 2.08 19.656 3.17 4.312
*****
```

```
1.08 7.593 | 2.17 15.741 | 3.25 4.060 |
```

```
005:0003 ****
***** PROPOSED SITE ****
* AREA 201 -> PROPOSED LONGWOODS ROAD INDUSTRIAL SUBDIVISION
| CALIB STANDYD | Area (ha)= 6.65
| 01201 DE-5.00 | Total Imp (#= 60.00 Dir. Conn. (%)= 50.00
|                 | IMPERVIOUS PERVIOUS
| Surface Area (ha)= 3.99 2.66
| Dev. Storage (mm)= 2.00 5.00
| Average Slope (%)= 1.00 2.50
| Length (m)= 80.00 80.00
| Manning n = .015 .035
| Max.eff.inten.(mm/hr)= 184.48 89.26
| Storage Coeff. over (min)= 5.00 5.00
| Unit Hyd. Peak (min)= 1.91 (ii)
| Unit Hyd. Peak (hrs)= 5.00 5.00
| Unit Hyd. Peak (cms)= *32 *21
* TOTALS*
PEAK FLOW (cms)= 1.62 .51
TIME TO PEAK (hrs)= 1.67 1.667
RUNOFF VOLUME (mm)= 62.33 44.977
TOTAL RAINFALL (mm)= 64.33 64.326
RUNOFF COEFFICIENT = .97 .43
*** WARNING: Storage Coefficient is smaller than DT!
*** Use a smaller DT or a larger area.

(i) CN PROCEDURE SELECTED FOR PREVIOUS LOSSES:
CN* = 74.0 Ta = Dep* Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
*****
```

```
005:0004 ****
***** COMPUTE VOLUME ****
| ID:01 (201) | DISCHARGE | TIME
|             | (cms)    | (hrs)
| START CONTROLLING AT | .000 | *58.3
| INFLOW HYD. PEAKS AT | 2.052 | 1.667
| STOP CONTROLLING AT | .017 | 4.144
|                 |          |
| REQUIRED STORAGE VOLUME (ha.m.)= .2880
| TOTAL HYDROGRAPH VOLUME (ha.m.)= .2891
| % OF HYDROGRAPH TO STORE = 96.2738
*****
```

NOTE: Storage was computed to reduce the inflow peak to .017 (cms).

PROPOSED SITE					
AREA 201 -> PROPOSED LONGWOODS ROAD INDUSTRIAL SUBDIVISION					
CAIB STANDID 01/12/01	DI= 5.00	Area (ha) = Total Imp (\$) =	6.65 60.00	Diff. Conn. (%) =	50.00
Surface Area Dee. Storage Average Slope Length Mannings n	(ha) = (mm) = (%) = (m) = -	Total Imp (\$) = PERVIOUS	2.66 5.00 2.50 80.00 .035		
Max.eff.inten.(mm/hr) = Storage over (min) Storage Coeff. (min)= Unit Hyd. Peak (min)= Unit Hyd. peak (cms) =	205.11 5.00 1.83 (ii.) 5.00 *.32		108.38 5.00 4.80 (ii.) 5.00 .22	*TOTALS*	
PEAK FLOW TIME TO PEAK RUNOFF VOLUME TOTAL RAINFALL	(cms) = (hrs) = (mm) = (mm) =		1.81 1.67 69.91 71.91	.62 1.75 33.10 71.907	.368 (iii) 1.667 51.505 71.907
RUNOFF COEFFICIENT	=		97		.716
*** WARNING: Storage Coefficient is smaller than DT! Use a smaller DT or a larger area.					

(ii) CN PROCEDURE SELECTED FOR PREVIOUS LOSSES:
 $CN^* = 74.0$ $T_a = \text{Def. } \text{STORAGE } (\text{Above})$
 (iii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

COMPUTE VOLUME		DISCHARGE	TIME
ID-01	(201)	(cms)	(hrs)
START CONTROLLING AT		0.00	5.00
INFLOW HD. PEAKS AT		2.368	1.667
STOP CONTROLLING AT		0.017	4.148
REQUIRED STORAGE VOLUME	(ha.m.)	=	
TOTAL HYDROGRAPH VOLUME	(ha.m.)	=	
% OF HYDROGRAPH TO STORE		=	

NOTE: Storage was computed to reduce the In peak to .017 (cms).

006:0004-----
 006:0002-----
 006:0002-----
 006:0002-----
 006:0002-----
 006:0002-----
 ** END OF RUN : 6

PROPOSED SITE					
* AREA 201 > PROPOSED LONGWOODS ROAD INDUSTRIAL SUBDIVISION					
	Area	(ha) =	6.65	Dir. Conn. (%) =	50.00
CALIB STANDARD DT = 5.00	Total Imp (%) =	60.00	PERVIOUS	(i)	
Surface Area (ha) =	3.99	2.66			
Dep. Storage (mm) =	2.00	5.00			
Average Slope (%) =	1.00	2.00			
Length (m) =	80.00	80.00			
Mannings n =	.015				
Max.eff.inten.(mm/hr) =	225.19	127.80			
Storage Coeff. (min) =	5.00	5.00			
Unit Hyd. Tpeak (min) =	5.00	5.00			
Unit Hyd. peak (cms) =	.32	.23			
TOTALS					
PEAK FLOW (cms) =	2.00	.74	2.675	(iii)	
TIME TO PEAK (hrs) =	1.67	.75	1.667		
RUNOFF VOLUME (mm) =	77.25	38.51	77.933		
TOTAL RAINFALL (mm) =	79.15	79.5	79.251		
RUNOFF COEFFICIENT =	.97	.49	.97		
*** WARNING: Storage Coefficient is smaller than DT!					
Use a smaller DT or a larger area.					

007:0004 -----

(i) CN PROCEDURE SELECTED FOR PERVERIOUS LOSSES:
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

TIME (hrs)	DISCHARGE (cms)
START CONTROLLING AT INLW HYD. PEAKS AT STOP CONTROLLING AT	.500 2.675 1.667 .017 4.150
REQUIRED STORAGE VOLUME (ha.m.) = % OF HYDROGRAPH TO STORE	3739 97.0423

NOTE: Storage was computed to reduce the inflow peak to .017 (cms).

007:0005 -----

TIME (hrs)	DISCHARGE (cms)
START CONTROLLING AT INLW HYD. PEAKS AT STOP CONTROLLING AT	.500 2.675 1.667 .017 4.150
REQUIRED STORAGE VOLUME (ha.m.) = % OF HYDROGRAPH TO STORE	3739 97.0423

NOTE: Storage was computed to reduce the inflow peak to .017 (cms).

007:0006 -----

007:0007 -----

PROPOSED SITE					
* AREA 201 > PROPOSED LONGWOODS ROAD INDUSTRIAL SUBDIVISION					
	Area	(ha) =	6.65	Dir. Conn. (%) =	50.00
CALIB STANDARD DT = 5.00	Total Imp (%) =	60.00	PERVIOUS	(i)	
Surface Area (ha) =	3.99	2.66			
Dep. Storage (mm) =	2.00	5.00			
Average Slope (%) =	1.00	2.00			
Length (m) =	80.00	80.00			
Mannings n =	.015				
Max.eff.inten.(mm/hr) =	225.19	127.80			
Storage Coeff. (min) =	5.00	5.00			
Unit Hyd. Tpeak (min) =	5.00	5.00			
Unit Hyd. peak (cms) =	.32	.23			
TOTALS					
PEAK FLOW (cms) =	2.00	.74	2.675	(iii)	
TIME TO PEAK (hrs) =	1.67	.75	1.667		
RUNOFF VOLUME (mm) =	77.25	38.51	77.933		
TOTAL RAINFALL (mm) =	79.15	79.5	79.251		
RUNOFF COEFFICIENT =	.97	.49	.97		
*** WARNING: Storage Coefficient is smaller than DT!					
Use a smaller DT or a larger area.					

007:0003 -----

PROPOSED SITE					
* AREA 201 > PROPOSED LONGWOODS ROAD INDUSTRIAL SUBDIVISION					
	Area	(ha) =	6.65	Dir. Conn. (%) =	50.00
CALIB STANDARD DT = 5.00	Total Imp (%) =	60.00	PERVIOUS	(i)	
Surface Area (ha) =	3.99	2.66			
Dep. Storage (mm) =	2.00	5.00			
Average Slope (%) =	1.00	2.00			
Length (m) =	80.00	80.00			
Mannings n =	.015				
Max.eff.inten.(mm/hr) =	225.19	127.80			
Storage Coeff. (min) =	5.00	5.00			
Unit Hyd. Tpeak (min) =	5.00	5.00			
Unit Hyd. peak (cms) =	.32	.23			
TOTALS					
PEAK FLOW (cms) =	2.00	.74	2.675	(iii)	
TIME TO PEAK (hrs) =	1.67	.75	1.667		
RUNOFF VOLUME (mm) =	77.25	38.51	77.933		
TOTAL RAINFALL (mm) =	79.15	79.5	79.251		
RUNOFF COEFFICIENT =	.97	.49	.97		
*** WARNING: Storage Coefficient is smaller than DT!					
Use a smaller DT or a larger area.					

007:0002 -----

PROPOSED SITE					
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	Area	(ha) =	6.65	Dir. Conn. (%) =	50.00
CALIB STANDARD DT = 5.00	Total Imp (%) =	60.00	PERVIOUS	(i)	
Surface Area (ha) =	3.99	2.66			
Dep. Storage (mm) =	2.00	5.00			
Average Slope (%) =	1.00	2.00			
Length (m) =	80.00	80.00			
Mannings n =	.015				
Max.eff.inten.(mm/hr) =	225.19	127.80			
Storage Coeff. (min) =	5.00	5.00			
Unit Hyd. Tpeak (min) =	5.00	5.00			
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(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY,
THAN THE STORAGE COEFFICIENT.

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08:004		08:005		08:006		08:007	
COMPUTE VOLUME ID:01 (201)	DISCHARGE (hrs)	START CONTROLLING AT INFLOW HD. PEAKS AT STOP CONTROLLING AT	TIME (hrs)	REQUIRED STORAGE VOLUME TOTAL HYDROGRAPH VOLUME TO STORE % OF HYDROGRAPH VOLUME (ha.m.)	TIME (hrs)	REQUIRED STORAGE VOLUME TOTAL HYDROGRAPH VOLUME TO STORE % OF HYDROGRAPH VOLUME (ha.m.)	TIME (hrs)
9.42	27.388	15.50	1.338	21.58	671	15.50	21.58
9.50	42.582	15.58	1.319	21.67	667	15.58	21.67
9.59	81.716	15.67	1.301	21.75	662	15.67	21.75
9.67	265.689	15.75	1.283	21.83	658	15.75	21.83
9.75	161.512	15.83	1.266	21.92	654	15.83	21.92
9.83	17.716	15.92	1.250	22.00	650	15.92	22.00
9.92	51.283	16.00	1.233	22.08	646	16.00	22.08
0.00	36.148	16.08	1.218	22.17	642	16.08	22.17
0.08	27.388	16.17	1.202	22.25	638	16.17	22.25
0.17	21.793	16.25	1.187	22.33	634	16.25	22.33
0.25	1.962	16.33	1.173	22.42	630	16.33	22.42
0.33	15.202	16.42	1.158	22.50	626	16.42	22.50
0.42	13.133	16.50	1.145	22.58	622	16.50	22.58
0.50	11.532	16.58	1.131	22.67	618	16.58	22.67
0.58	10.262	16.67	1.118	22.75	615	16.67	22.75
0.67	9.232	16.75	1.105	22.83	611	16.75	22.83
0.75	8.383	16.83	1.093	22.92	607	16.83	22.92
0.83	7.672	16.92	1.080	23.00	604	16.92	23.00
0.92	7.069	17.00	1.068	23.08	600	17.00	23.08
1.00	6.551	17.08	1.057	23.17	597	17.08	23.17
1.08	6.103	17.17	1.045	23.25	593	17.17	23.25
1.17	5.711	17.25	1.034	23.33	590	17.25	23.33
1.25	5.365	17.33	1.023	23.42	587	17.33	23.42
1.33	5.059	17.42	1.013	23.50	583	17.42	23.50
1.42	4.785	17.50	1.002	23.58	580	17.50	23.58
1.50	4.549	17.58	.992	23.67	577	17.58	23.67
1.58	4.318	17.67	.982	23.75	574	17.67	23.75
1.67	4.117	17.75	.972	23.83	571	17.75	23.83
1.75	3.934	17.83	.962	23.92	567	17.83	23.92
1.83	3.766	17.92	.953	24.00	564	17.92	24.00
1.92	3.613	18.00	.944	24.08	561	18.00	24.08
2.00	3.471	18.08	.935	24.17	558	18.08	24.17
2.08	3.340	18.25	.925	24.25	555	18.25	24.25
2.17	3.219	18.41	.917	24.33	552	18.41	24.33

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中華書局影印

* AREA 201 -> PROPOSED LONGWOODS ROAD INDUSTRIAL SUBDIVISION

Dep. Storage	(mm) =	2.00	5.00
Average Slope	(%) =	1.00	2.50
Length	(m) =	80.00	80.00
Mannings n	=	.015	.035

Max.eff.Inten. (mm/hr) = 265,*69 192.02

Storage Coeff. (min) = 1.65 (11) 4.02 (11)

Unit Hyd. peak (cms) = *32 *24

PEAK FLOW (cms) = 2.37
PEAK FLOW (cms) = 1.09
PEAK FLOW (cms) = 3.461 (iii)

RUNOFF VOLUME (mm) = $\frac{1}{3} \times 33 = 11$

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Use a smaller BI or a larger area.

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(11) TIME SIEF (11) SHOULD BE SMALLER OR EQUAL

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